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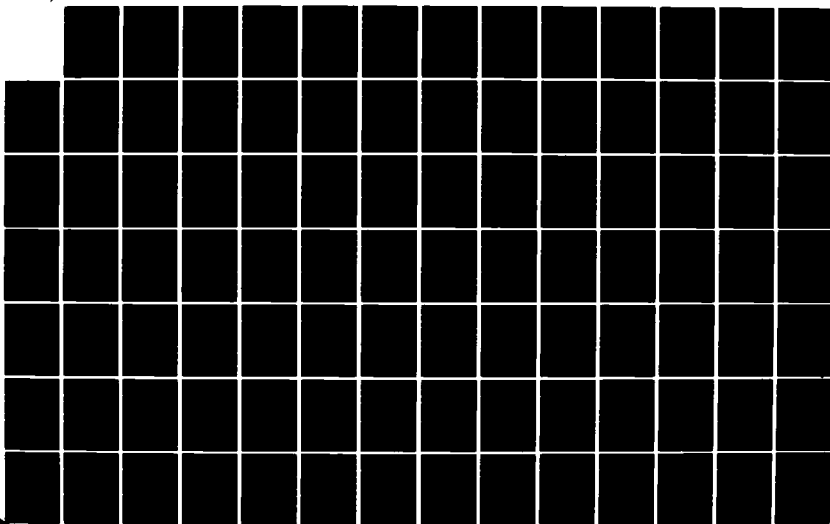
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TO TURN MISSILE IN THE TERMINAL HOMING PHASE(U) NAVAL
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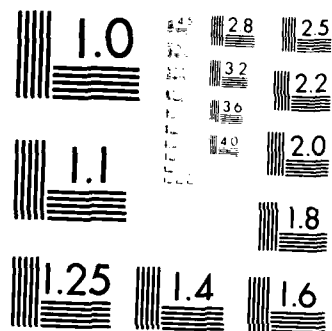
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THESIS

AN INVESTIGATION INTO THE CONTROL
LIMITATIONS OF A BANK TO TURN MISSILE
IN THE TERMINAL HOMING PHASE

by

Barton P. Anderson

September 1984

Thesis Advisor:

M. D. Hewett

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simulation program to examine the effects of electronic countermeasures (ECM) blinking and glint upon the missile's control system and accuracy against a simulated medium sized combatant vessel traveling at 20 knots perpendicular to the missile's track over the earth. In addition to the standard attack profile involving a popout attack, several other attack profiles were tested including skid-to-turn (STT) control laws and a ballistic trajectory. Miss distances varied from 3.7 feet without ECM or glint to 35 feet with ECM operating. Susceptibility of the missile to ECM blinking varied with the blinking frequency. The largest miss distances occurred with ECM frequencies below 0.2 Hz and near 6.0 Hz. Analysis of the data showed that errors at the low frequencies were primarily caused by the bank command loop of the autopilot. Those at the higher frequency were due to the roll rate command loop. Variation of the geometry of the missile's flight profile had no significant impact upon missile accuracy except that, without a popup maneuver, the roll rate channel demonstrated a marked decrease in effectiveness. Variation of the autopilot gain in the roll rate control loop changed the frequency at which degradation occurred but actually increased its effects. Skid to turn control laws were tested however the missile was unable to produce the necessary sideforce needed to track a passive target and produced undesirable coupling in the flight controls. An attempt to use the altitude command channel to fly a ballistic profile was unsuccessful due to instabilities created in the control system. It is recommended that a popup maneuver be included in the terminal guidance of a BTT cruise missile and that further tests be conducted to determine the extent to which autopilot modifications and gain adjustments can decrease the effectiveness of an ECM blinker against a BTT missile.

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An Investigation into the Control
Limitations of a Bank to Turn Missile
in the Terminal Homing Phase

by

Barton P. Anderson
Commander, United States Navy
P.S., Wheaton College, 1970

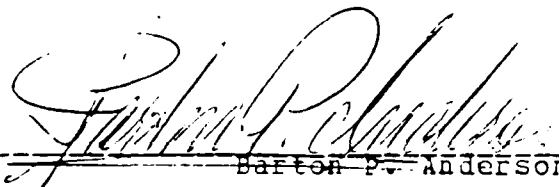
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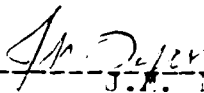
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ABSTRACT

The purpose of this thesis was to examine guidance and control deficiencies in a bank to turn (BT) cruise missile with limited roll authority in the terminal homing phase of its mission. A six degree of freedom simulation of a typical BT missile was translated into FORTRAN H from the Continuous System Modelling Program (CSMP) simulation language and run on the IBM System 370 computer. Tests were conducted with the revised simulation program to examine the effects of electronic countermeasures (ECM) blinking and glint upon the missile's control system and accuracy against a simulated medium sized combatant vessel traveling at 20 knots perpendicular to the missile's track over the earth. In addition to the standard attack profile involving a popout attack, several other attack profiles were tested including skid-to-turn (STT) control laws and a ballistic trajectory. Miss distances varied from 3.7 feet without ECM or glint to 85 feet with ECM operating. Susceptibility of the missile to ECM blinking varied with the blinking frequency. The largest miss distances occurred with ECM frequencies below 0.2 Hz and near 6.0 Hz. Analysis of the data showed that errors at the low frequencies were primarily caused by the bank command loop of the autopilot. Those at the higher frequency were due to the roll rate command loop. Variation of the geometry of the missile's flight profile had no significant impact upon missile accuracy except that, without a popout maneuver, the roll rate channel demonstrated a marked decrease in effectiveness. Variation of the autopilot gain in the roll rate control loop changed the frequency at which degradation occurred but actually increased its effects. Skid to turn control laws were tested

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I. INTRODUCTION

A. BACKGROUND

Bank-To-Turn (BTT) control is utilized extensively on missiles which must cruise for long ranges within the atmosphere. These missiles utilize a primary lifting surface (wing) and smaller controlling surfaces as on a conventional airplane. This method has two primary advantages. First, the wing provides lift to support the missile's weight at a relatively high efficiency thereby permitting longer ranges for a given size engine and fuel load. Second, the lift vector can be positioned by banking the missile to provide large lateral accelerations resulting in excellent turn performance. Certain BTT cruise missile configurations, however, use differential tail for roll control as opposed to ailerons and suffer from poor roll rate and acceleration performance. It is the investigation into the control limitations of a BTT cruise missile configured this way in the terminal homing phase which is the subject of this thesis.

B. STATEMENT OF THE PROBLEM

In order to provide compact storage of a BTT missile, the main wings are usually folded back and designed to snap into position as the missile emerges from its canister at launch. Because of this feature, it is generally not feasible to install roll control devices at the extremities of the wings. Roll control is normally provided by differential actuation of the tail fins of the missile. Because of their short moment arm and small area and because the main wing has a relatively large degree of roll damping, BTT missiles are limited in their ability to roll rapidly.

Because of the need to bank the missile in order to align its lift vector in the desired direction it has been suggested that the requirement for rapid roll maneuvering in the terminal phase of flight would limit the accuracy of the missile. In addition, natural fluctuations in the position of the radar target, known as glint, and artificial fluctuations due to the presence of electronic countermeasures (ECM) might further degrade the performance of a BT missile.

C. MISSION SCENARIO

1. Control Configuration

The missile simulated in this thesis is a hypothetical bank to turn cruise missile with limited roll control authority. Its design incorporates characteristics typical of many similar designs. The missile is equipped with a standard rudder for yaw control and stabilizers for both roll and pitch control. Inner loop closures for stabilization and command are included in the simulation. Command loop closures consist of normal acceleration, bank angle, and lateral acceleration. The lateral acceleration command system can be used as a turn coordinator in the bank-to-turn mode (normal) mode or as a lateral load factor (NY) command system in a skid-to-turn mode. Outer loop closures are provided for altitude and flight path angle. The autopilot control loop design is presented in detail in [Ref. 1].

2. Target

The target is assumed to be a surface combatant ship located initially 24,000 feet due North from the missile and moving East at a constant speed of 20 knots. It is assumed that the missile seeker tracks an aim point perfectly. The aim point is located nominally 10 feet above the ship's

waterline and amidships. This aim point continually shifts as a function of ECM blinking and a random glint simulation.

3. ECM Simulation

The ECM blinker simulation shifts the radar target seen by the missile's seeker forward and aft from the true target aim point by ± 75 feet along the ships longitudinal axis at a specified frequency. The aim point is simultaneously shifted vertically ± 10 feet at the same frequency.

4. Attack Profiles

The attack profile used as a baseline for this simulation began at 50 feet of altitude at a speed of Mach 0.75. The missile tracked toward the target using proportional navigation in azimuth and altitude hold at 50 feet. At a range of 18000 feet the missile rolled to 60 degrees of bank and turned away from the target to the right until the target line of sight was offset by 10 degrees. When the offset was reached, the missile climbed to an altitude of approximately 250 feet and then dove toward the target using proportional navigation in both azimuth and elevation. This mission profile is often referred to as a popout attack.

Variations of this mission included eliminating the 10 degree offset turn and/or the climb to altitude and substituting skid-to-turn control laws for some phase of the mission. A ballistic altitude profile was also attempted.

D. EXISTING WORK

In order to examine the existence of such problems and to test several proposed solutions, a six degree of freedom simulation of a typical BTT cruise missile was produced by LCDR Kent Watterson and published in [Ref. 1]. This simulation was produced using the IBM Continuous System Modelling

Program (CSMP III) simulation language. A detailed description of this language and its constructions is presented in [Ref. 2] and [Ref. 3]. The simulation included dynamics, autopilot, guidance and mission profiles. It did not represent any specific missile but, rather, included characteristics typical of missiles configured in this way. In order to overcome limitations imposed upon the simulation program by the available computer installation, this CSMP program was rewritten in extended FORTRAN H. This allowed greater flexibility and full utilization of the DISPLA graphics programming package available at NPS. A complete copy of the program listing is presented in Appendix D.

E. SCOPE OF TESTS

The tests conducted with the revised simulation program were limited to examining the effects of ECM blinking and glint upon the missile's control system and accuracy against a simulated medium sized combatant vessel traveling at 20 knots perpendicular to the missile's track over the earth. Alternate attack profiles using modified flight geometry and, in some cases, skid-to-turn control laws were also tested. A listing of the different flight profiles examined is presented in table I.

For all flight tests of the missile, certain parameters were held constant. A list of these values is presented in table II.

TABLE I
Missile Attack Profile Test Configurations

	OFFSET BURN	POP-UP	REOLIF	TOPN
BASLINE	X	X	0.5	BTT
II		X	0.5	BTT
III			0.5	BTT
IV		X	0.1	BTT
V		X	0.5	STT
VI		X	0.5	*

* 90 degree bank on ballistic terminal trajectory

TABLE II
Simulation Variables Held Constant

Variable Name	Value
*****	*****
Radar Burn-Through Range	500 ft
EC* Blinker Shifts:	
Longitudinal	± 75 ft
Lateral	± 00 ft
Vertical	± 10 ft
Baseline guidance scheme:	
Offset	10 deg
PopUp Altitude	100 ft
PopUp Range	13000 ft
Roll rate limit	75 dps
*****	*****

II. PROGRAM DESCRIPTION

A. INTEGRATION OF THE EQUATIONS OF MOTION

This simulation uses the linear, six degree of freedom equations of flight developed by Boskam in [Ref. 5:vol 1] and modified by Hewett in [Ref. 4]. The CSMP program developed by Watterson [Ref. 1] used a variable step Runge-Kutta integration method. The FORTRAN translation program uses a

$$\text{INTEGRAL}(\text{YDOT DT}) = \text{Y} + (\text{YDOT}) * \text{DT} \quad (\text{eqn 2.1})$$

simple Eulerian integration which is given by equation 2.1. The incremental time element, DT, is fixed at 0.01 seconds and the integration period lasts for less than 30 seconds.

B. PROGRAM NOMENCLATURE

A detailed description of the nomenclature used throughout the simulation program is presented in Appendix C. The variable names used in the FORTRAN translation are, with few exceptions, the same as those used in the the CSMP simulation.

C. AXIS SYSTEM

The simulation uses a right handed earth reference frame where the x-axis points North, the y-axis points East and the z-axis points down. However, altitude and vertical velocity are always given as positive upwards (i.e. ALTITUDE = -Z). For plotting the geographical track in the output routines, the axes are transformed so that the X,Y, and Z axes point East, North and upward, respectively.

D. PROGRAM ARCHITECTURE

The FORTRAN simulation program consists of an executive program which calls seven major subroutines which are briefly described as follows.

1. Executive Program

The main calling program is short and handles only three tasks. It increments the TIME variable for each integration cycle. It calls the output data storage routine, PREPAP, at the specified output interval and it controls the execution of multiple flights within a single program run changing one or more key variables between the runs.

2. Subroutine INIT

This subroutine contains a small section of executable statements which resets variables to their initial value when more than one flight is flown during a program run. Included with this subroutine is the BLOCK DATA subroutine which must be used to initialize all variables in named common areas. The majority of the BLOCK DATA subprogram is taken up with arrays listed in table form which contain the aerodynamic coefficient data for the missile. Static coefficients which are functions of one variable are shown in figures A.2 through A.9 Static coefficients which are functions of two parameters are presented in figures A.10 through A.13 Dynamic coefficients are assumed to be constant and are not presented graphically.

3. Subroutine MISSION

This subroutine dictates the mission profile. It is divided into sections which activate in sequence as the mission progresses. Each section takes the flight dynamics data for the missile, compares it with the target

acquisition data (generated in subroutine TGTNAV) and outputs vertical and horizontal acceleration commands in the geographic earth reference frame. These in turn are translated into commanded bank angle and normal load factor for the missile according to equations 2.2 and 2.3. A diagram

$$PHIC = \text{ARCTAN}(AYC/AZC) \quad (\text{eqn 2.2})$$

$$NCC = AZC \cos(PHI) + AYC \sin(PHI) \quad (\text{eqn 2.3})$$

of these vectors is given in figure A.1. Different terminal attack profiles are implemented using variations of this subroutine, MISSN1 and MISSN2, which are presented in Appendices E and F.

4. Subroutine ABPILOT

This subroutine takes the commanded normal load factor and bank angle and applies them to the missile autopilot system. A detailed description of the design of the missile's autopilot is presented in reference [Ref. 1]. The output of the control system is delivered in terms of conventional airplane elevator, aileron and rudder control positions. These are mixed to obtain the commanded missile fin positions. The control limits of ± 15 degrees are applied to the fins and these controls are then unmixed to obtain the limited conventional control positions. The dynamics of the servo actuators that move the tail surfaces are modelled as a first order real pole. Although CSM2-III provides macros that perform the simulation of many types of transfer functions within the control system only the first order real pole transfer function was necessary for this program. It is modelled in the FORTRAN translation using subroutine REALPI, presented in the program listing in Appendix C.

5. Subroutine AEFC

Subroutine AEFC uses two table lookup routines to retrieve the aerodynamic coefficients from the data presented in figures A.2 through A.18. Linear interpolations are used to obtain values between given parameters. Error messages are printed when the input parameters are outside the bounds of the data in the lookup table and these are suppressed after about 5 successive integration cycles. AEFC completes the buildup process, uses these data to compute the forces and moments on the aircraft and then integrates the equations of motion to update all of the aircraft's flight parameters and position information.

6. Subroutine TGTNAV

The TGTNAV subroutine navigates the target vessel on a course of East at a steady speed of 20 knots. It shifts the position of the radar target relative to its real position according to the ECM and GLINT parameters. The GLINT offset is produced by multiplying the GLINT shift in each axis by a random number between -1 and 1. The GLINT offset is calculated every output interval rather than 100 times per second. The ECM offset is switched according to the sign of a sine wave which runs at the ECM blinking frequency, FFEQ. These offsets are then added to the actual target position to produce the radar target position. Line of sight angles and rates are calculated from this information with the assumption that the seeker has perfect pointing capability.

7. Subroutine PFEPAE

At intervals specified by the output counter, this subroutine is called and stores up to 20 variables in a large array call PTS. The output interval used for all tests

was 0.20 sec. The PTS array is passed to the output routines when the simulation run is completed. This subroutine also converts output variables from radian to degree format and, in the final attack phase, calculates four error functions. These error functions are time averaged differences between commanded variables (e.g. BANK or ROLL RATE) and their actual counterparts. These are later used to analyse the performance of the control system under various conditions.

8. Subroutine OUTPUT

OUTPUT produces 3 forms of output information. The primary data output lists the value of MISDST (the distance at which the missile passed the target at its closest approach), the value of the error functions at the end of the mission, and the ranges of all the variables stored. These data are also printed to another file followed by the full contents of the PTS array in tabular form. This gives a numerical history of all the output variables from the start to the finish of the mission. (Normally, to save disk space, this file was routed to a dummy variable. It was needed only when detailed data histories of a portion of the mission were required.)

OUTPUT also calls the necessary DISPLA routines to print graphs of the output variables. The independent variable in six graphs is TIME. In the seventh graph the positions of the missile and the target ship are plotted in three dimensional space for each output interval. Each of the graphs in this subroutine are controlled by the setting of 7 flags in the first column of the data statement at the beginning of the routine (0 to pass over and 1 to plot).

III. BASELINE ATTACK CONFIGURATION

A. AUTOPILCT ROLL RATE COMMAND LOOP ADJUSTMENT

Initial testing of the simulation was conducted on the CSMP version of the program. The frequency of the ECM blinker was varied from 0.2 Hz to a maximum of 2.0 Hz and the roll performance of the missile was graphed. Figure A.19 shows the commanded roll rate and actual roll rate plotted against time for the duration of a thirty second flight straight toward the target at a constant altitude of 50 feet. The target's radar position was blinked at a rate of 0.4 Hz and roll rate command was limited to 75 degrees per sec. In the figure, the command oscillations increased in magnitude as the target range decreased and, after 24 seconds, the autopilot commanded the maximum rate with every shift of the target's apparent position. While the commanded roll rate remained at 75 degrees per second, the actual roll rate never exceeded 35 degrees per second. Figure A.20, which plots the fin positions as a function of time, shows that the fin servos never used more than 3 degrees (of the maximum 15) of travel in either direction. To remedy this problem, the missile autopilot roll rate command loop gain (KROLLPT in the program) was increased from 0.1 to 0.5. The value of this gain had been set by Watterson [Ref. 1] using root locus based upon the perturbation equations of motion [Ref. 4] in steady state level flight. Figures A.21 and A.22 show the results of a subsequent run with the revised guidance loop. Steady state error in roll rate was significantly reduced and the full range of available flight controls (± 15 deg.) was used. This difference in the autopilot was incorporated into the baseline program and remained throughout all subsequent tests.

E. BASELINE PROGRAM

In order to provide a baseline performance record against which to examine the effects of ECM and glint and/or alternate attack profiles on the accuracy of the missile and the performance of its control system, a standard, pop-out attack with an offset turn was selected and flown and is used as a standard for comparison. The parameters which apply to this baseline are listed in table II. Figures A.23 through A.28 are a complete record of the baseline program run without any ECM or glint offsets applied to the target. Figures A.29 through A.35 are a complete record of the baseline program run with the ECM blinker operating at 0.2 Hz and the glint feature operating. The complete tabular data output from this latter run is presented in Appendix F.

IV. FREQUENCY SCAN TESTS

A. ERROR FUNCTIONS

For testing the effects of glint and ECM at various blinking frequencies against the control system of the missile, a quantitative measure of the system's effectiveness was needed. Four error functions were developed for this purpose. The time weighted difference between the commanded value and the actual value of a variable was computed according to equation 4.1. This time weighted error was summed over all of the time intervals and divided by the

$$EFE = DT * ABS(COMMAND - VARIABLE) \quad (\text{eqn 4.1})$$

total time to produce the error function for the variable. The variables for which these functions were computed are

TABLE III
Error Function Variables

VARIABLE	COMMAND VARIABLE
*****	*****
1. BANK	BANK
2. ROLL RATE	ROLLR
3. AZIMUTH LOS RATE	0.0
4. ELEVATION LOS RATE	0.0
*****	*****

listed in Table III. In the terminal phase where proportional guidance is used in both the azimuth and elevation channels, the commanded azimuth and elevation angle rates are zero to produce a constant bearing intercept.

B. ECM PHASING

At low frequency blinking rates, the phase of the ECM blinker at the start of the mission had a very large effect on the miss distance. To minimize the distortion of the data due to this effect, a phase variable was added to the ECM generator to change the phase of the blinker at the start of each run. Four runs were conducted at each frequency using values of 0.0, $\pi/2$, π , $(3/2)\pi$ for the phase variable. The data for each frequency were averaged to get mean values for the miss distance and each error function.

C. BASELINE TEST RESULTS

1. ECM Frequency Scans

Four simulated flights were conducted at each frequency from 0.0 to 30 Hz. Glint was disabled for the course of these tests. The attack profile flown was the baseline popout attack mission. A graph of the mean value of the miss distance (MISDST) versus frequency is presented in figure A.36. The data show that maximum miss distance occurs in the very low frequency range of the order of 0.2 Hz and again to a lesser degree in the vicinity of 6 Hz. Figures A.40 and A.44 are plots of the error function means against frequency for the autopilot command errors and the tracking errors respectively. These data show that the bank angle command loop is susceptible to ECM frequencies of the order of 0.2 Hz while the roll rate command loop is primarily responsible for the errors that occur at the higher frequencies in the range of 5 to 10 Hz. Figure A.44 also demonstrates that the time averaged tracking errors follow the same basic pattern.

Figures A.48 through A.53 demonstrate these effects in flight. Figures A.48 and A.51 show the bank angle and

roll rate performance of the baseline missile without ECM. Both variables track closely to their commanded values with the exception of a small, steady state error in the rate channel which is most evident at large commanded rates. Figures A.49 and A.50 show the effects of ECM at 0.4 and 6.0 Hz upon the bank channel. In figure A.49 significant errors exist in bank as the system cannot keep up with the large, sudden changes in commanded bank caused by the ECM shift of the target. The bracket in figure A.49 is drawn between two corresponding points to emphasize the large lag present in the channel. Roll rate tracks close to its commanded level at this frequency.

At 6.0 Hz, figures A.52 and A.53 show the opposite effect. In figure A.53 the bracket emphasizes the large lag that exists in the aircraft roll response to the rapid changes in rate command. The bank command loop at this frequency has effectively filtered out most of the high frequency input.

The results of the frequency scan tests showed that the baseline BTT cruise missile simulated by the program was more susceptible to ECM frequencies in the vicinity of 0.2 and 6.0 Hz due to the excitation of the bank and roll rate command loops respectively. If distances greater than 20 ft from the center of the target are considered likely misses, then the excitation of the roll rate command loop did not produce enough error to cause a likely miss. The best results, from the target's point of view, will be obtained with low blinking frequencies in the vicinity of 0.2 Hz.

2. Effects of Glint

In order to isolate the effects of glint, the baseline configuration was flown without ECM or glint and again with glint only. Figure A.33 shows a trace of the random glint

displacement applied to the target's position as a function of time. Figures A.23 through A.28, which trace the missile's load factor, bank angle, roll rate and flight controls without glint, may be compared with figures A.54 through A.57 which show the same traces for the mission with glint.

The miss distance recorded without glint and an ECM phase of 0 was 3.7 feet. The distance measured with glint was 9.4 feet. Although these distances are very small compared with the miss distances achieved with ECM, the degradation induced by glint was large (154 percent) compared to the best obtainable value. Ways of minimizing the effect of random perturbations in the target position due to radar glint will make a significant improvement in the missile's accuracy in the absence of ECM and should be developed.

Since the miss distances without ECM and glint were very small compared to those obtained with very slow blinking frequencies (0.05 to 0.2 Hz), further tests should be run concentrating on ECM in the very low frequency range. These tests should obtain a much larger sample of ECM phases in order to best define the shape of the miss distance curve below 0.2 Hz.

D. ALTERNATE CONFIGURATION FREQUENCY SCAN RESULTS

1. Mission Profile

Similar frequency scan profiles were flown using the MISSN1 (Appendix E) subroutine to generate the guidance commands for configurations II, III and IV. These attack profiles committed the offset turn and proceeded straight toward the target using proportional navigation in azimuth from start to finish. The popup maneuver was commenced at 15000 feet from the target. Of ranges from 20,000 to 5,000

feet which were tested, 15,000 feet produced the most consistent hits with a 200 foot popup altitude command. All subsequent tests of these missile attack configurations used 15,000 ft. popup range and a 200 ft. altitude command when the maneuver was performed.

An algorithm was added to the baseline proportional guidance scheme for the terminal phase which ensured that the missile rolled to place the nearest of the positive or negative Z-axis vectors on the direction commanded by the guidance system. This ensured that the missile would command negative load factor rather than trying to roll the missile upside down as it reached the apex of its climb. Azimuthal accelerations commanded by the guidance were still achieved by banking the missile except for configuration V.

A complete set of mission profile graphs for configurations II, III, and IV against a target with glint and ECM blinking at 0.2 Hz are presented in figures A.58 through A.75

2. Frequency Scan Results

a. Miss Distances

Each configuration was flown against the target four times per test frequency. The tests covered a range of blinker frequencies from 0.05 through 30.0 Hz. The mean miss distances recorded are graphically presented as a function of frequency in figures A.37 through A.39. The results obtained were very similar to those obtained from the baseline configuration. There were two areas of higher than normal errors, one at low frequency below 0.2 Hz and another at a higher frequency near 6.0 Hz. Table IV compares the miss distances for each of the configurations.

The maximum values that occurred for all configurations appeared at the same frequencies with one

TABLE IV
Maximum Miss Distances

CONFIGURATION	FREQ. RANGE (Hz)	LOCATION (ft)	MAGNITUDE
BASLINE	0.20 - 20.0	≤ 0.20 6.00	≥ 45 22
II	0.05 - 21.0	≤ 0.05 6.00	≥ 75 17
III	0.10 - 30.0	≤ 0.10 5.50	≥ 75 17
IV	0.10 - 30.0	≤ 0.10 N/A	≥ 75 N/A

exception: changing the roll rate gain from 0.5 to 0.1 eliminated the maximum at the higher frequency. In addition, the magnitude of the errors did not differ significantly. (The baseline shows a smaller magnitude because the data do not extend below 0.2 Hz. while the other configurations were tested down to 0.1 and 0.05 Hz). Changing the attack geometry of the missile did not significantly alter its susceptibility to ECM jamming within the scope of these tests. Altering the gain of the roll rate command channel in the missile autopilot significantly decreased its susceptibility to ECM blinking at higher frequencies. Further testing should be conducted to determine the extent to which autopilot modifications and gain adjustments can decrease the effectiveness of an ECM blinker against a bank to turn missile.

1. Autopilot Errors

Figures A.40 through A.43 graphically present the error functions for both the bank angle and roll rate command loops within the autopilot. These functions are representative of the ability of the missile to follow the

commands given it by the autopilot (the higher the function, the poorer the performance). As with the baseline configuration these figures demonstrate that the bank angle loop contributed most to the errors at low frequency and the roll rate loop contributed most at the higher frequency. Table V

TABLE V
Autopilot Errors

CONFIGURATION	BANK ERROR		RATE ERROR	
	FREQ (HZ)	MAGNI- TUDE	FREQ (HZ)	MAGNI- TUDE
BASELINE	0.4	0.22	7.0	0.19
II	0.6	0.17	8.0	0.18
III	0.5	0.18	8.0	0.27
IV	0.6	0.21	2.0	0.37

is a summary of these graphs.

Magnitude of the bank error function and the frequency at which it occurred were not significantly altered in any one of the tested configurations. Changing the geometry of the attack had no effect on the frequency at which ECM was most effective against the roll rate control system, however the magnitude of the errors were increased by approximately 50 percent when the popup maneuver was eliminated (configuration III).

Decreasing the roll rate autopilot gain from 0.5 to 0.1 (configuration IV) moved the resonant frequency for the roll rate command system to a lower frequency but

increased the magnitude of the errors by more than 100 percent. This effect is reflected in the miss distance graphs (figures A.36 through A.39) in the disappearance of the distinct maximum at 6 Hz and a widening of the lower maximum (figure A.39). Altering the autopilot gain was effective at moving the resonant frequency to a different region but could not eliminate its effect.

c. Tracking System Errors

Errors in the tracking loops are charted in figures A.44 through A.47. These errors follow the trends of the autopilot and miss distance errors. At the lower frequencies, azimuth performance was dominant while at higher frequencies the elevation tracking loop experienced the largest degradation.

3. Skid To Turn Guidance Results

The MISSN1 subroutine was further modified to allow the lateral load factor command variable, NYC, to be set according to guidance commands rather than being kept at zero for turn coordination purposes. The commanded bank angle was set to zero in the terminal phase in order to examine the effectiveness of lateral G command. No changes to the basic dynamics of the autopilot were made. The missile was flown in this configuration against a passive target. Figures A.76 through A.81 present the full data set from this test. The missile splashed into the water 99 feet left and short of the target. Once the missile came within 5 seconds of impact, cross coupling between the rudder channel and normal load factor, roll rate and bank can be seen in the figures. Although the rudder commands were never saturated, neither could the lateral load factor control loop create enough sideforce to follow the ship's lateral drift to the right. The addition of ECM and/or glint would have

only worsened the performance of the missile in this configuration. No further tests of this configuration were conducted. The use of skid-to-turn control laws could not produce sufficient sideforce to adequately follow a passive crossing target and produced excessive coupling into the longitudinal and lateral flight controls of the missile.

4. Ballistic Trajectory

Because the majority of the apparent target shift with ECM blinking occurs in the horizontal plane, an attempt was made to place the missile on a ballistic trajectory and then roll the aircraft to 90 degrees angle of bank until impact using the primary load factor to follow the ECM target and lateral load factor to maintain the ballistic trajectory. In order to fly the ballistic trajectory, the altitude hold system was driven by a commanded altitude slaved to a parabolic trajectory derived from the missile's vertical speed and range to the target according to equation

$$ALT = HMDOT * RANGE / V_H + (G/2) * (RANGE / V_T)^2 + 10 \quad (\text{eqn 4.2})$$

4.2. where HMDOT, V_H and V_T are the vertical, horizontal and total speeds of the missile. The controlling subroutine used for this mission was MISSN2 and is presented in Appendix F.

Figures A.82 through A.85 show that the addition of the dynamics of the altitude command loop made the missile's control system unstable. Oscillations to the limits occurred in normal load factor and in roll rate. Considerable cross coupling occurred between the lateral-directional and longitudinal dynamics of the missile. The attempt to fly a ballistic trajectory using the existing altitude control system was unsuccessful. In order to fly the attempted profile, a major redesign of the missile's autopilot would be necessary.

V. CONCLUSIONS

The conclusions listed below were derived from analysis of the results of simulated flights conducted using the baseline popout attack profile configuration, three variations of the baseline attack, a skid-to-turn control configuration and a ballistic altitude trajectory.

A. BASELINE CONFIGURATION TESTS

At low frequency blinking rates, the phase of the ECM blinker had a very large effect on the miss distance.

The best obtainable performance for the baseline mission without ECM or glint was a miss distance of 3.7 feet. The addition of GLINT produced a miss distance of 9.7 feet, a degradation of 154 percent.

The bank angle command loop of the missile autopilot in the baseline configuration was especially susceptible to ECM frequencies of the order of 0.2 Hz while the roll rate command loop was primarily affected at the higher frequencies in the range of 5 to 10 Hz. The time averaged tracking errors also followed the same basic pattern.

If distances greater than 20 ft from the center of the target are considered likely misses, then the excitation of the roll rate command loop did not produce enough error to cause a likely miss. The best results, from the target's point of view, will be obtained with low blinking frequencies in the vicinity of 0.2 Hz.

B. ALTERNATE ATTACK PROFILE CONFIGURATIONS

In terms of the average miss distances measured, changing the flight geometry of the missile did not signifi-

cantly alter its susceptibility to ECM jamming within the scope of these tests.

Altering the gain of the roll rate command channel in the baseline missile autopilot significantly decreased its susceptibility to ECM blinking at higher frequencies.

Changing the geometry of the attack had no effect on the magnitude of the bank error function and the frequency at which its maximum occurred.

Changing the roll rate gain from 0.5 to 0.1 had no noticeable affect on the magnitude of the bank error function and the frequency at which its maximum occurred.

Changing the geometry of the attack had no effect on the frequency at which ECM was most effective against the roll rate control system, however the magnitude of the errors were increased by approximately 50 percent when the popup maneuver was eliminated (configuration III).

Decreasing the roll rate autopilot gain from 0.5 to 0.1 (configuration IV) moved the resonant frequency for the roll rate command system to a lower frequency but increased the magnitude of the errors by more than 100 percent. This effect was reflected in the miss distance data by the disappearance of the distinct maximum at 6 HZ and a widening of the lower maximum. Altering the autopilot gain was effective at moving the resonant frequency to a different region but could not eliminate its effect and, in this case enlarged it.

Errors in the azimuth and elevation tracking loops closely followed the trends of the autopilot and miss distance errors. At the lower frequencies, azimuth performance was dominant while at higher frequencies the elevation tracking loop experienced the largest degradation.

C. SKID TO TURN CONTROL

The use of skid-to-turn control laws could not produce sufficient sideforce to adequately follow a passive crossing target and produced excessive coupling into the longitudinal and lateral flight controls of the missile.

D. BALLISTIC ATTACK PROFILE

The attempt to fly a ballistic trajectory using the existing altitude control system was unsuccessful. In order to fly the attempted profile, a major redesign of the missile's autopilot would be necessary.

VI. RECOMMENDATIONS

Ways of minimizing the effect of random perturbations in the target position due to radar glint will make a significant improvement in the missile's accuracy in the absence of ECM and should be developed.

Further testing should be conducted to determine the extent to which autopilot modifications and gain adjustments can decrease the effectiveness of an ECM blinker against a bank to turn missile.

Since the elimination of a popup increased roll rate errors by 50 percent, a popup profile is recommended for the terminal phase of a BTT cruise missile. Further testing should be conducted to determine the effects of different popup profiles on the susceptibility of the roll rate command system to ECM blinking.

Since the miss distances without ECM and glint were very small compared to those with very slow blinking frequencies (0.05 to 0.2 Hz), further tests should be run concentrating on ECM in the very low frequency range. These tests should obtain a much larger sample of ECM phases in order to best define the shape of the miss distance curve below 0.2 Hz.

APPENDIX A
FIGURES

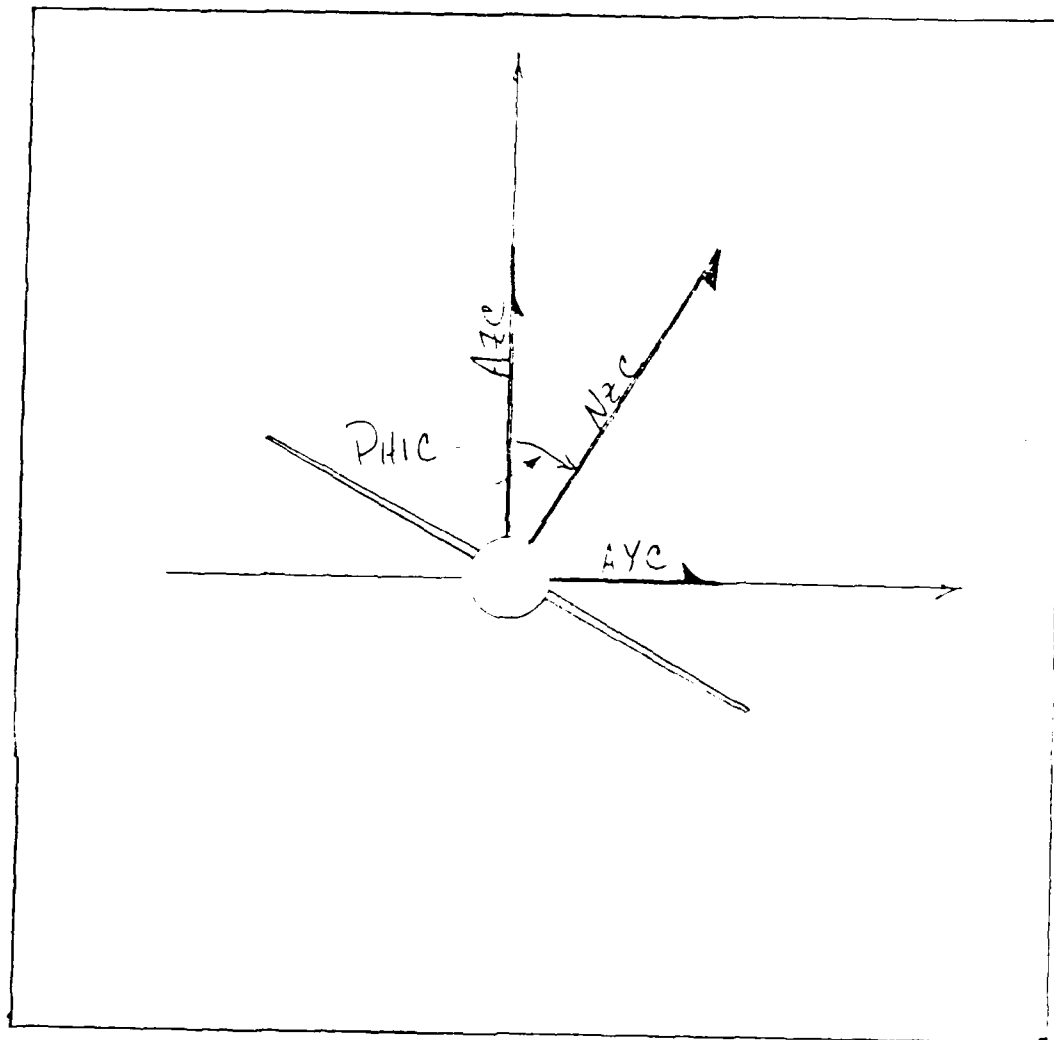


Figure A.1 Load Factor Commands.

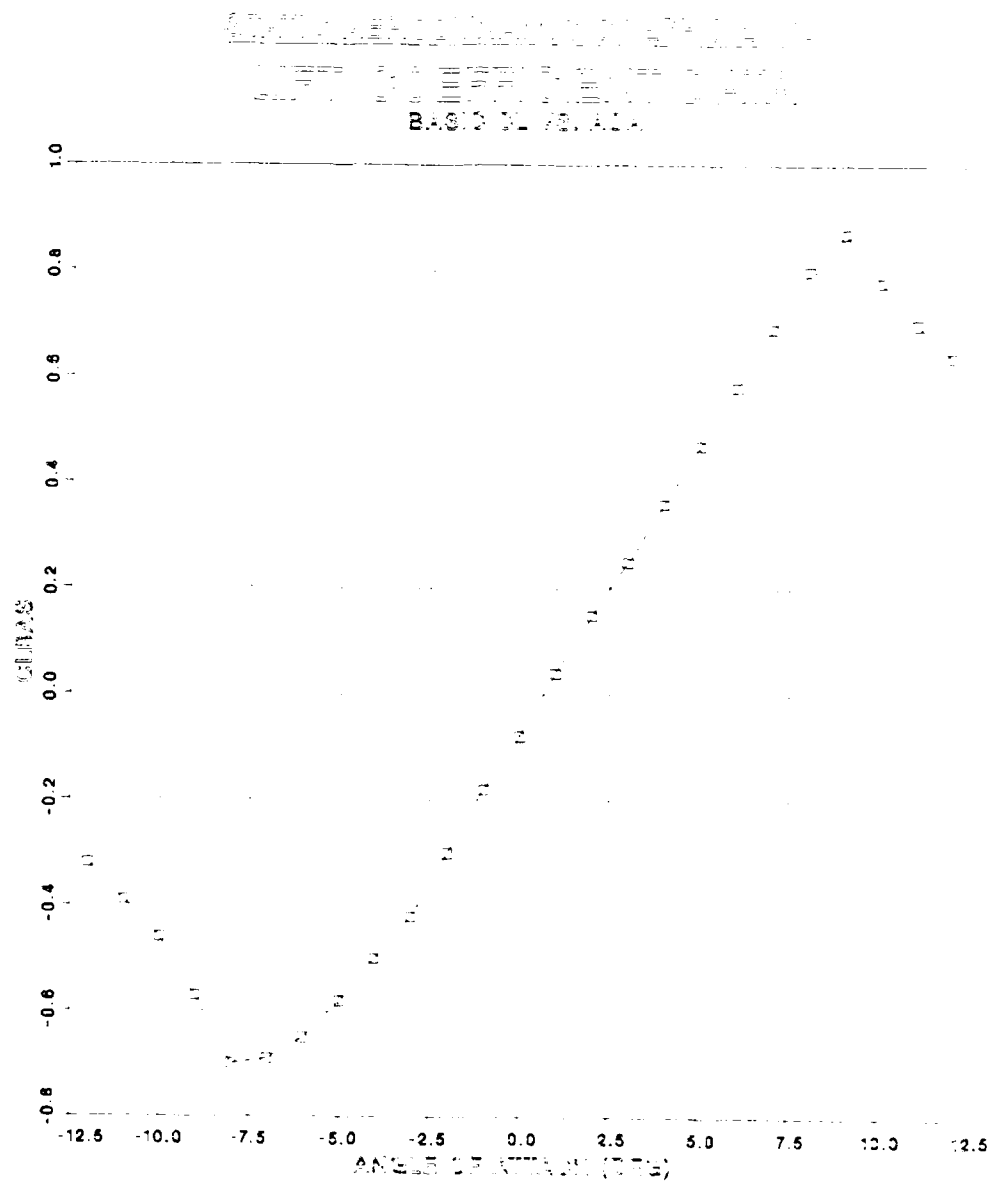


Figure A.2 Data Array LFT1.

BANK OF AMERICA

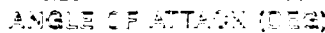


Figure A.4 Data Array DRG1.

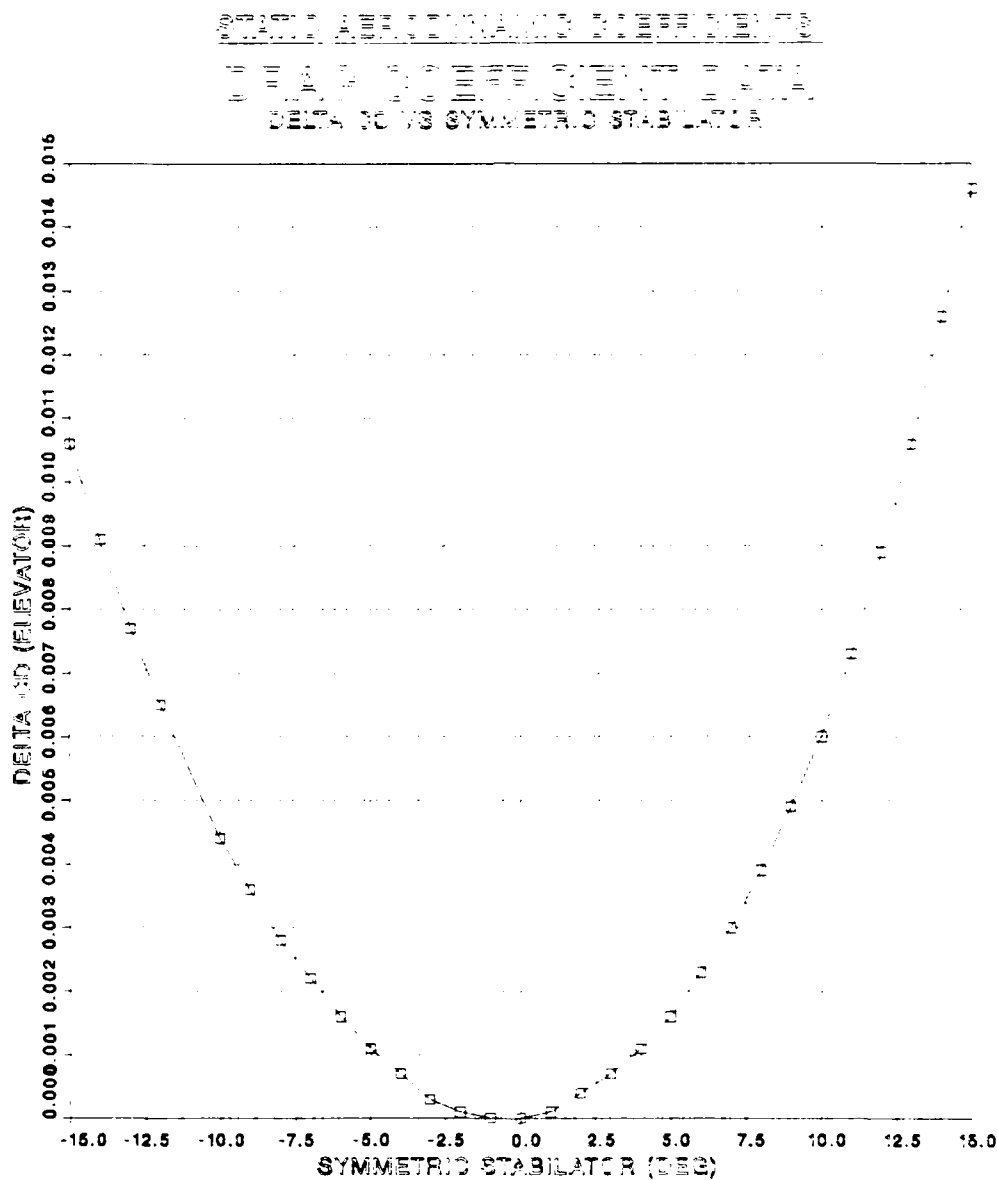


Figure A.5 Data Array DRG2.

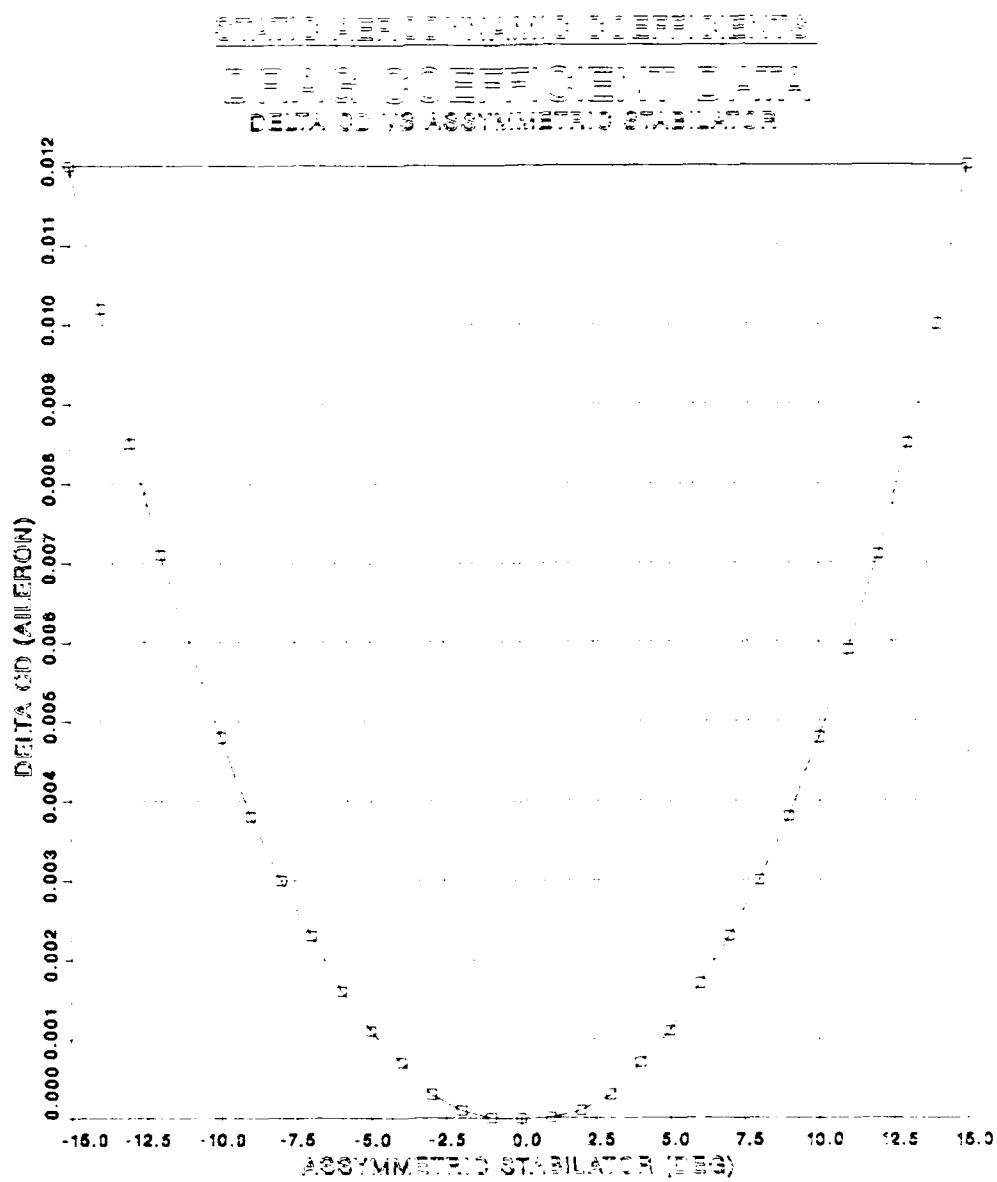


Figure A.6 Data Array DRG3.



Figure A.7 Data Array DPG4.

BIOGRAPHICAL

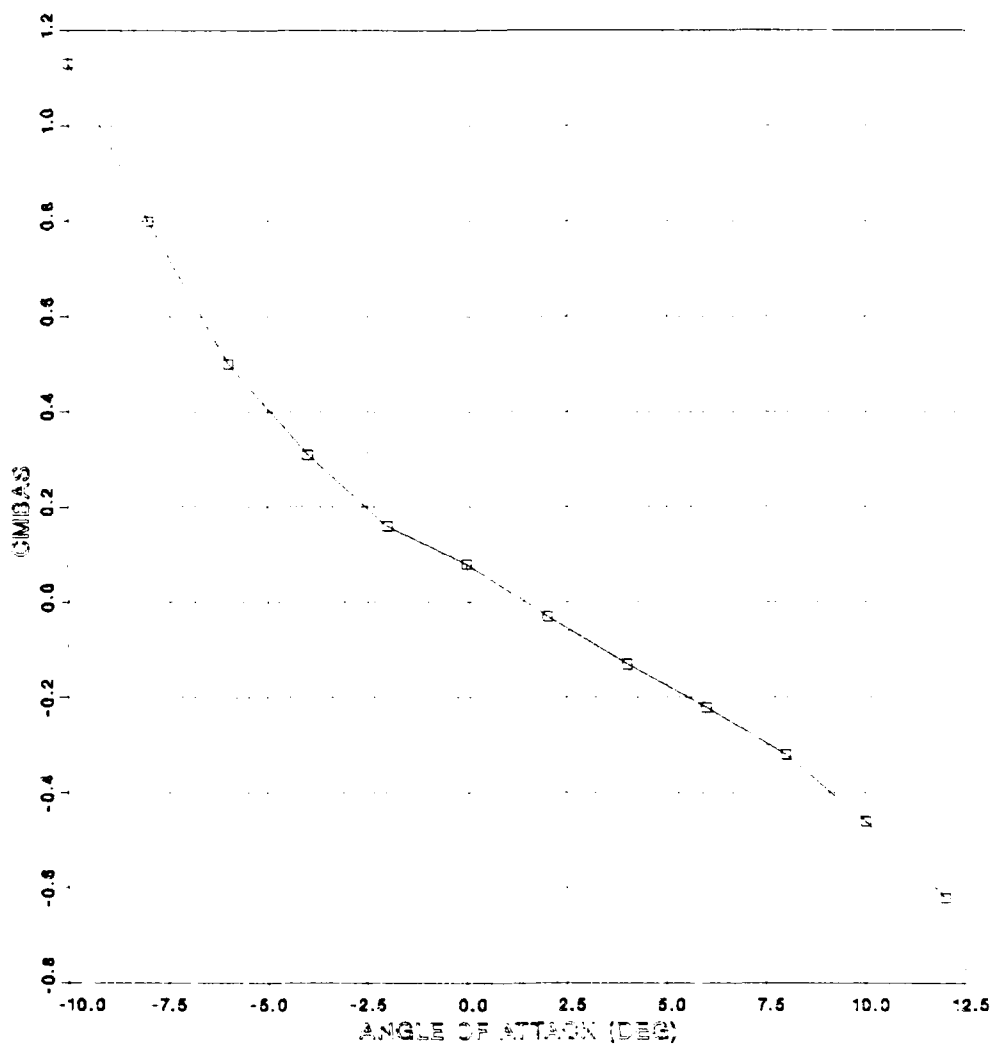


Figure A.8 Data Array PTCH1.

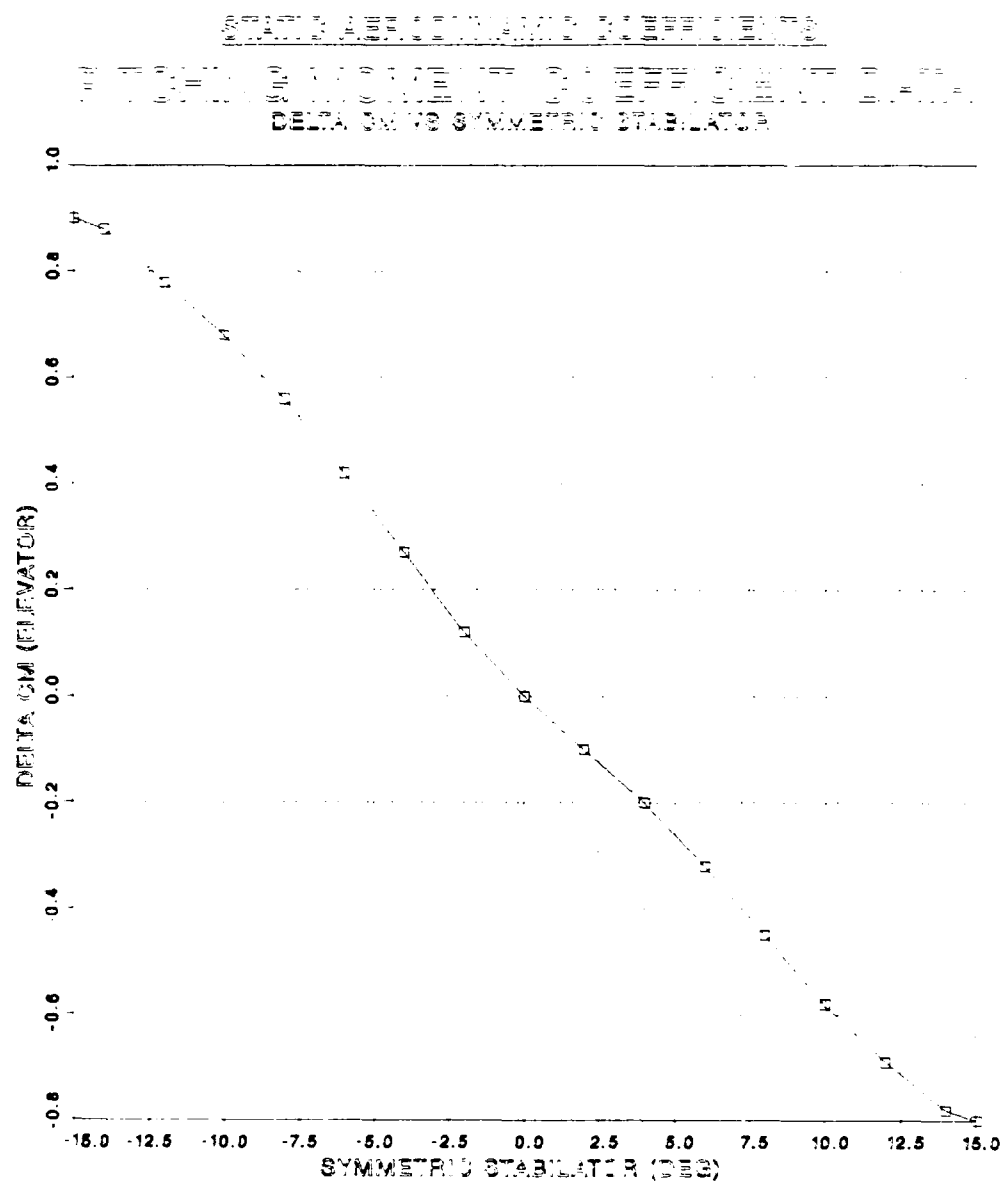


Figure A.9 Data Array PTCH2.

CONTROL SURFACE DEFLECTION
COEFFICIENT DATA
 BASED ON $C_{L\beta}$

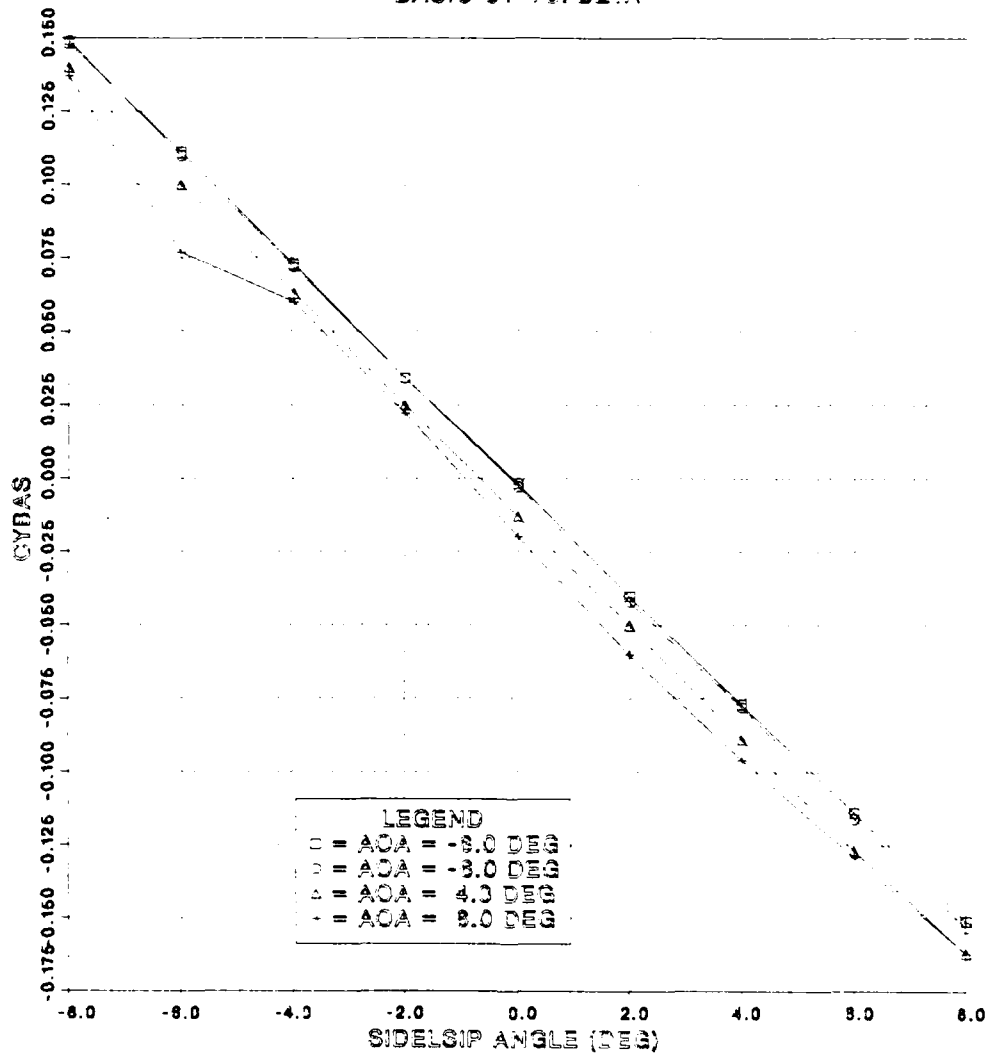


Figure A.10 Data Array SID1.

332 000 000 000

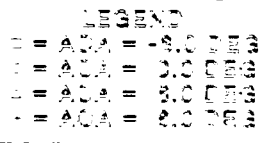


Figure A.12 Data Array SID3.

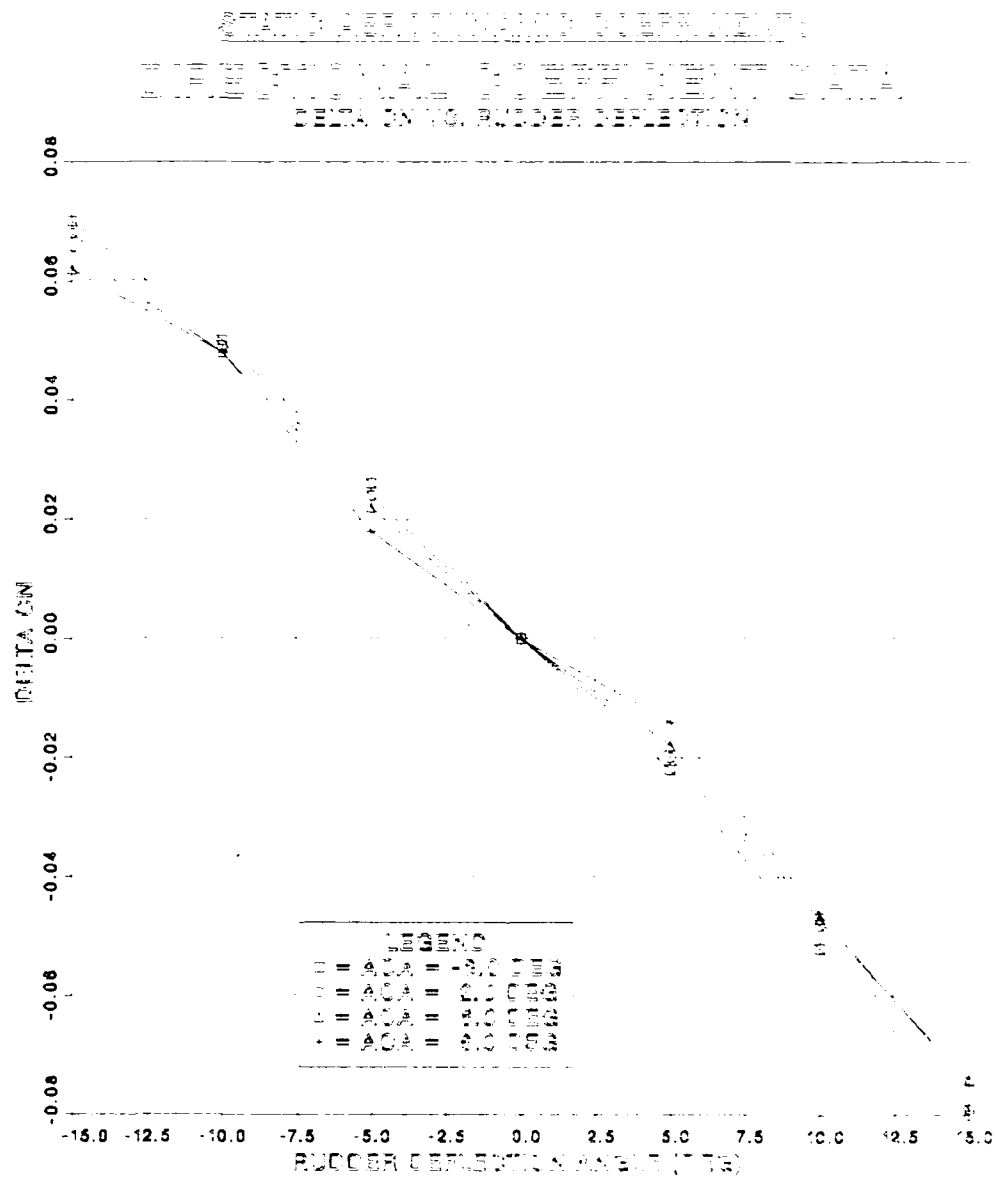


Figure A.14 Data Array DREC2.

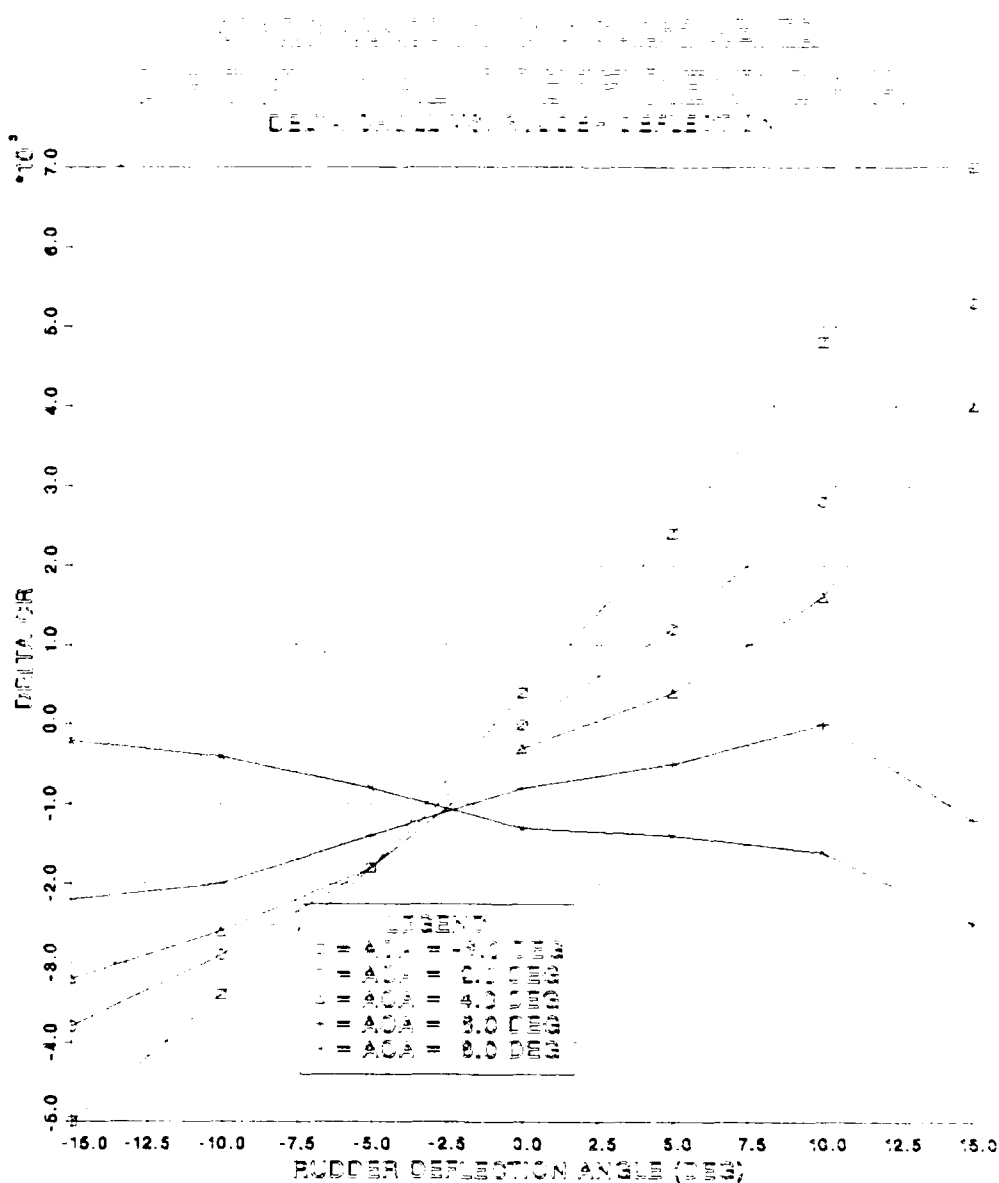


Figure A.15 Data Array DR3C3.

Figure 1 is a scatter plot with regression lines showing the relationship between the difference in time of day (X-axis) and the difference in time of day (Y-axis). The X-axis ranges from -15.0 to 15.0, and the Y-axis ranges from -0.04 to 0.02. The graph displays several data series, each represented by a different symbol and a corresponding regression line. The series are labeled with numbers 1 through 10. The regression lines show a positive correlation between the difference in time of day and the difference in time of day.

Series	Symbol	Regression Line
1	+	$y = 0.001x + 0.012$
2	•	$y = 0.001x + 0.010$
3	△	$y = 0.001x + 0.008$
4	×	$y = 0.001x + 0.006$
5	○	$y = 0.001x + 0.004$
6	□	$y = 0.001x + 0.002$
7	◇	$y = 0.001x + 0.000$
8	▽	$y = 0.001x - 0.002$
9	◊	$y = 0.001x - 0.004$
10	⊠	$y = 0.001x - 0.006$

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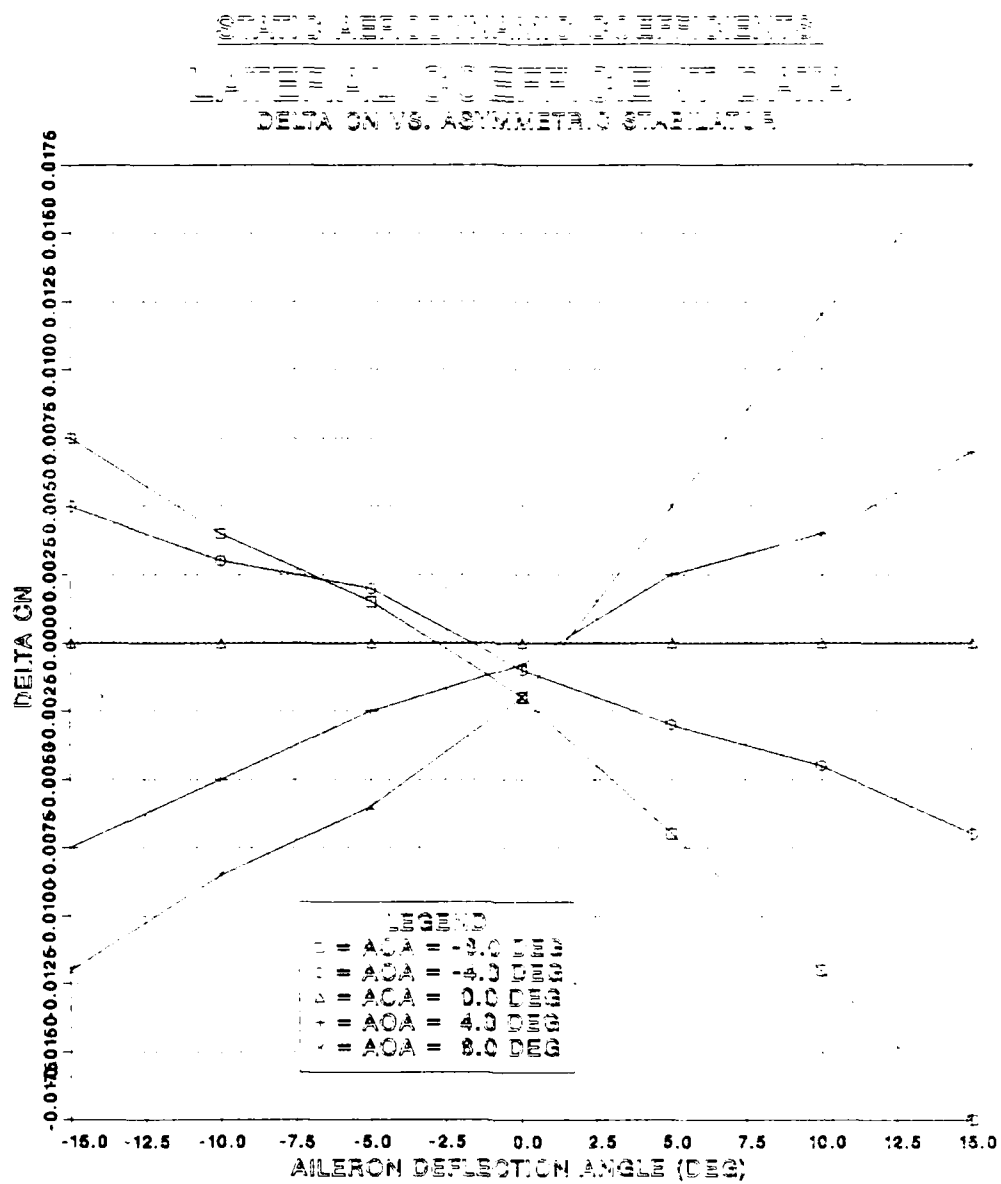


Figure A.17 Data Array LTFL2.

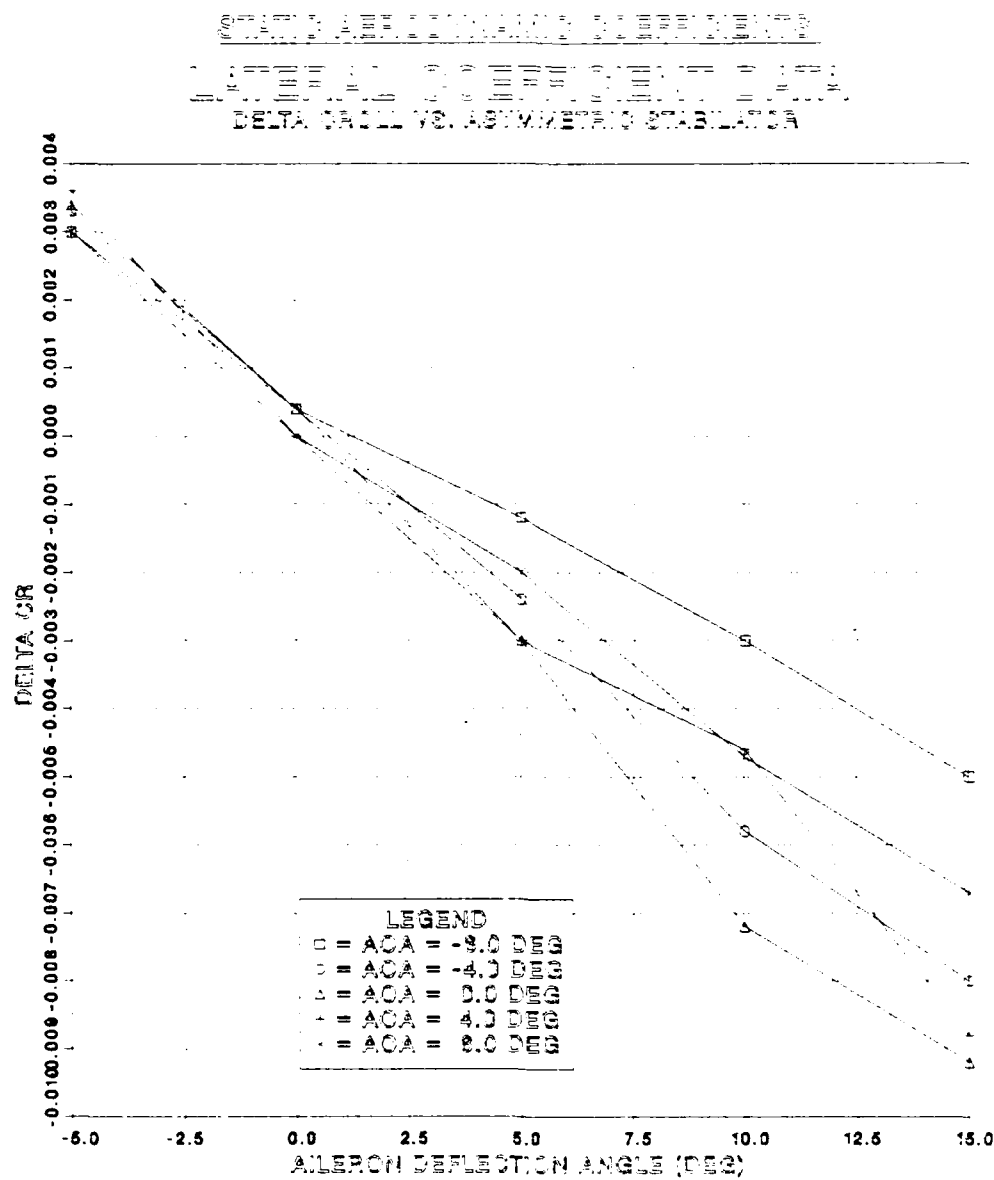


Figure A.18 Data Array LTFL3.

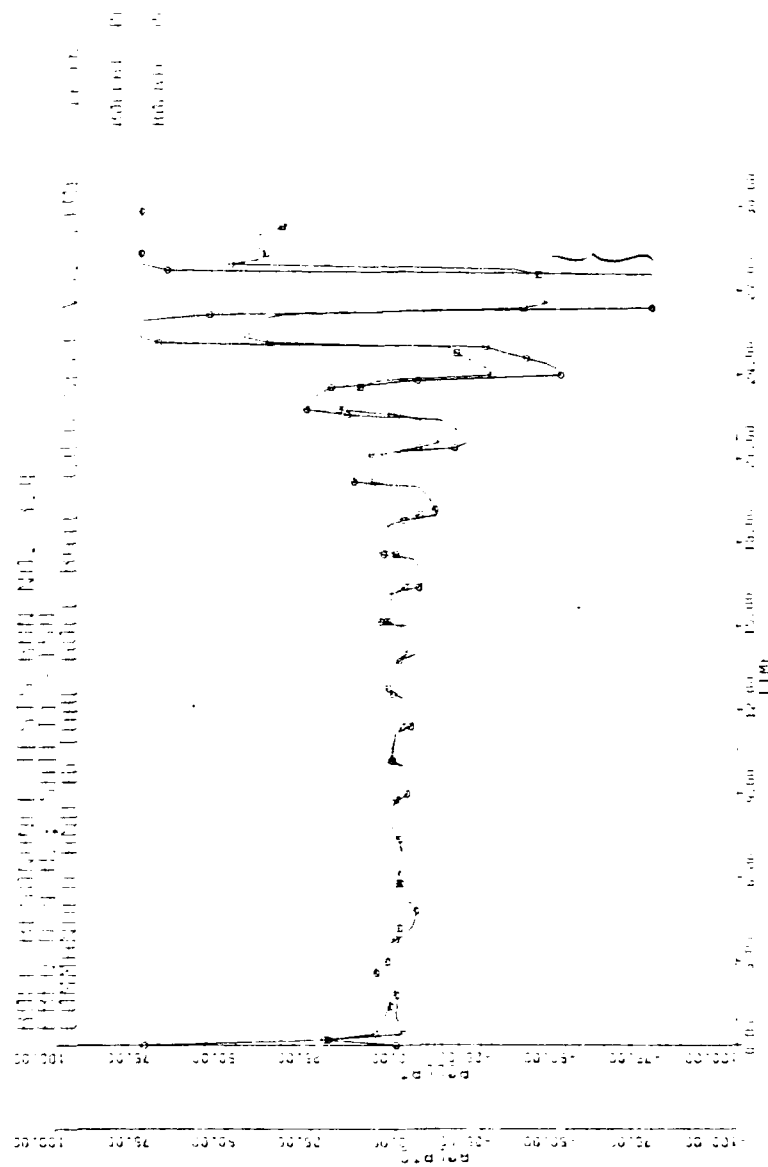


Figure A.19 CSMP Data (Roll Rate) - KROLLR = 0.1.

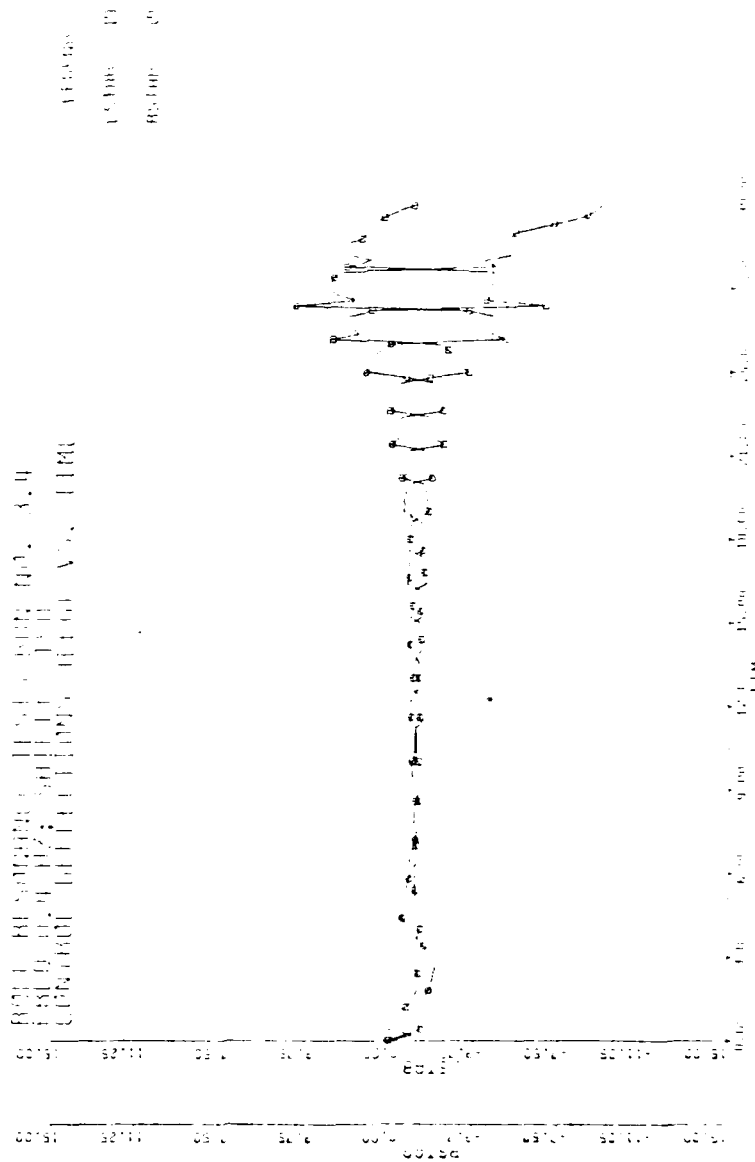


Figure A.20 CSMP Data (Controls) - KROLLF = 0.1.

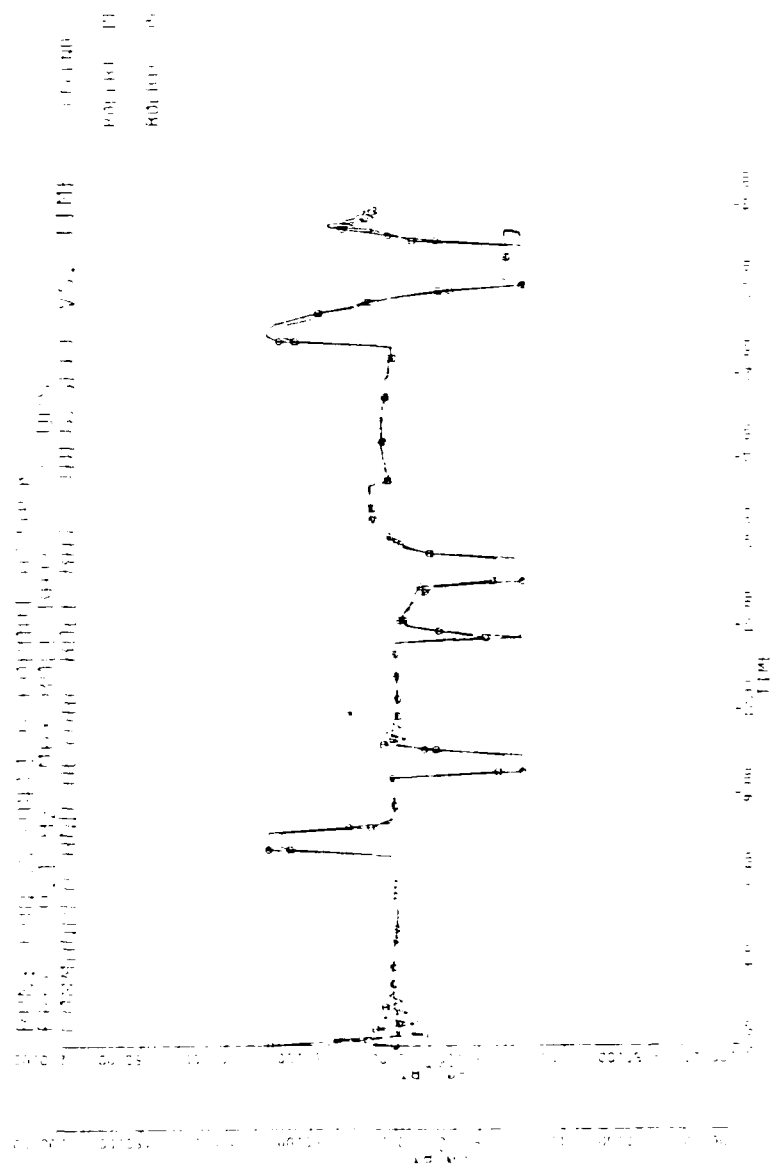


Figure A.21 CSMP Data (Roll Rate) - KROLLP = 0.5.

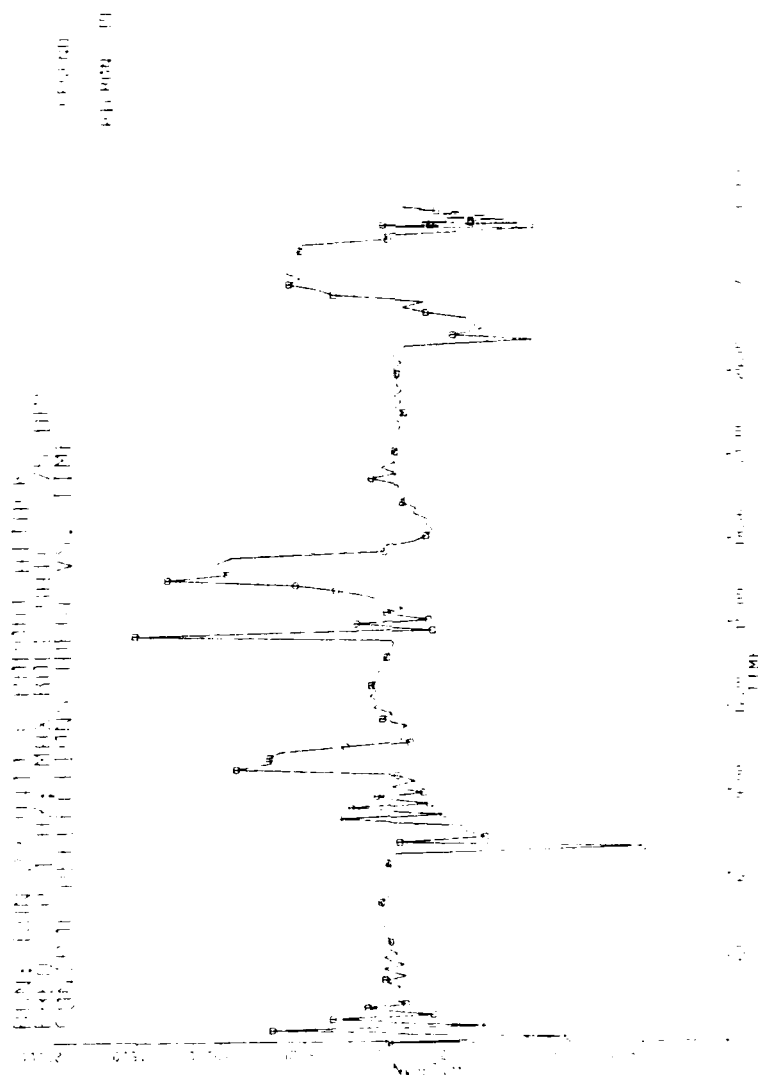


Figure A.22 CSMP Data (Controls) - Krollr = 0.5.

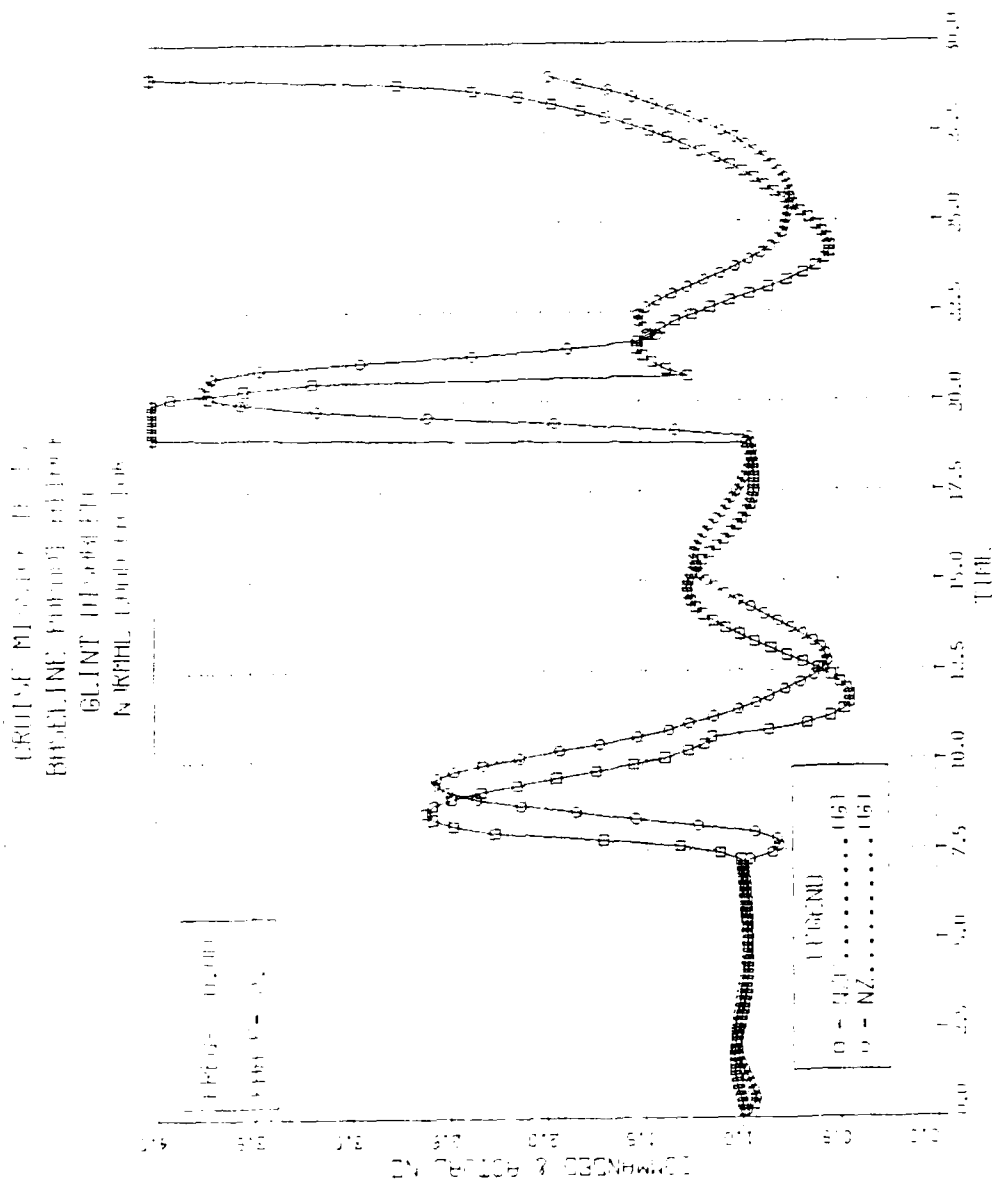


Figure A.23 Baseline - no FCM or GLINT - Load Factor.

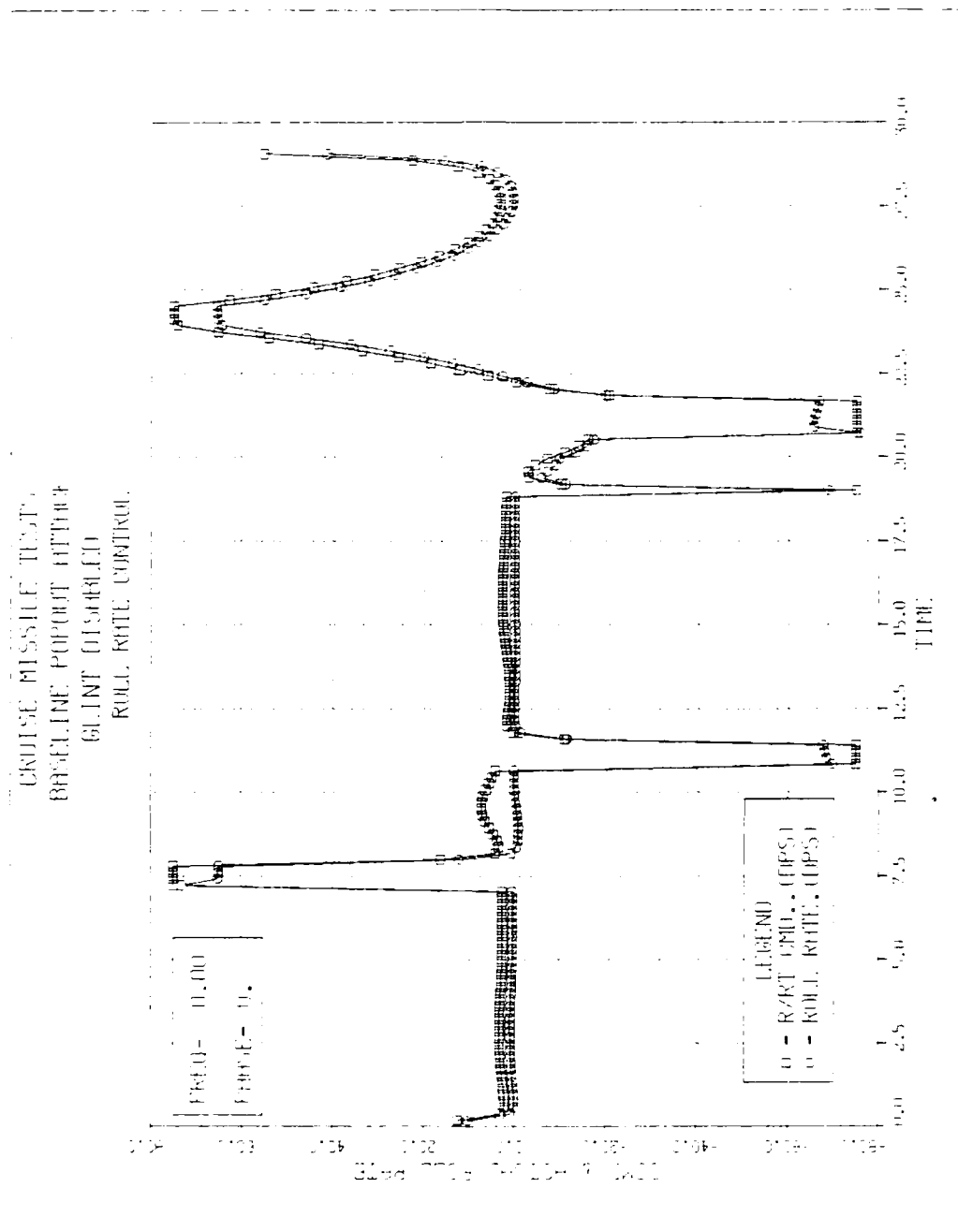


Figure A.24 Baseline - no ECM or GLINT - Roll Rate.

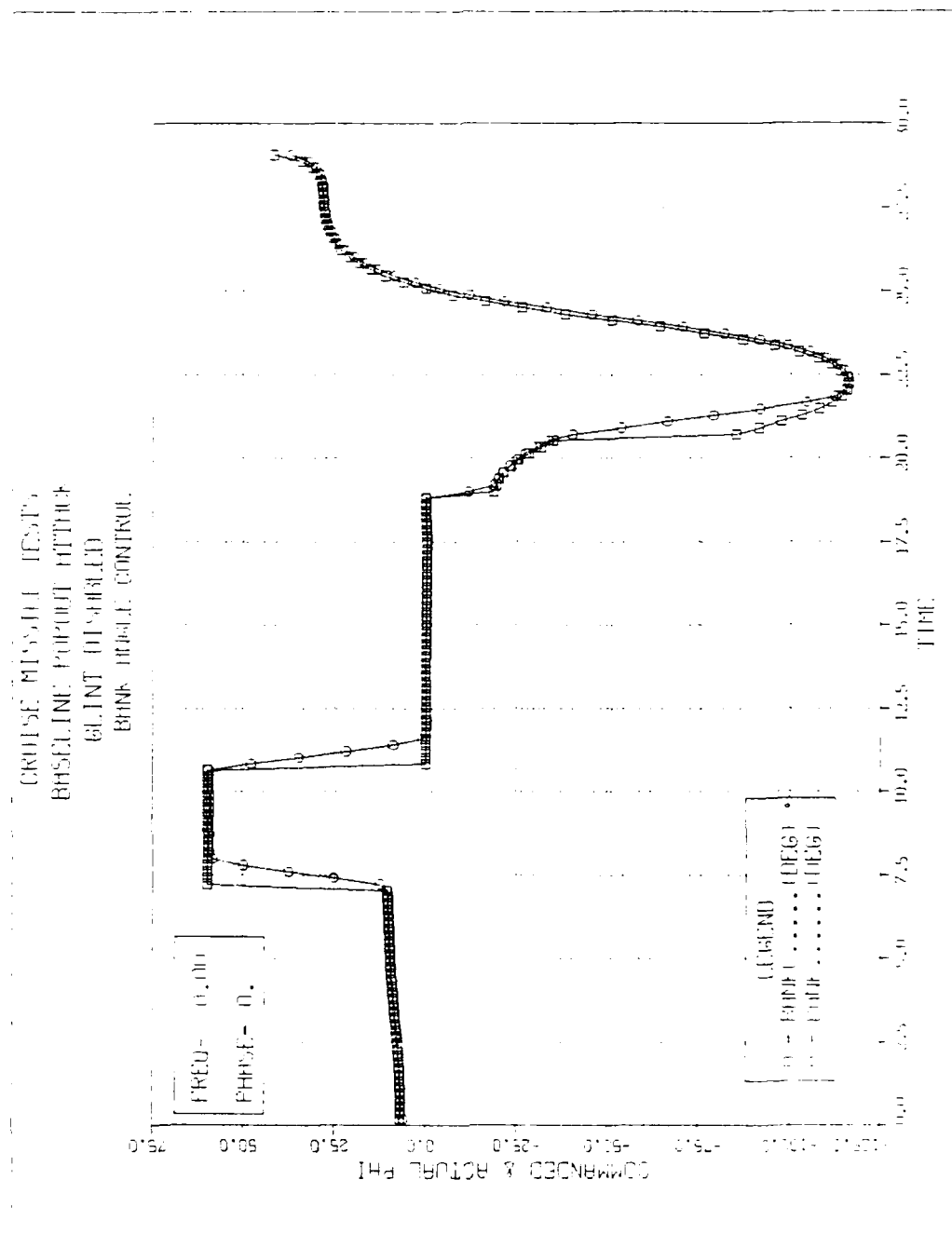


Figure A.25 Baseline - no ECM or GLINT - Bank.

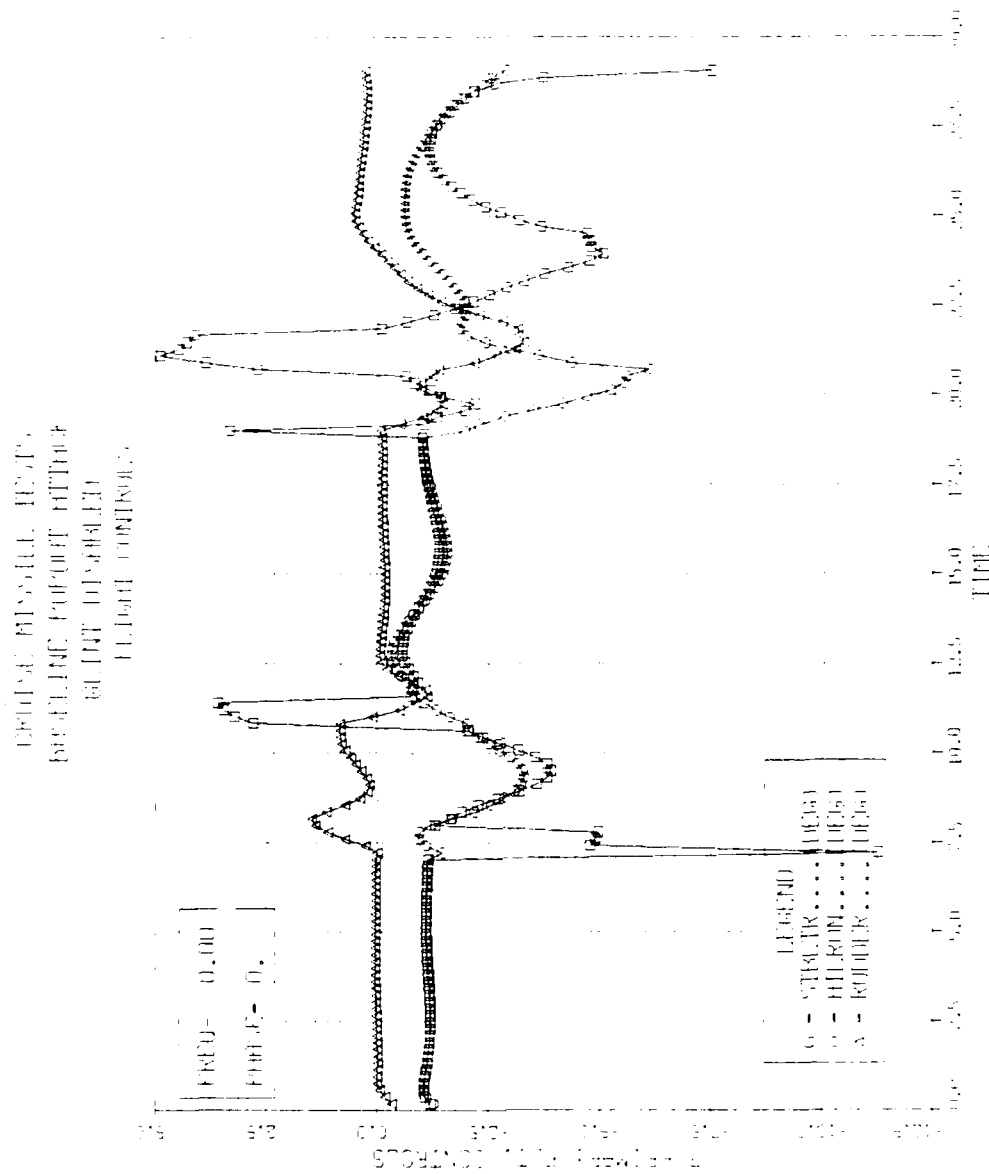


Figure A.26 Baseline - no ECM or GLINT - Controls.

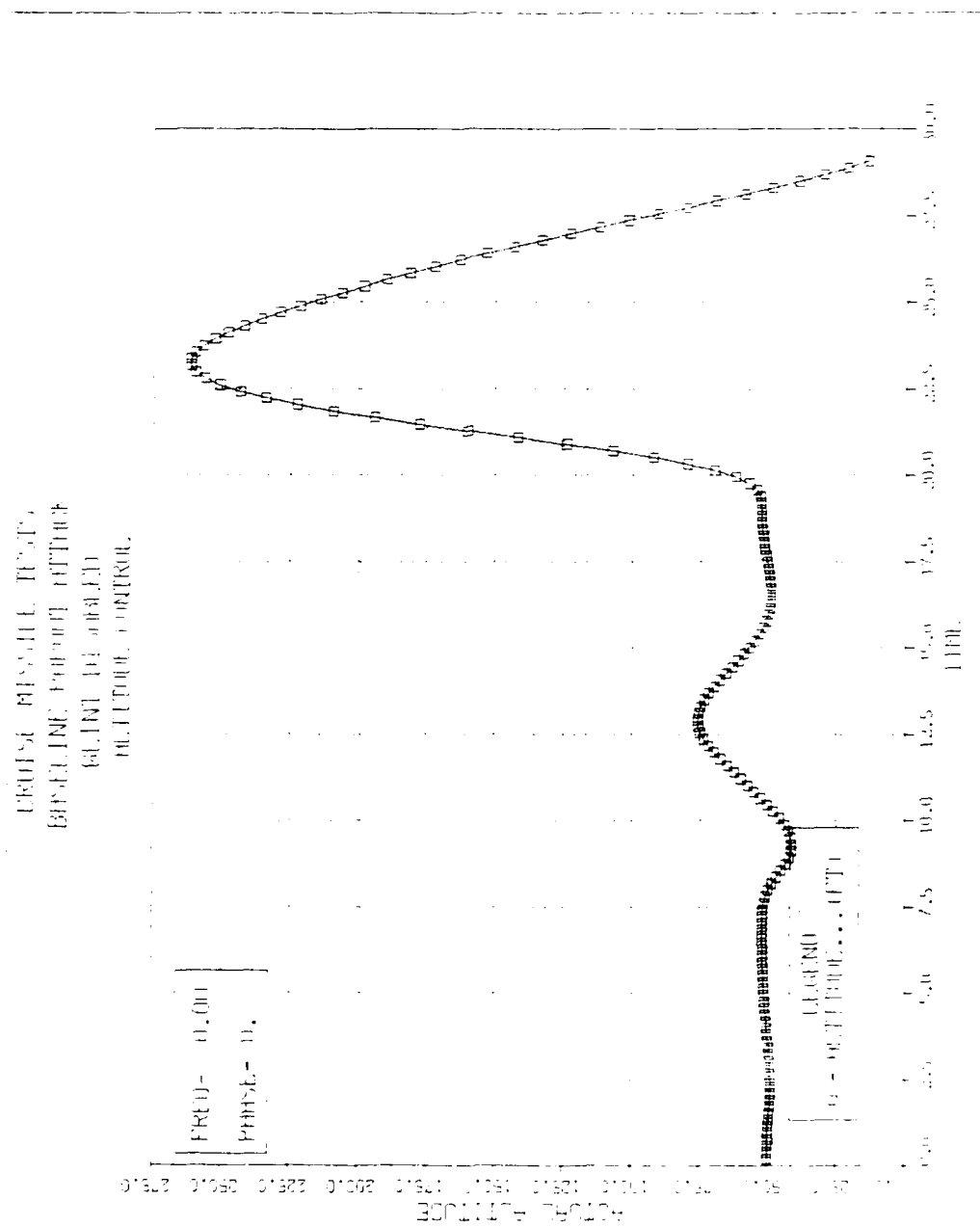
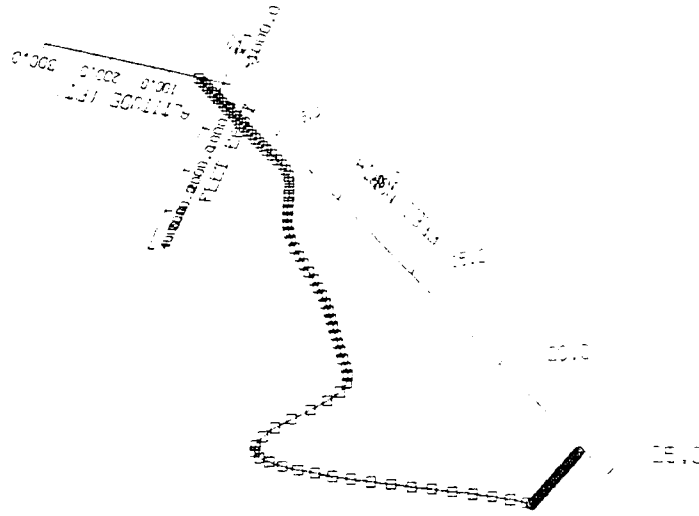
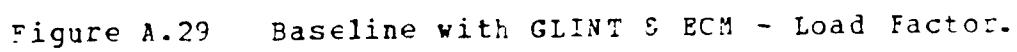


Figure A.27 Baseline - no ECM or GLINT - Altitude.

[illegible]

65



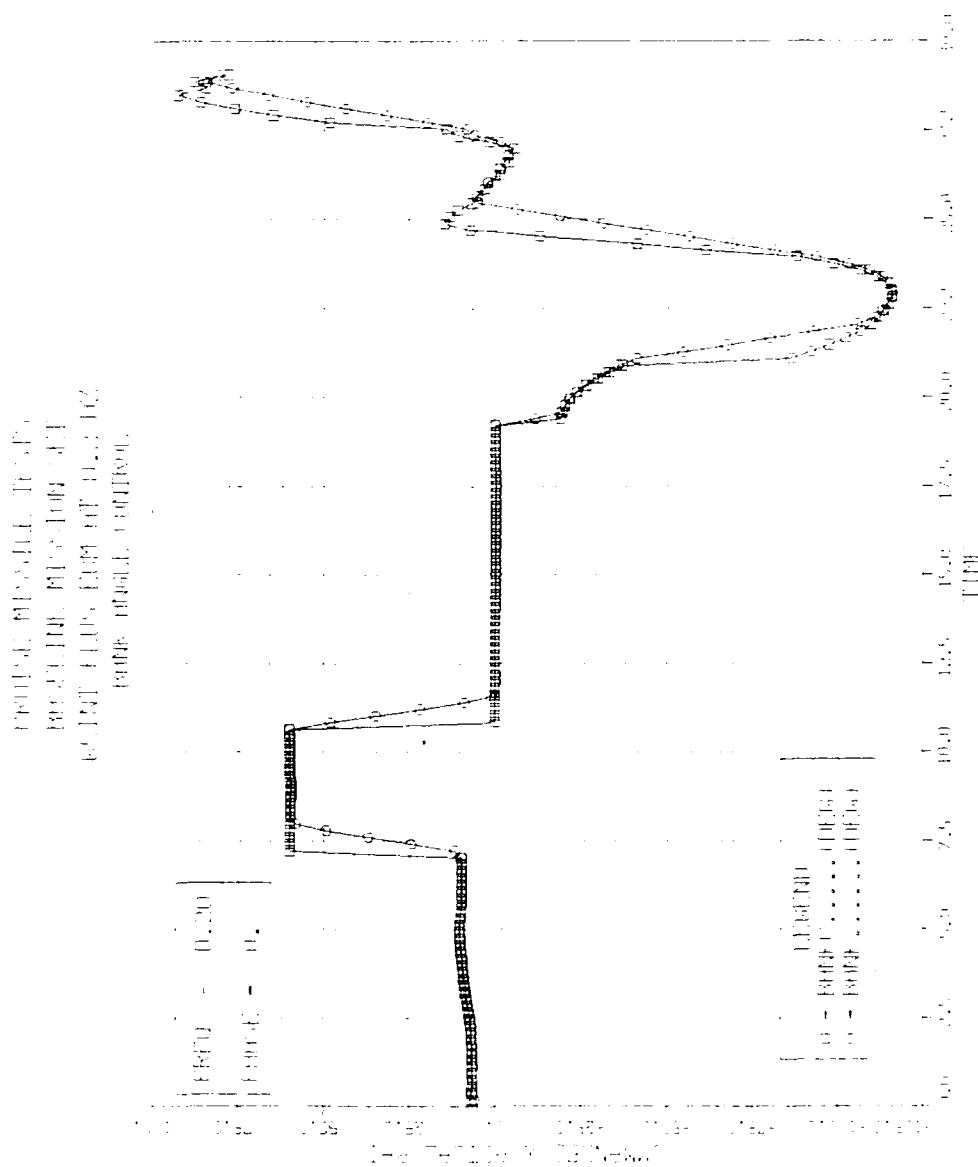


Figure A.30 Baseline with GLINT & ECM - Bank.

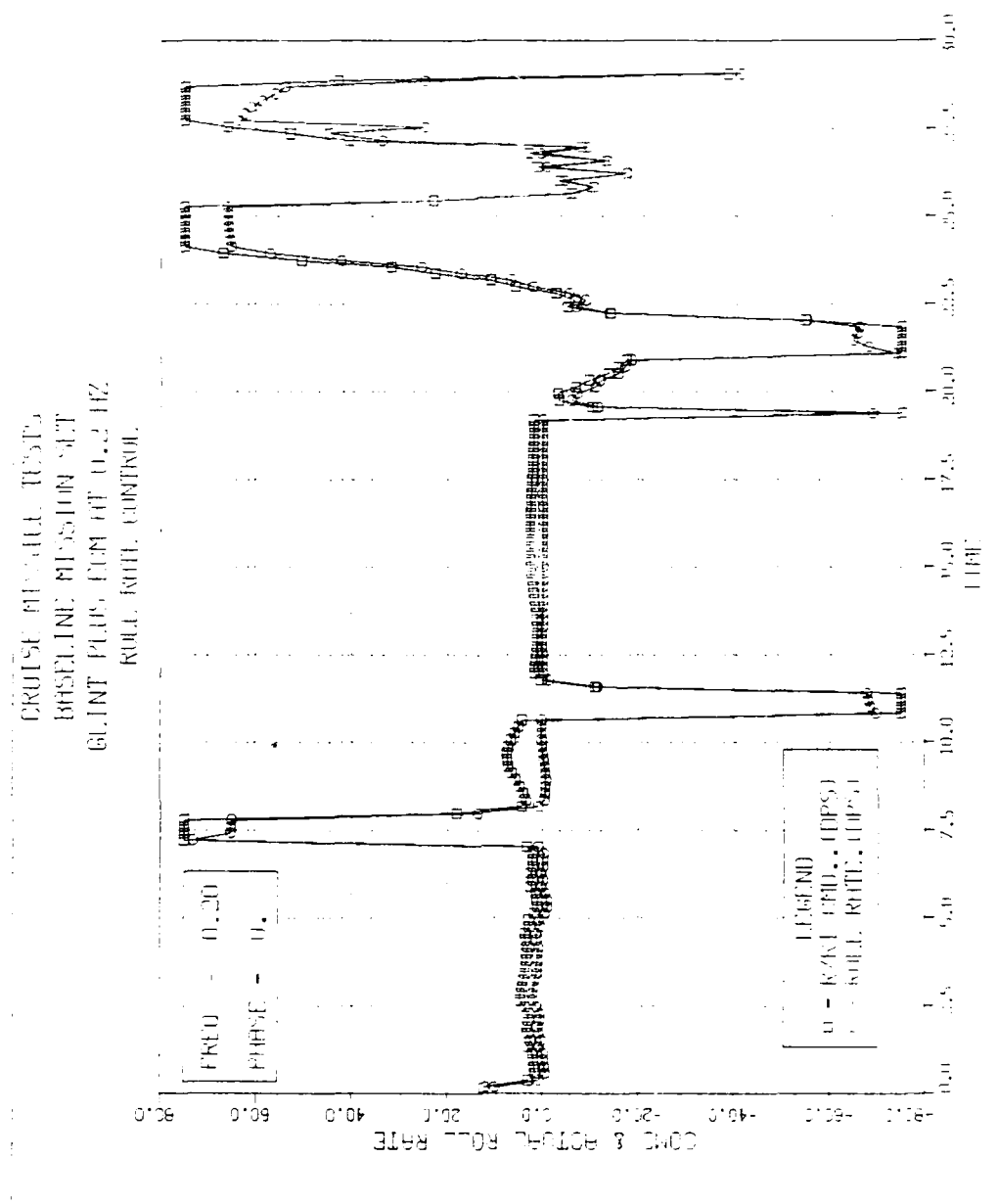


Figure A.31 Baseline with GLINT & ECM - Roll Rate.

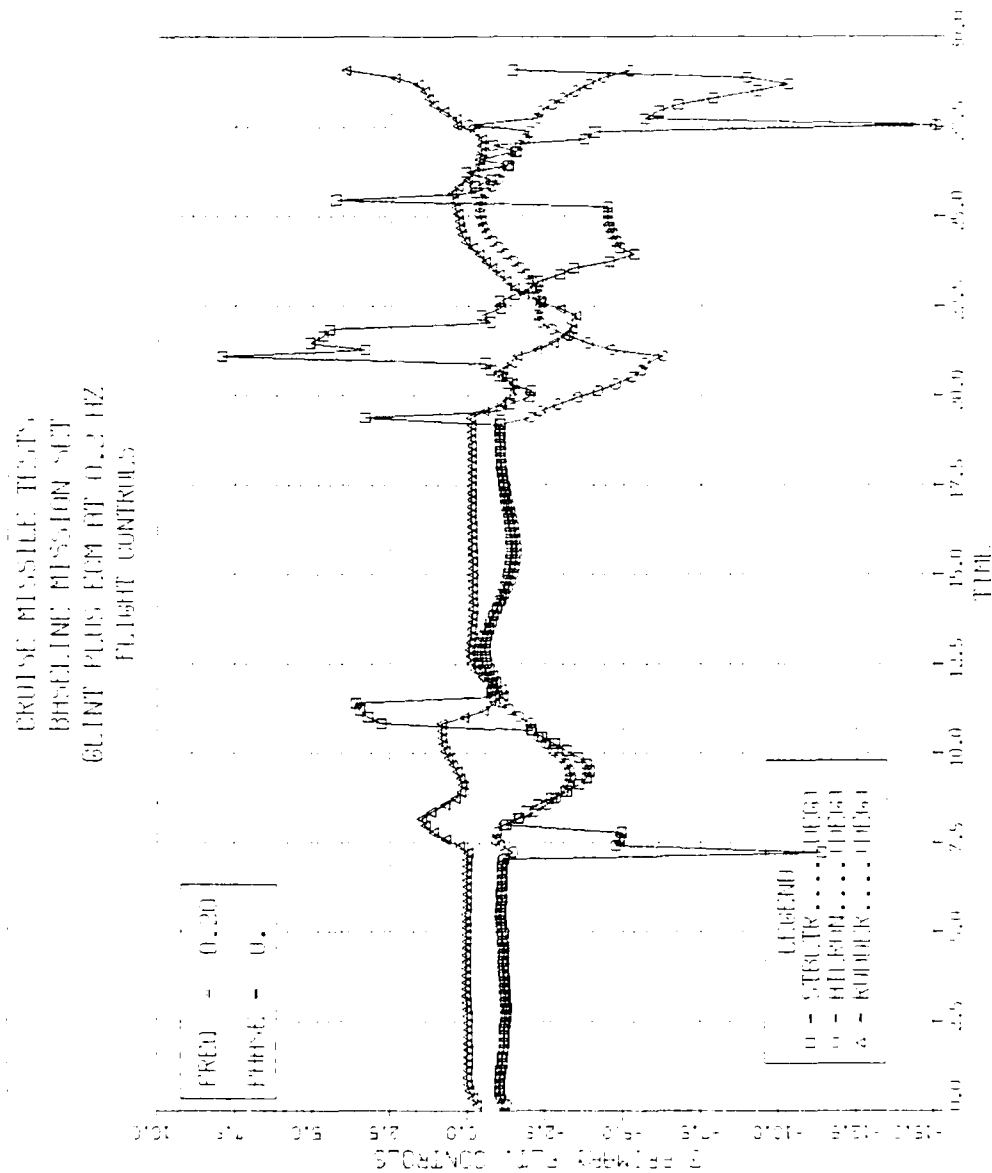


Figure A.32 Baseline with GLINT & ECM - Controls.

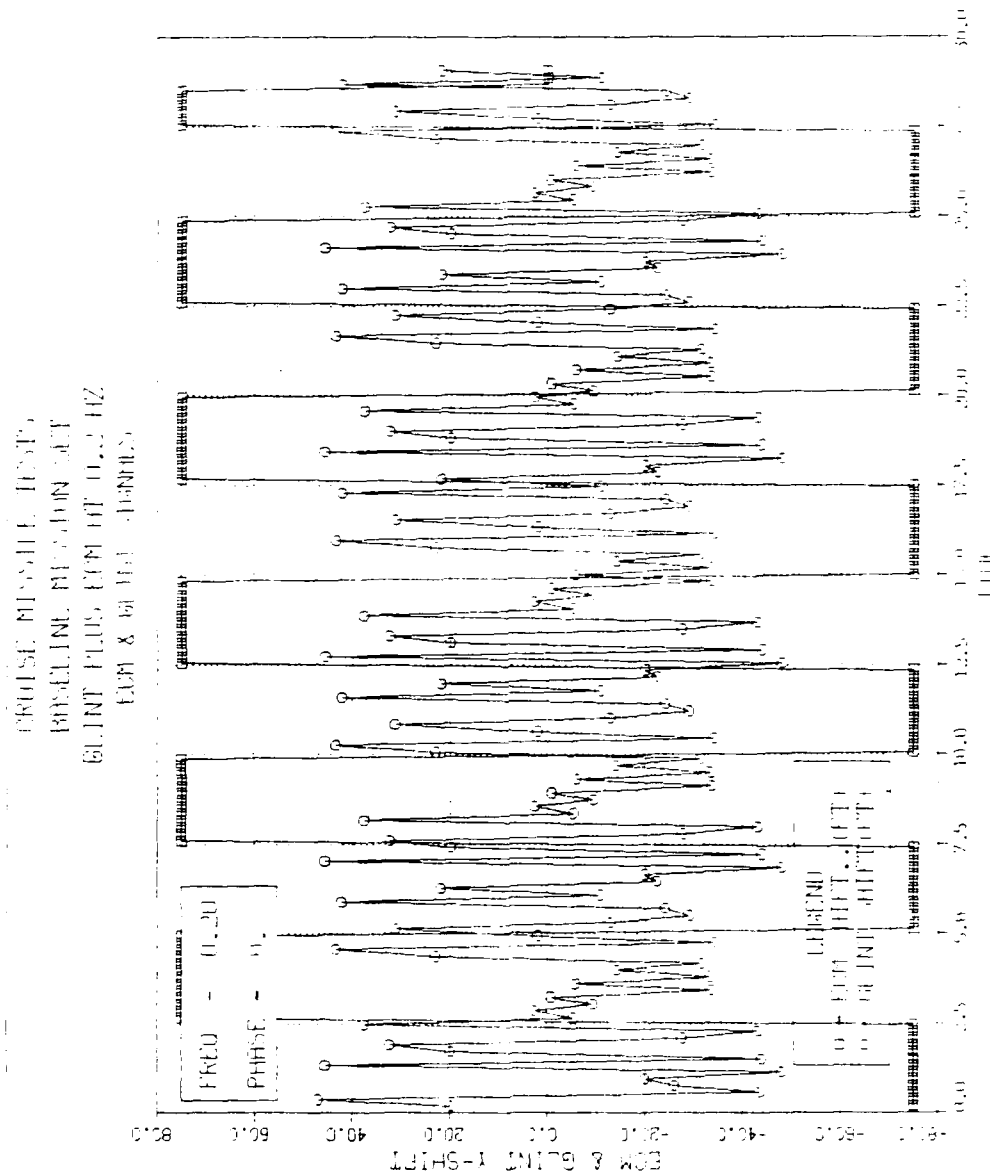


Figure A.33 Baseline with GLINT & ECM - ECM & GLINT.

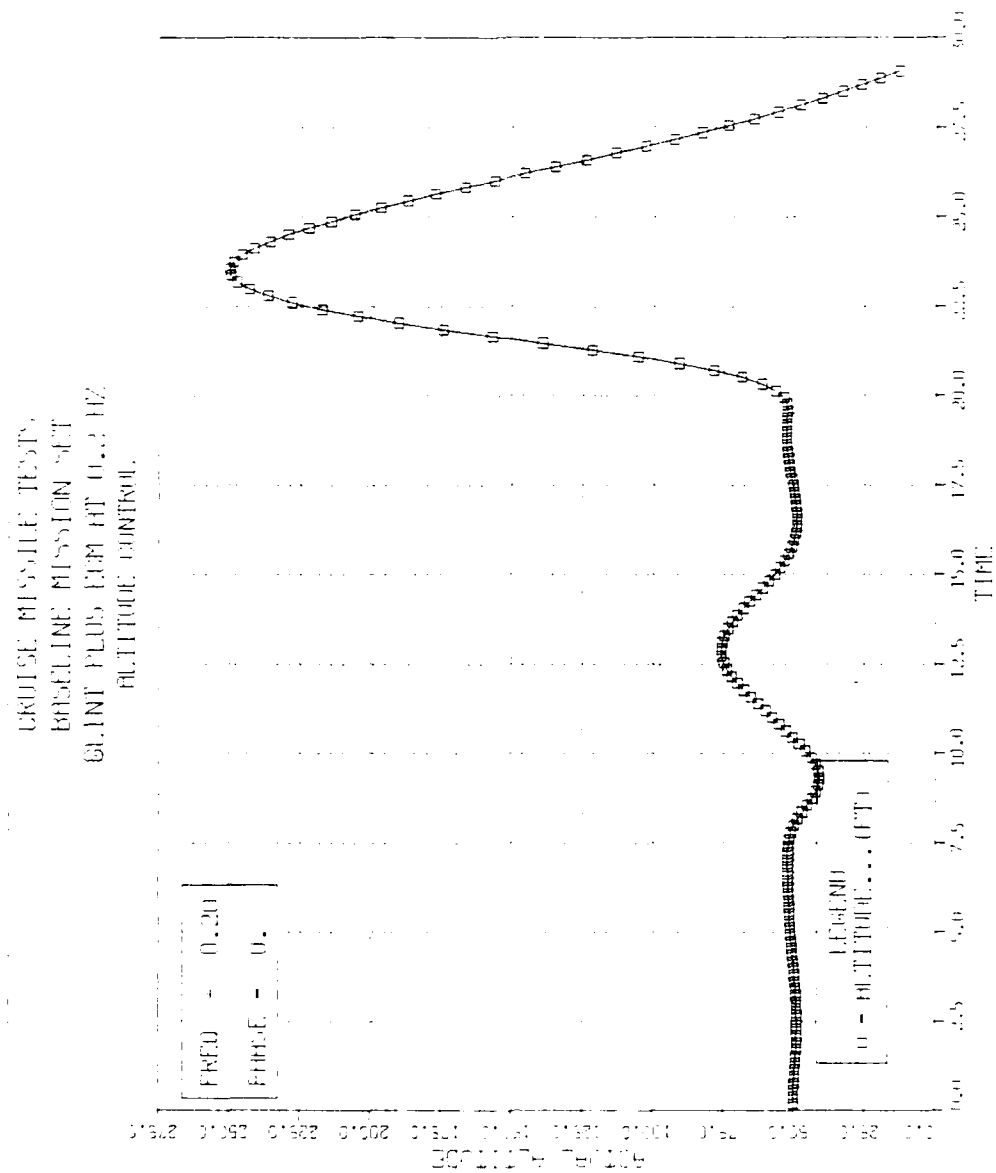


Figure A.34 Baseline with GLINT & ECM - Altitude.

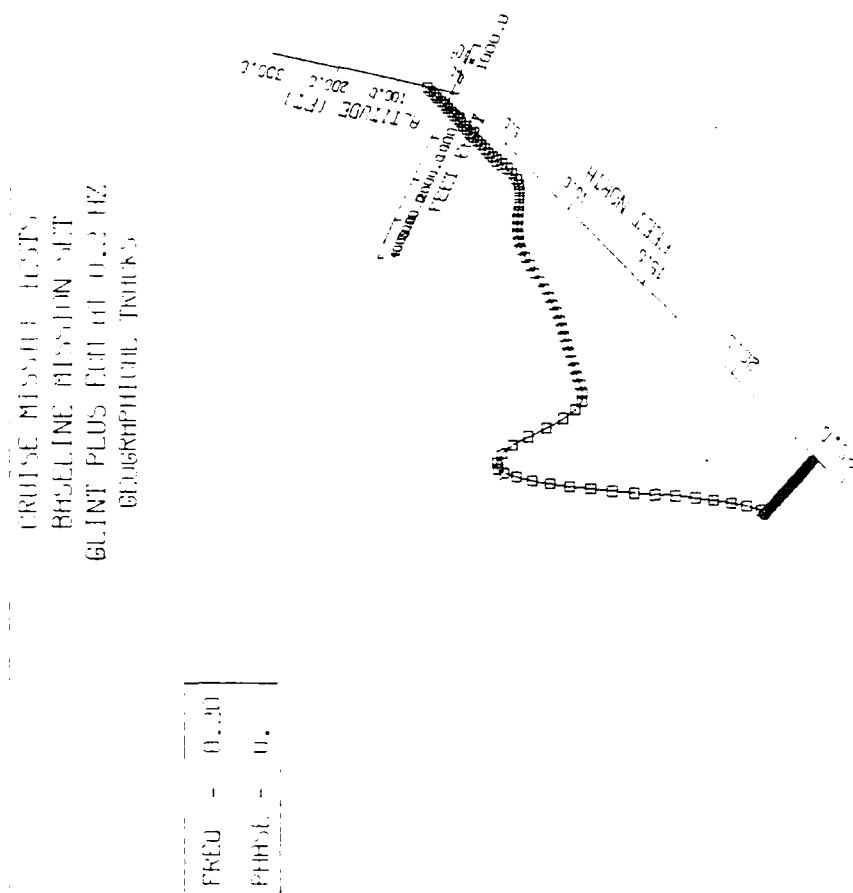


Figure A.35 Baseline with GLINT & ECM - Geo Plot.

BASELINE SCAN RESULTS

MISS DISTANCES

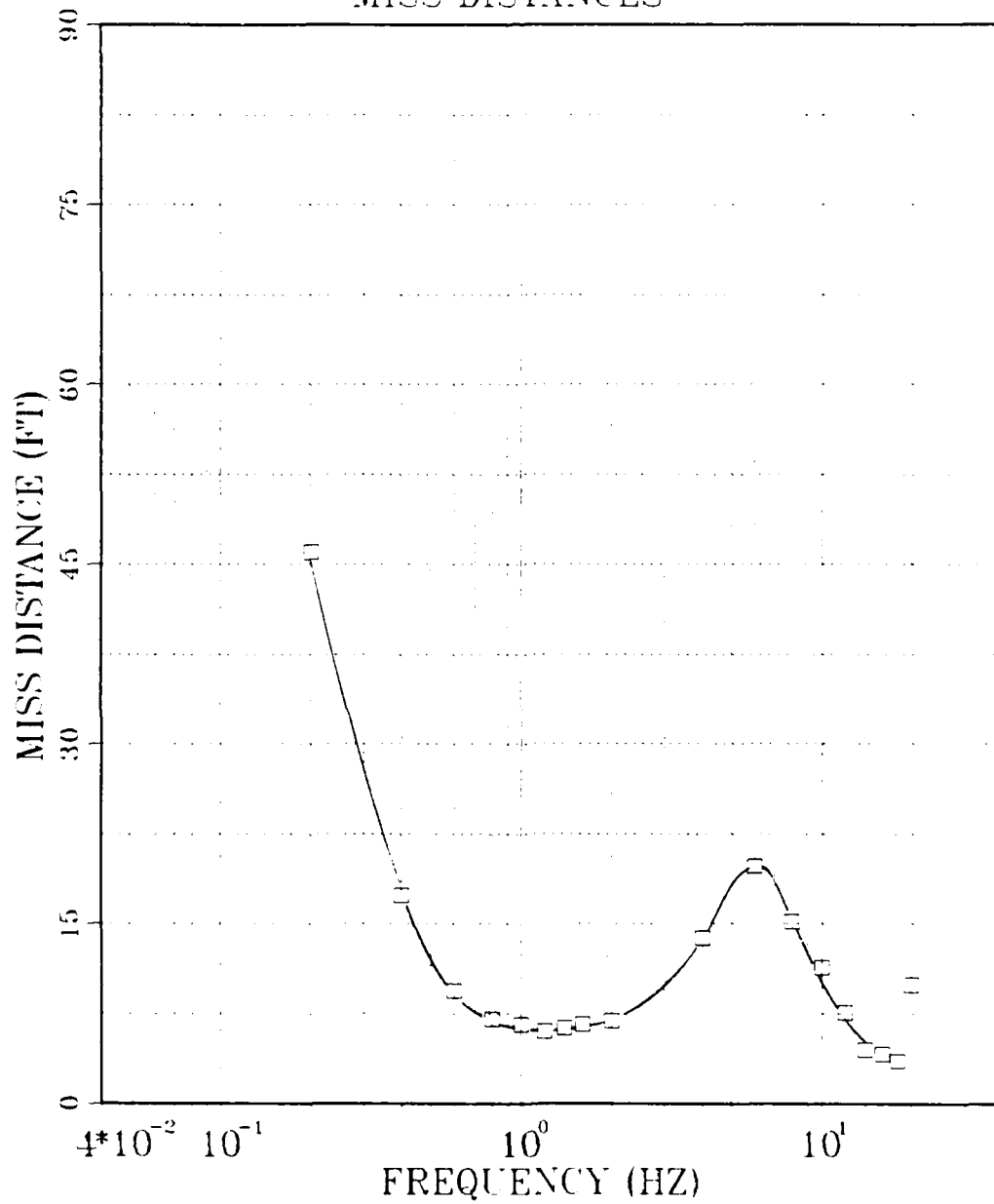


Figure A.36 Mean Miss Distances - Baseline.

CONFIGURATION II SCANS

MISS DISTANCES

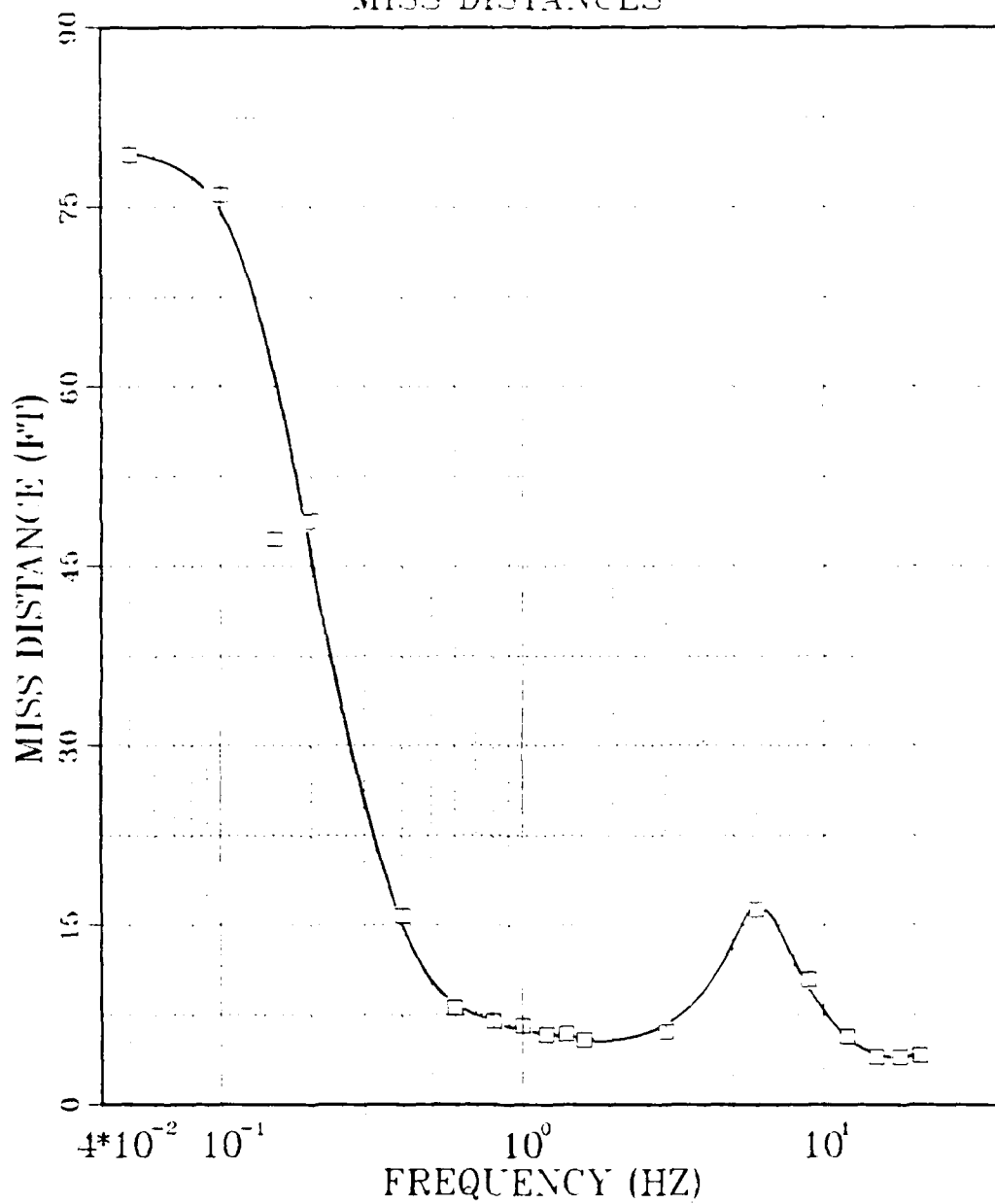


Figure A.37 Mean Miss Distances - Configuration II.

CONFIGURATION III SCANS

MISS DISTANCES

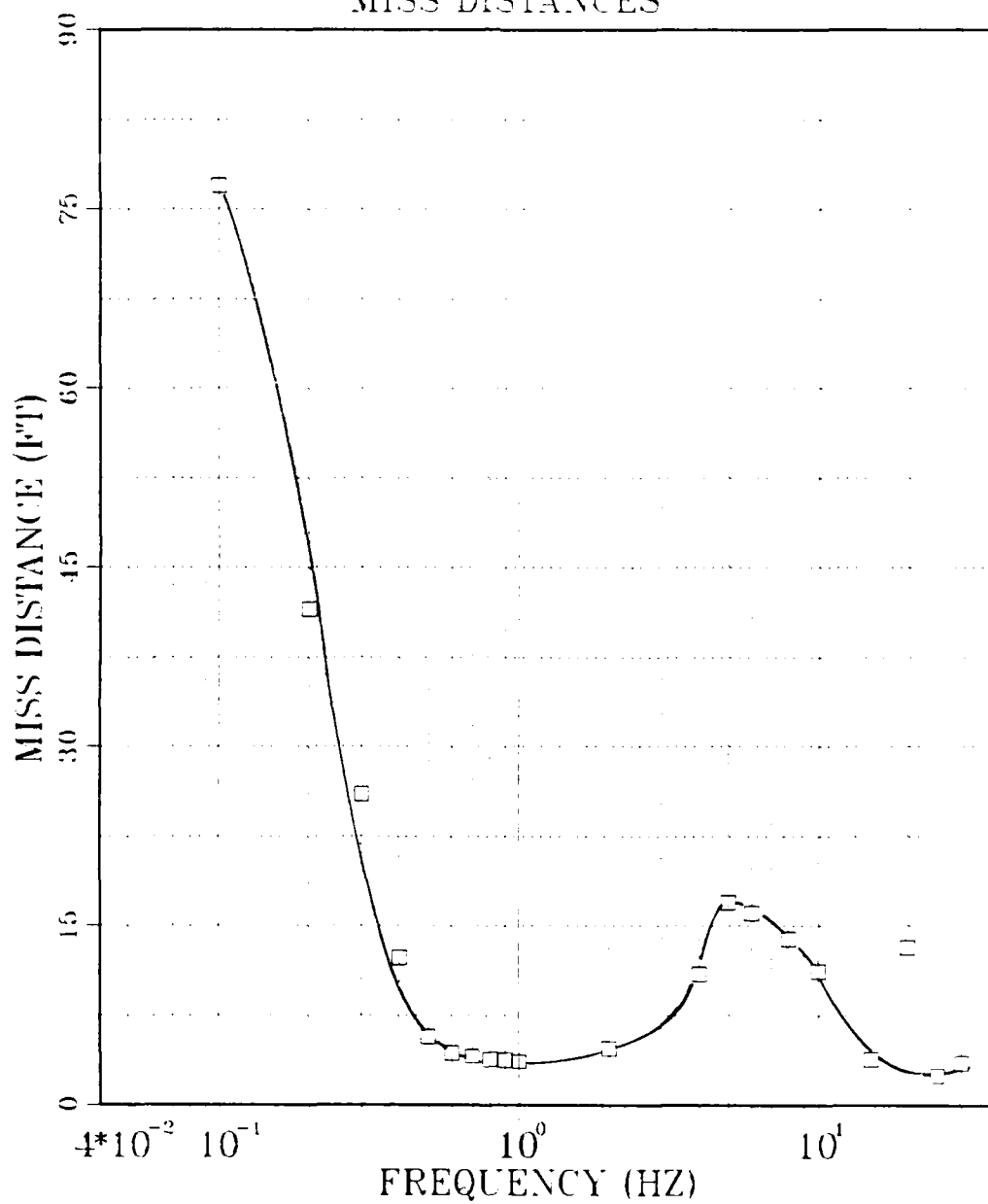


Figure A.38 Mean Miss Distances - Configuration III.

CONFIGURATION IV SCANS

MISS DISTANCES

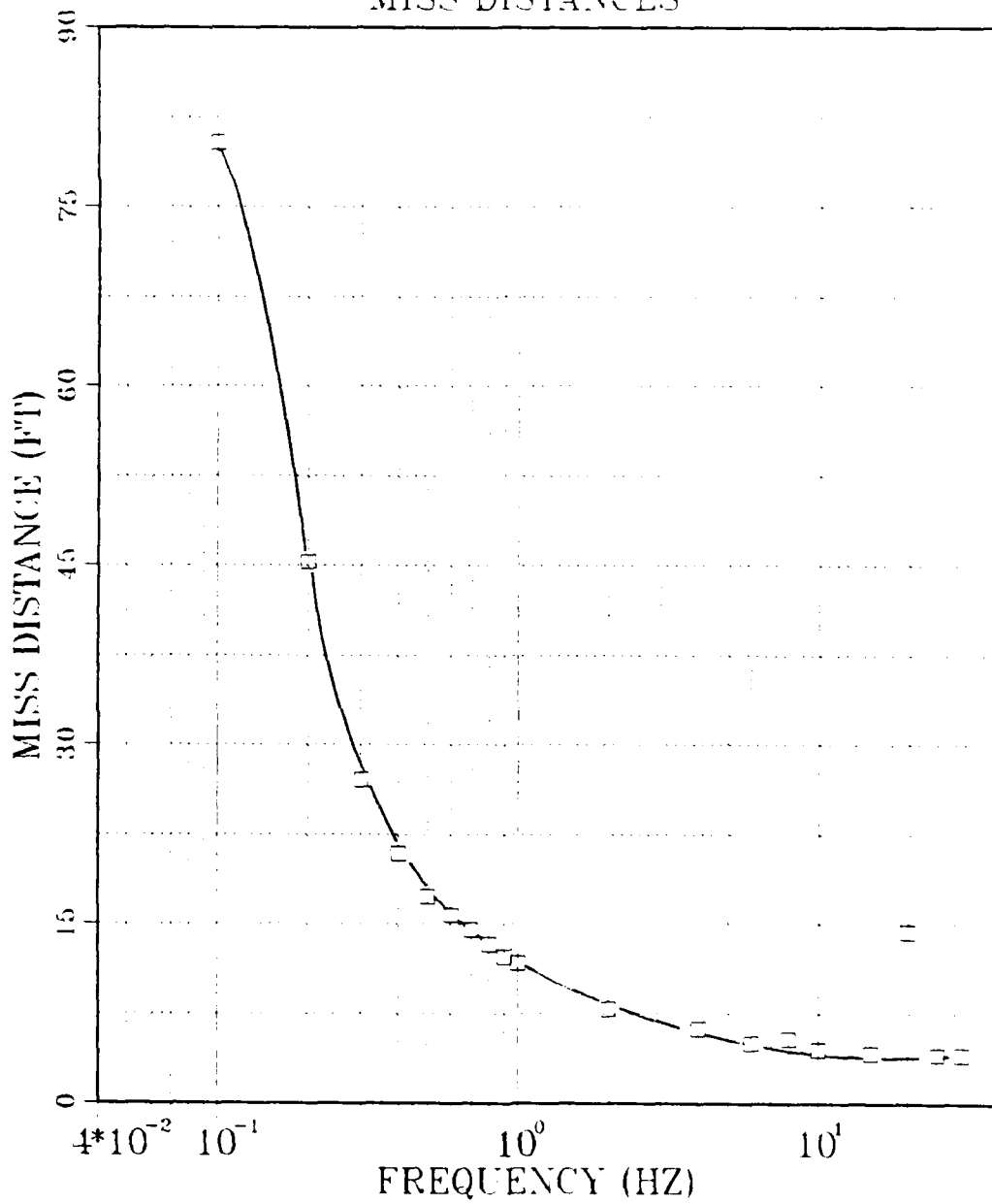


Figure A.39 Mean Miss Distances - Configuration IV.

BASELINE SCAN RESULTS

AUTOPILOT ERRORS

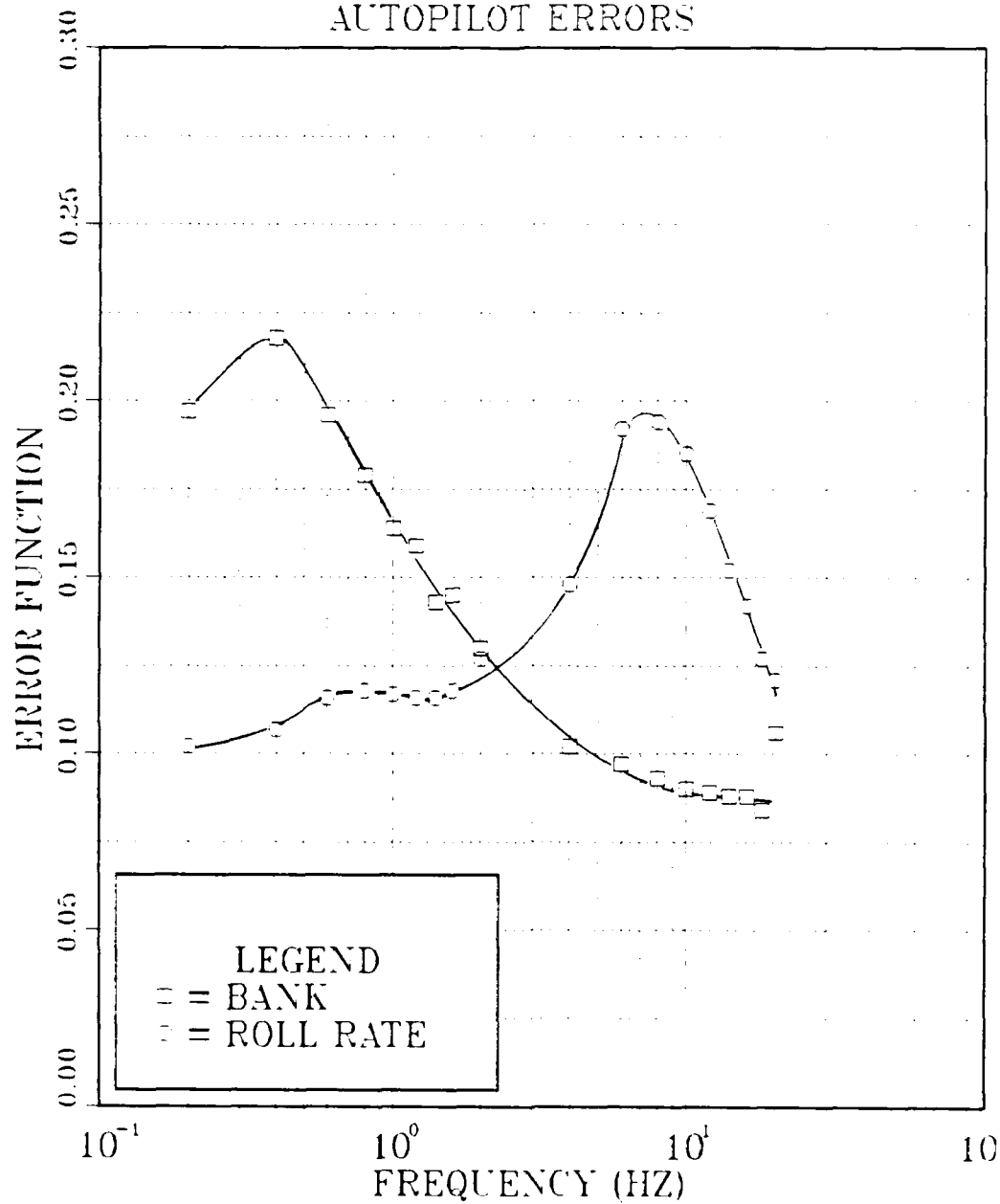


Figure A.40 Autopilot Errors - Paseline.

CONFIGURATION II SCANS

AUTOPILOT ERRORS

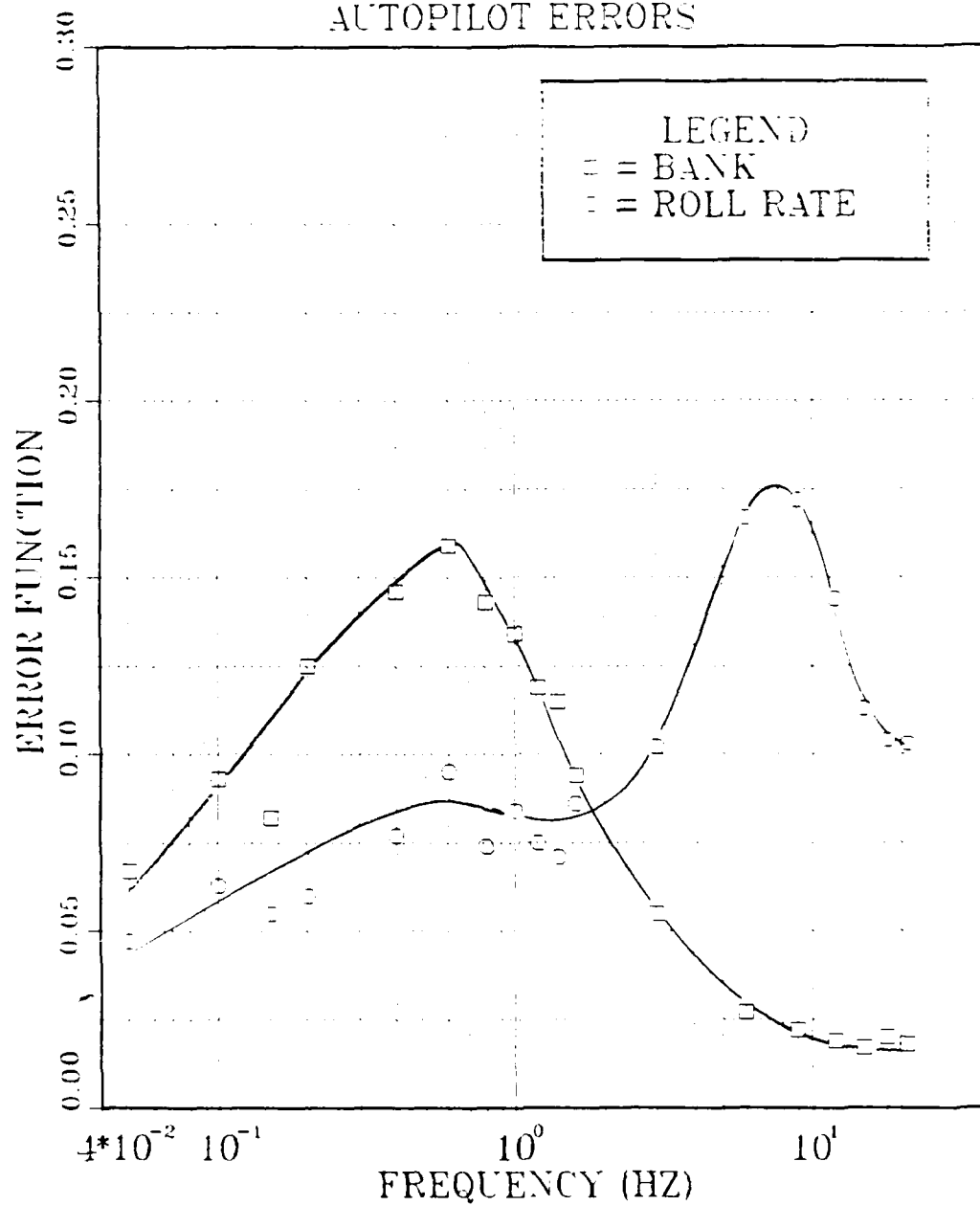


Figure A.41 Autopilot Errors - Configuration II.

CONFIGURATION III SCANS

AUTOPILOT ERRORS

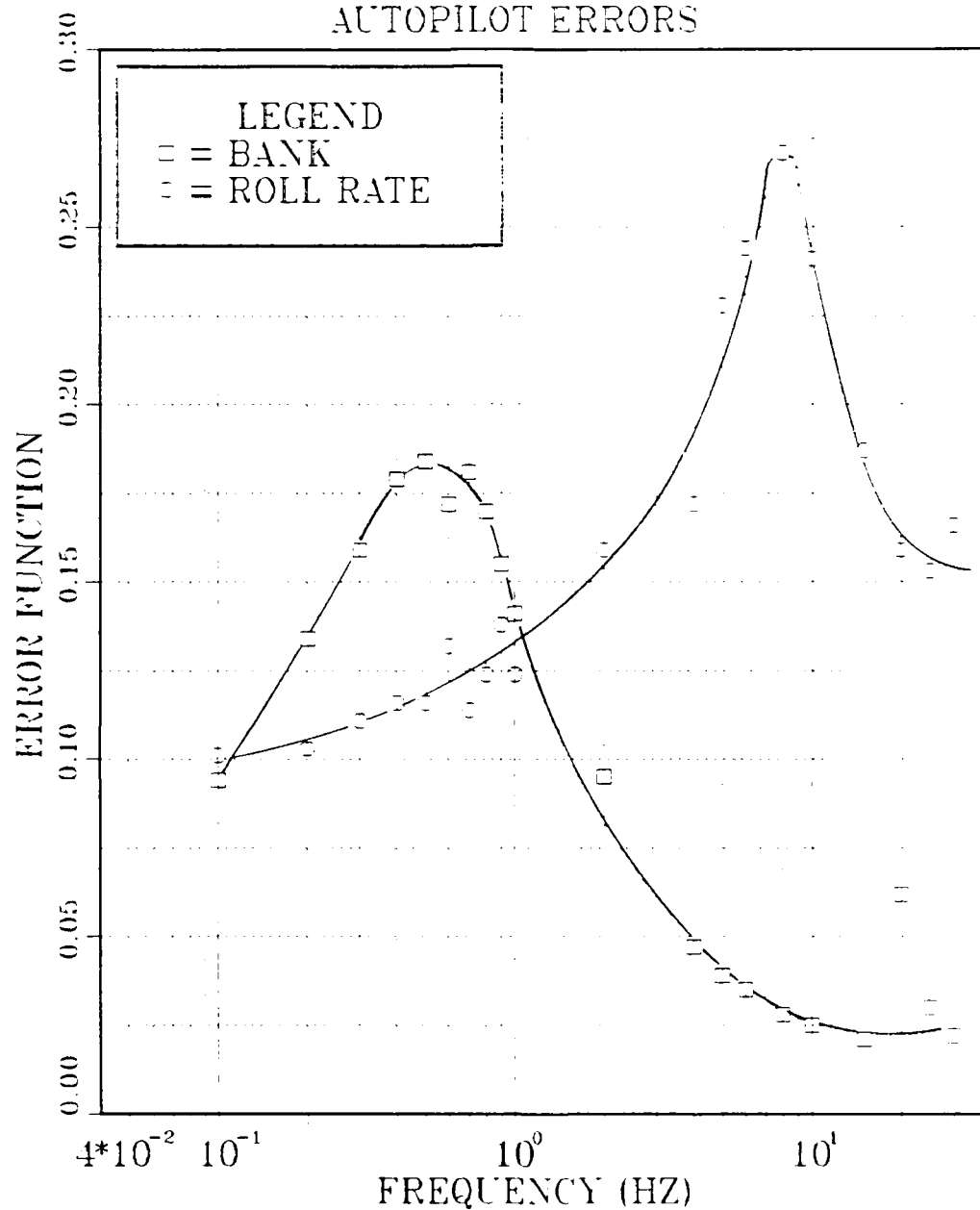


Figure A.42 Autopilot Errors - Configuration III.

CONFIGURATION IV SCANS

AUTOPILOT ERRORS

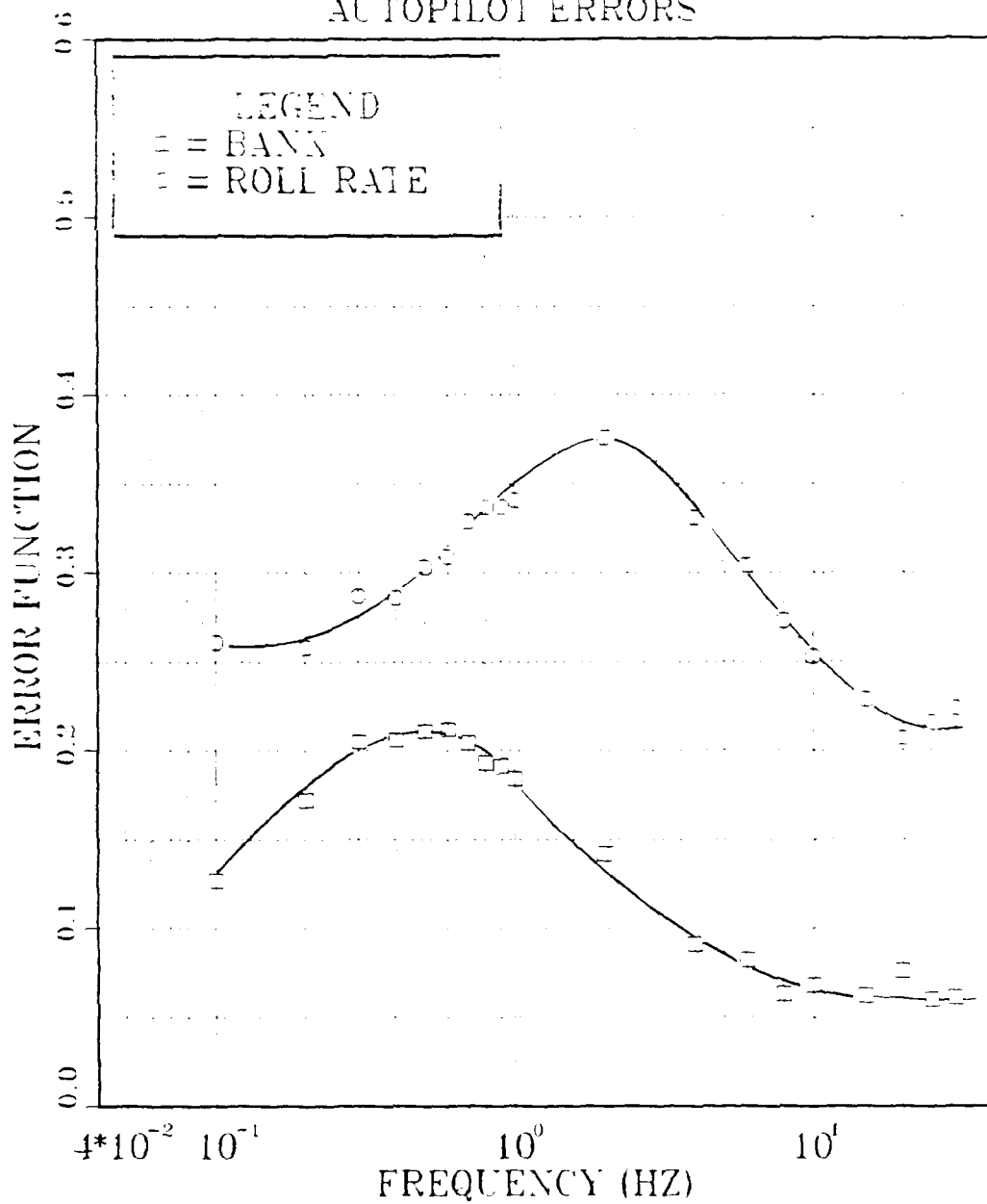


Figure A.43 Autopilot Errors - Configuration IV.

BASELINE SCAN RESULTS

TRACKING ERRORS

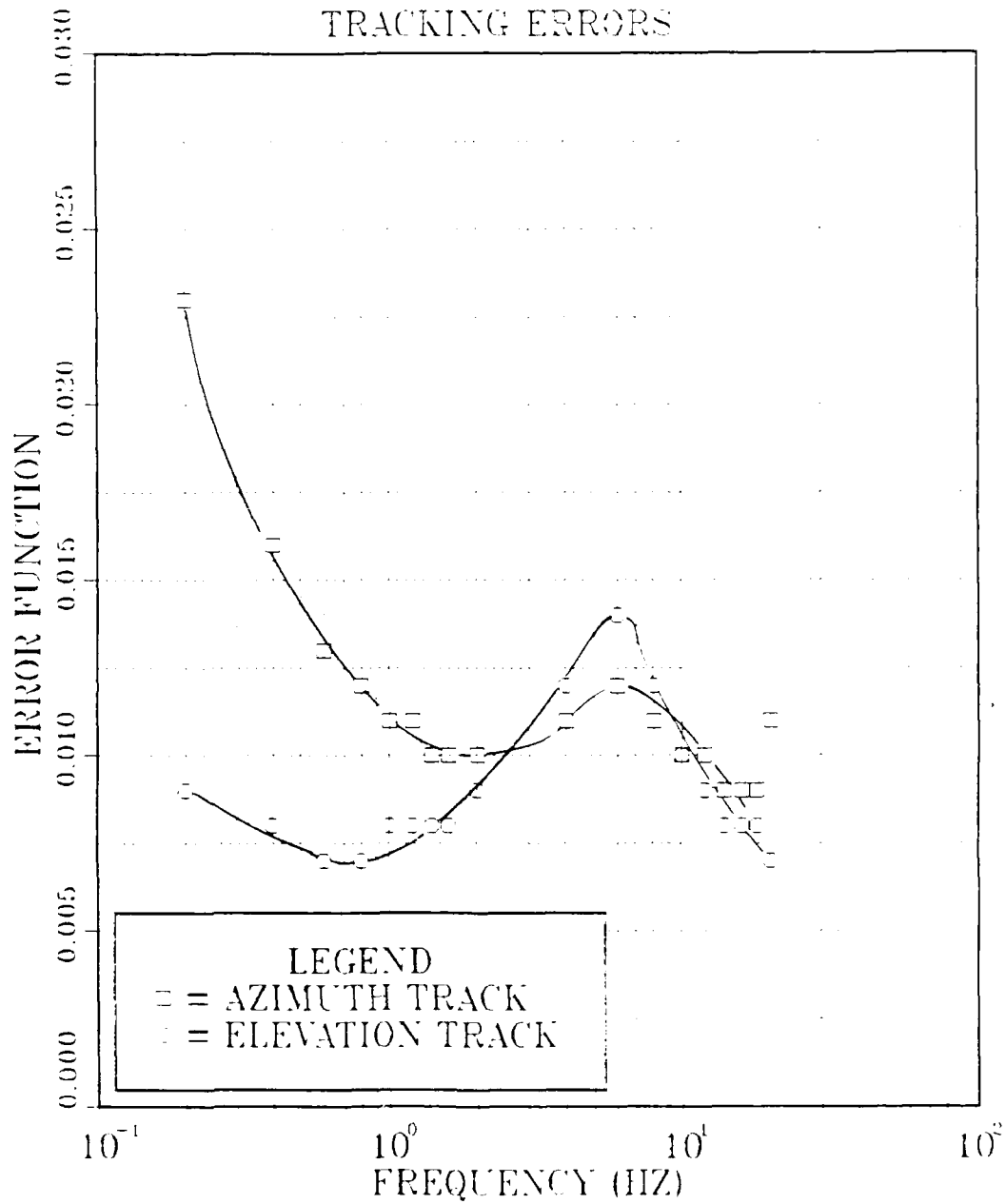


Figure A.44 Tracking Errors - Baseline.

CONFIGURATION II SCANS

TRACKING ERRORS

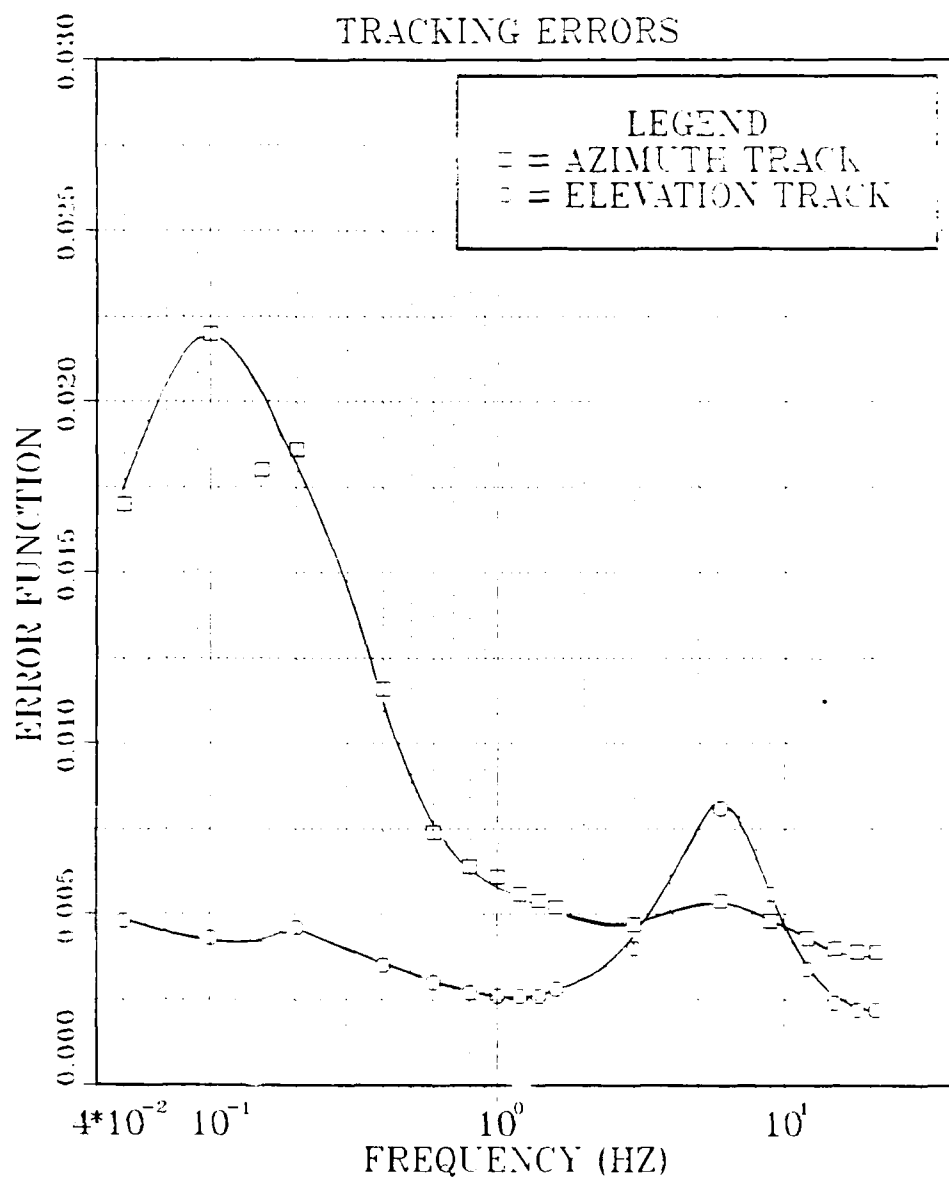


Figure A.45 Tracking Errors - Configuration II.

CONFIGURATION III SCANS

TRACKING ERRORS

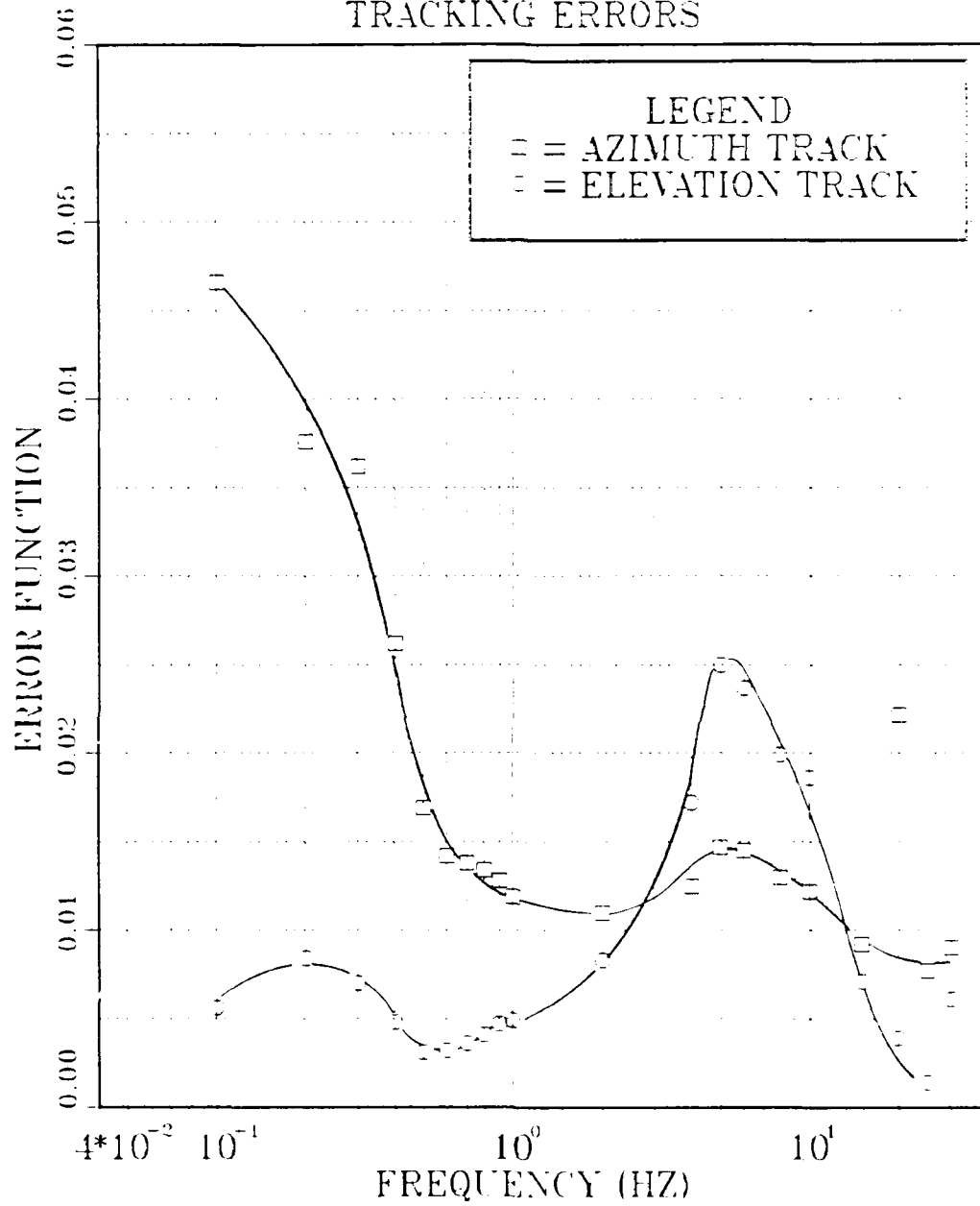


Figure A.46 Tracking Errors - Configuration III.

CONFIGURATION IV SCANS

TRACKING ERRORS

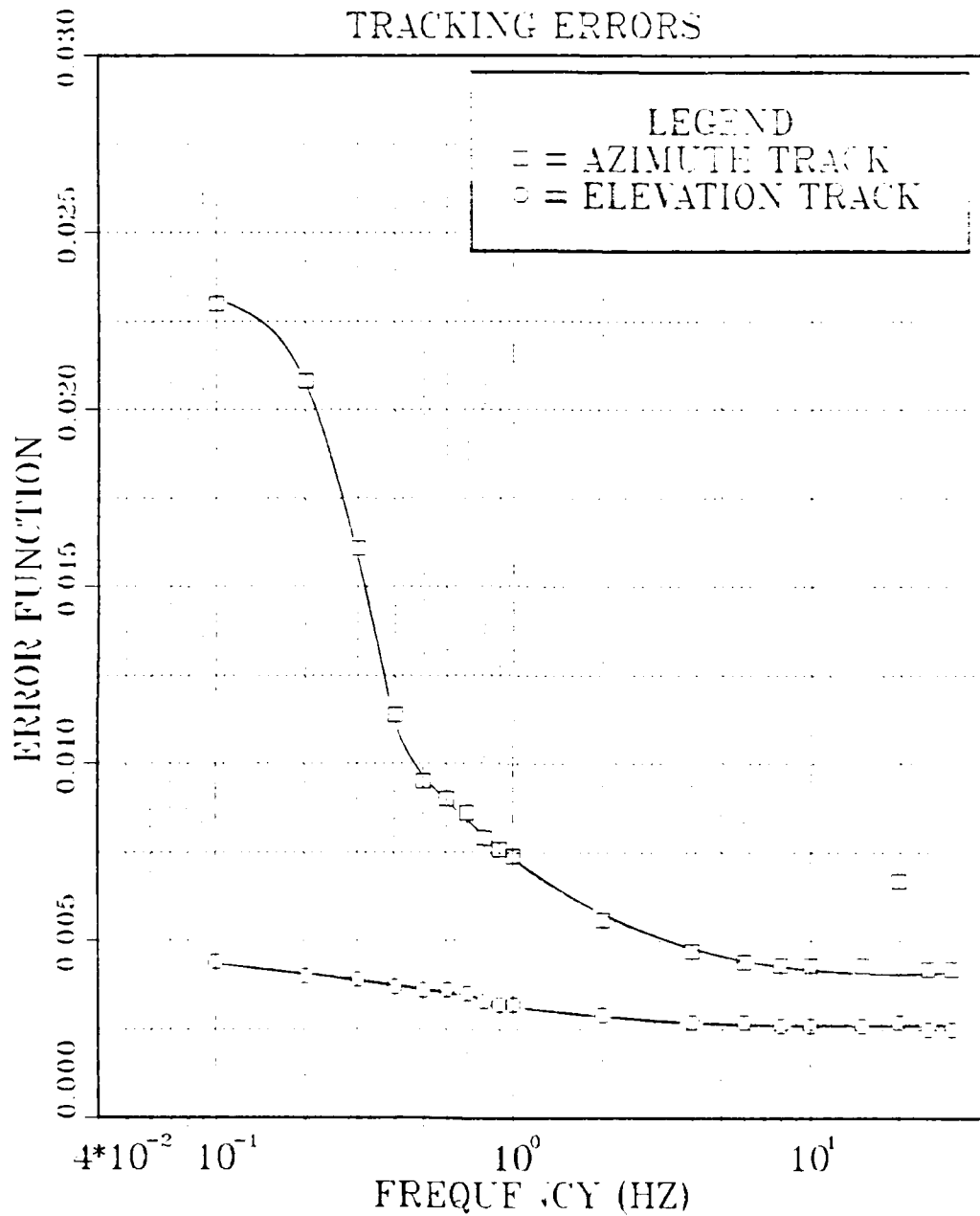


Figure A.47 Tracking Errors - Configuration IV.

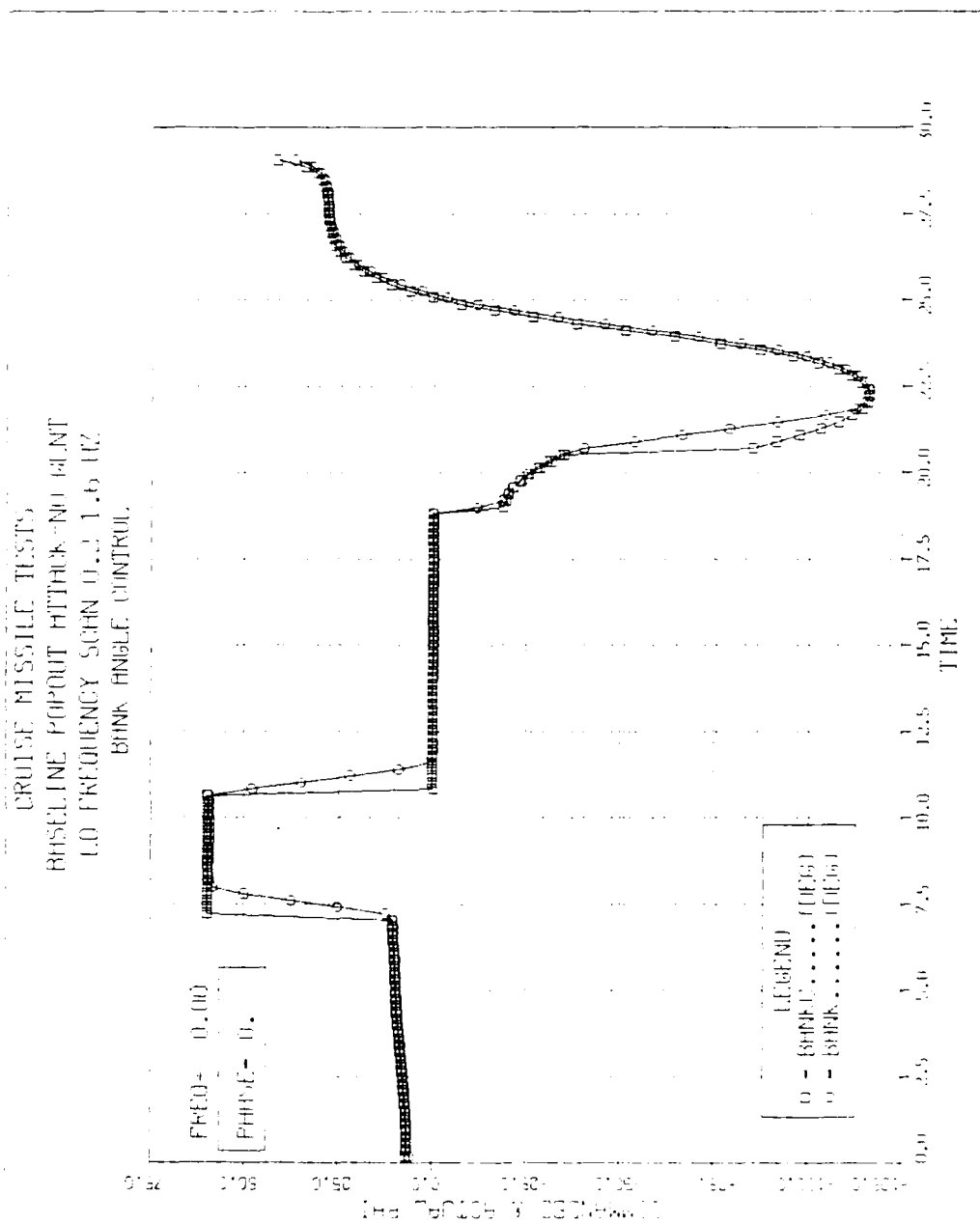


Figure A.48 Baseline/ECM Preq = 0.0 Hz - Bank.

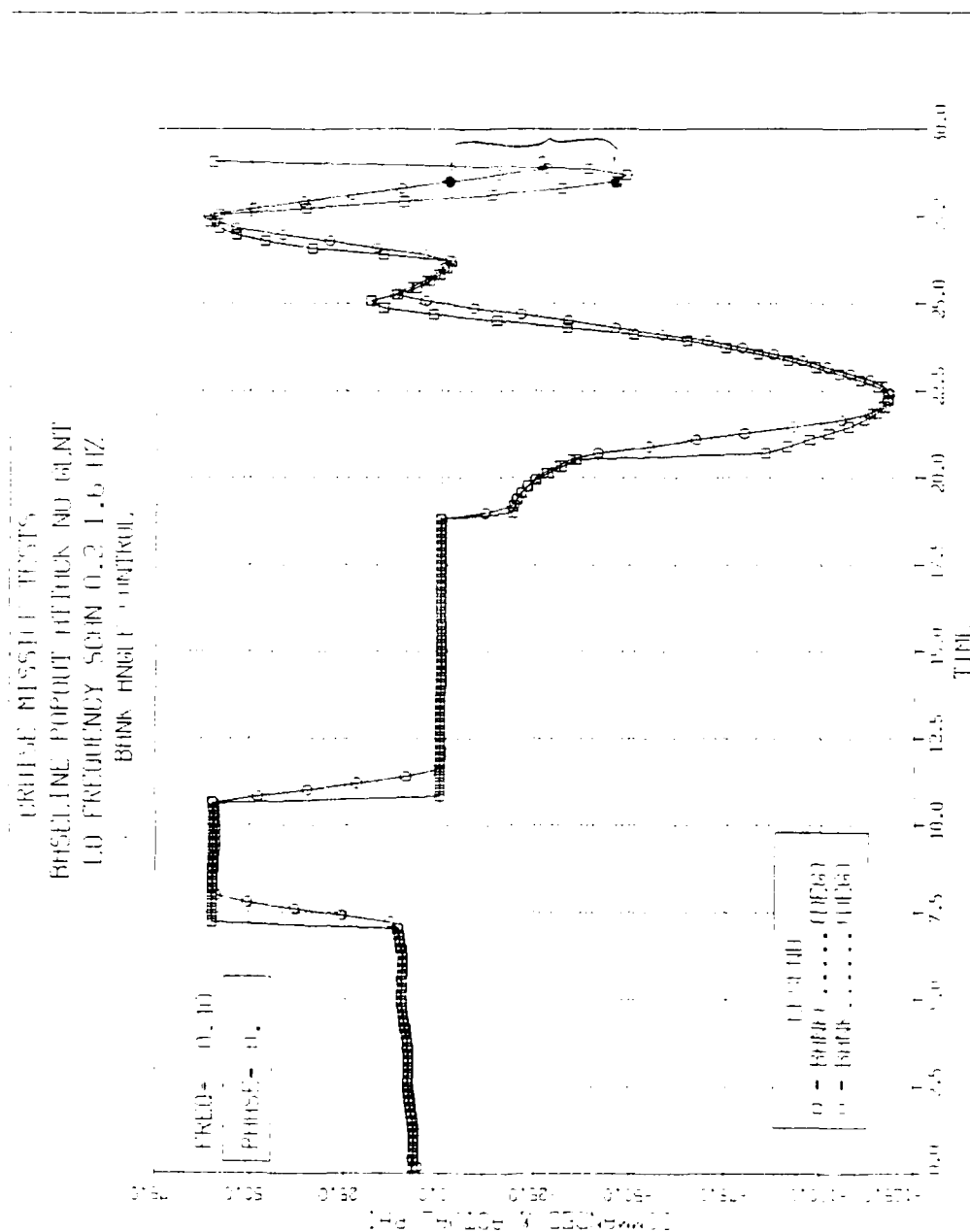


Figure A.49 Baseline/ECM Freq = 0.4 Hz - Bank.

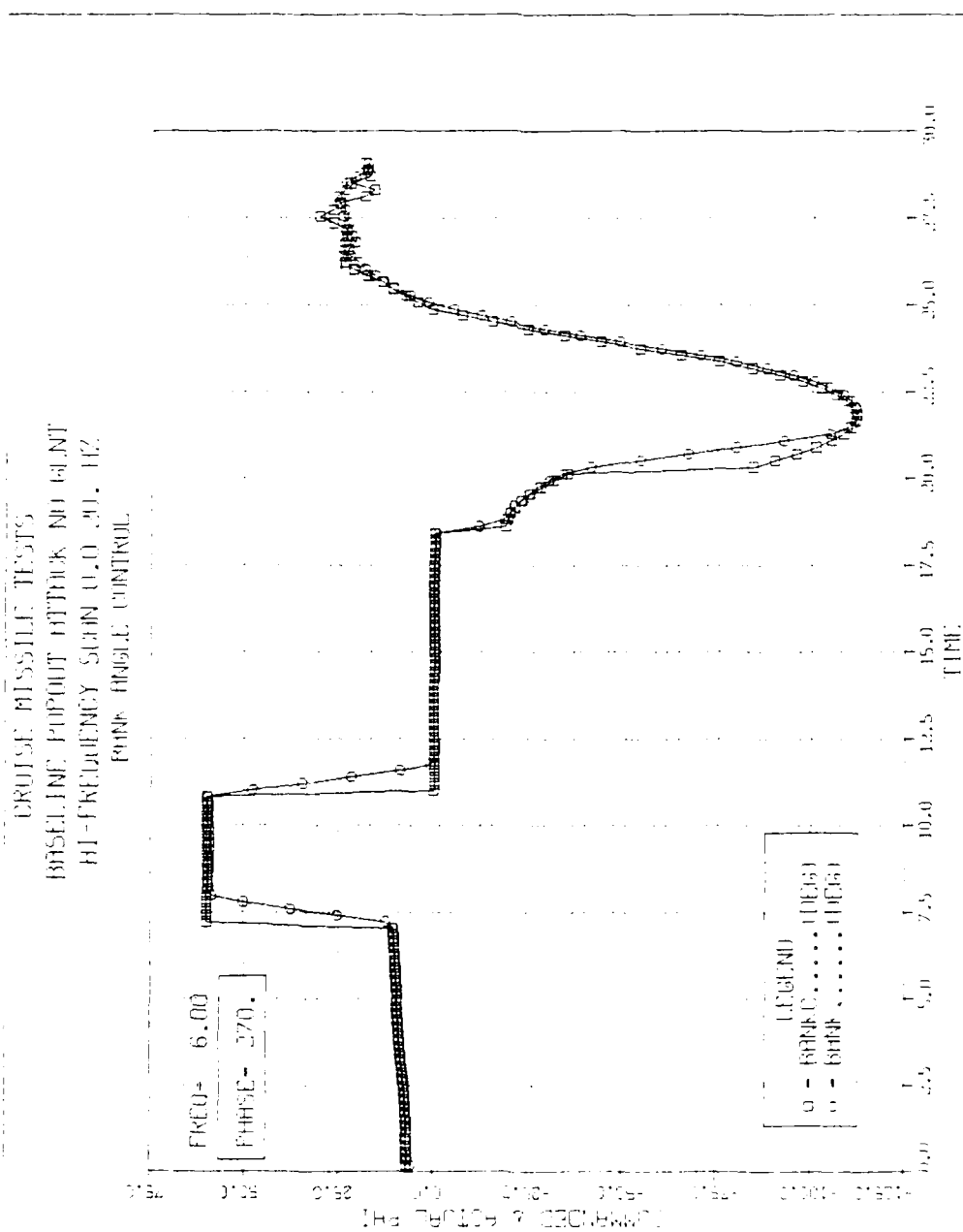


Figure A.50 Baseline/ECM Freq = 6.0 Hz - Bank.

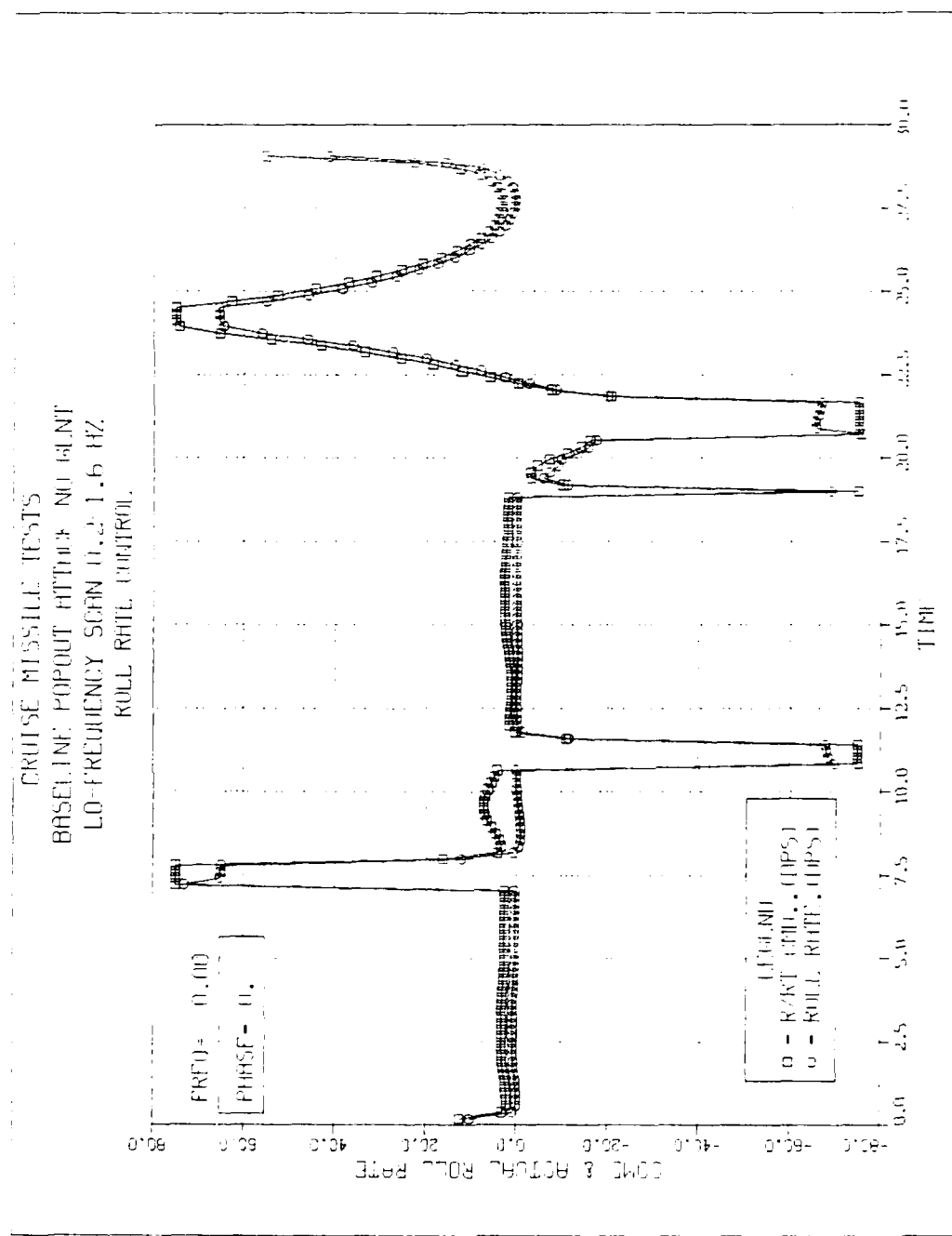


Figure A.51 Baseline/ECM Freq = 0.0 Hz - Roll Rate.

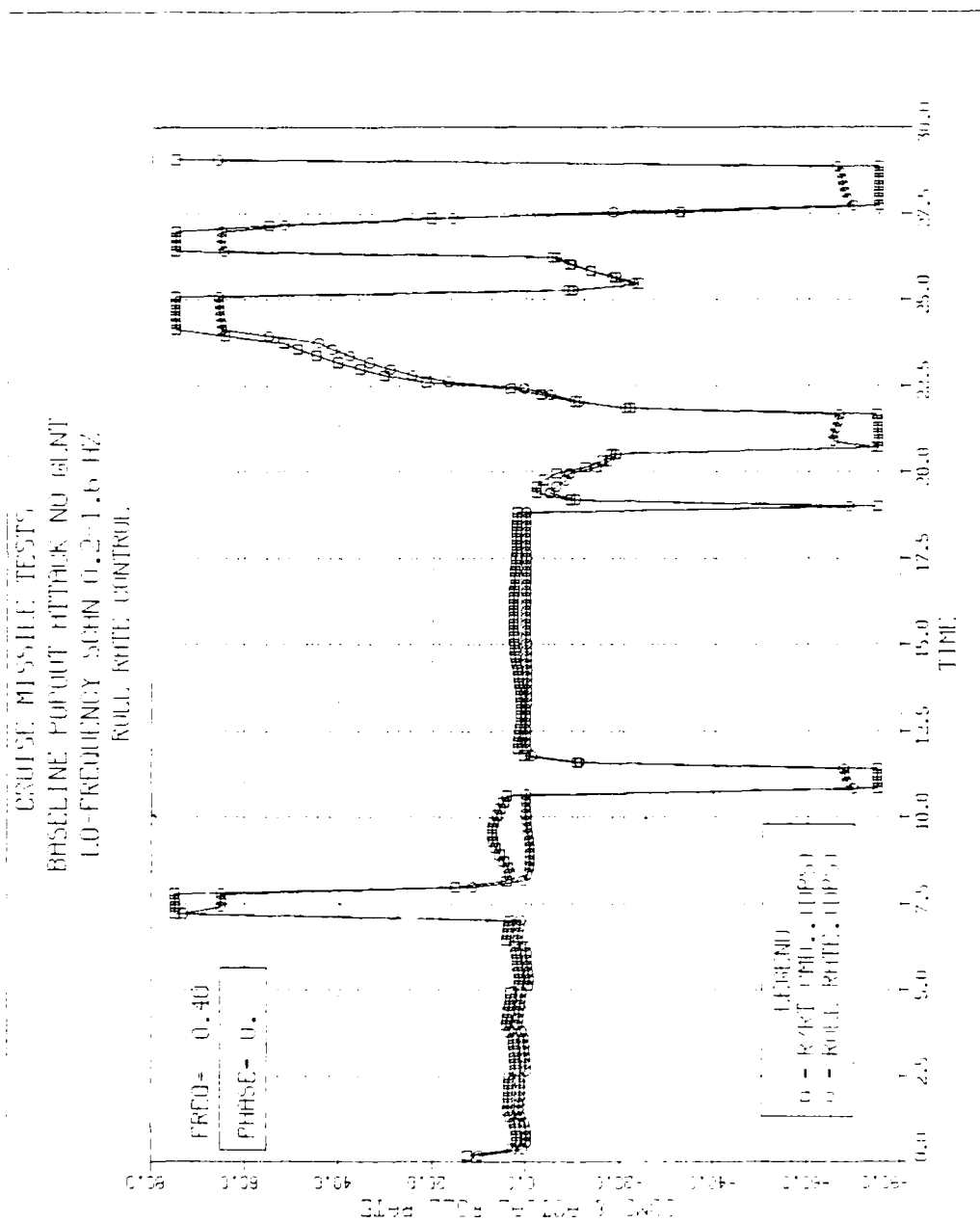


Figure A.52 Baseline/ECM Freq = 0.4 Hz - Roll Rate.

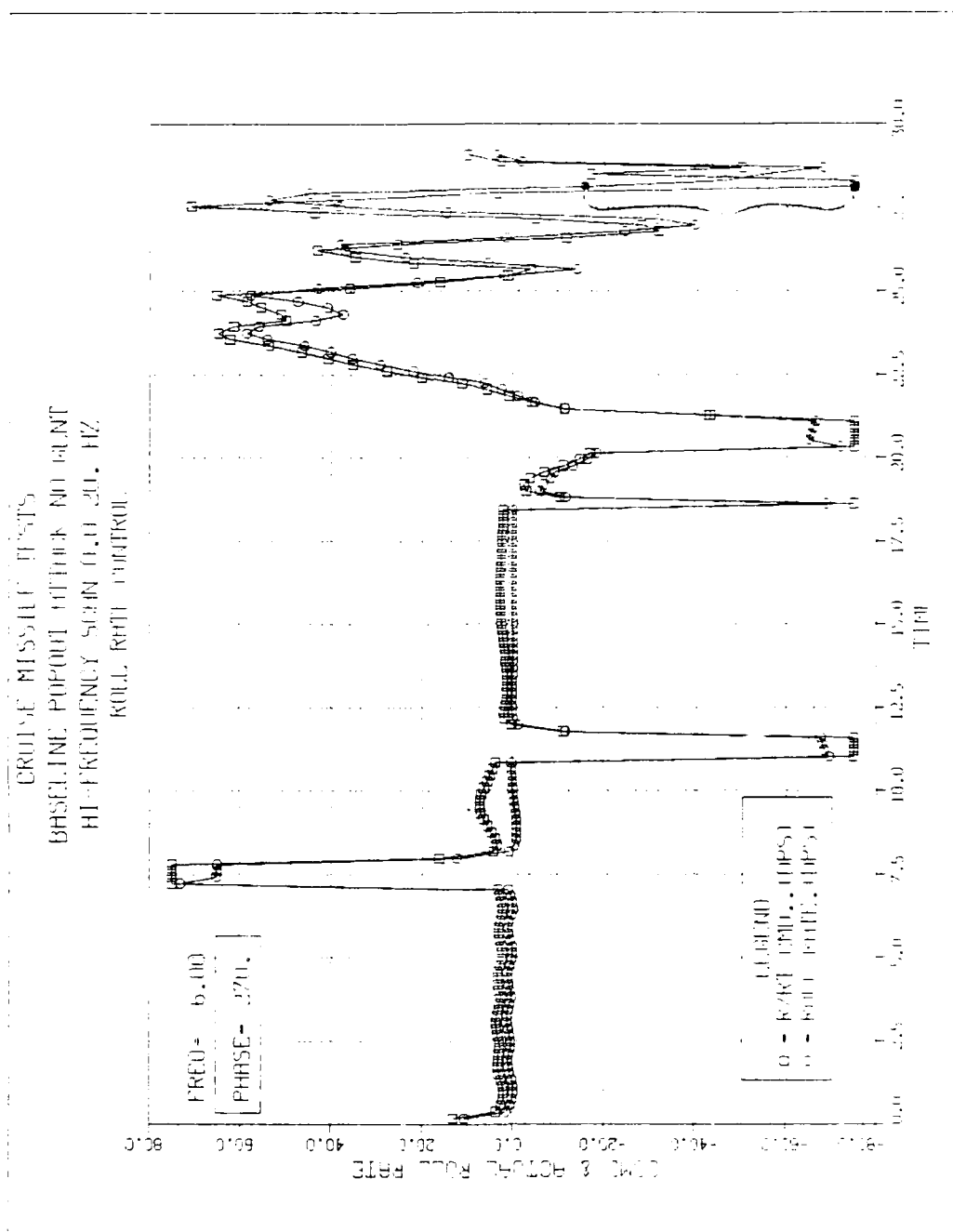


Figure A.53 Baseline/ECM Freq = 6.0 Hz - Roll Rate.

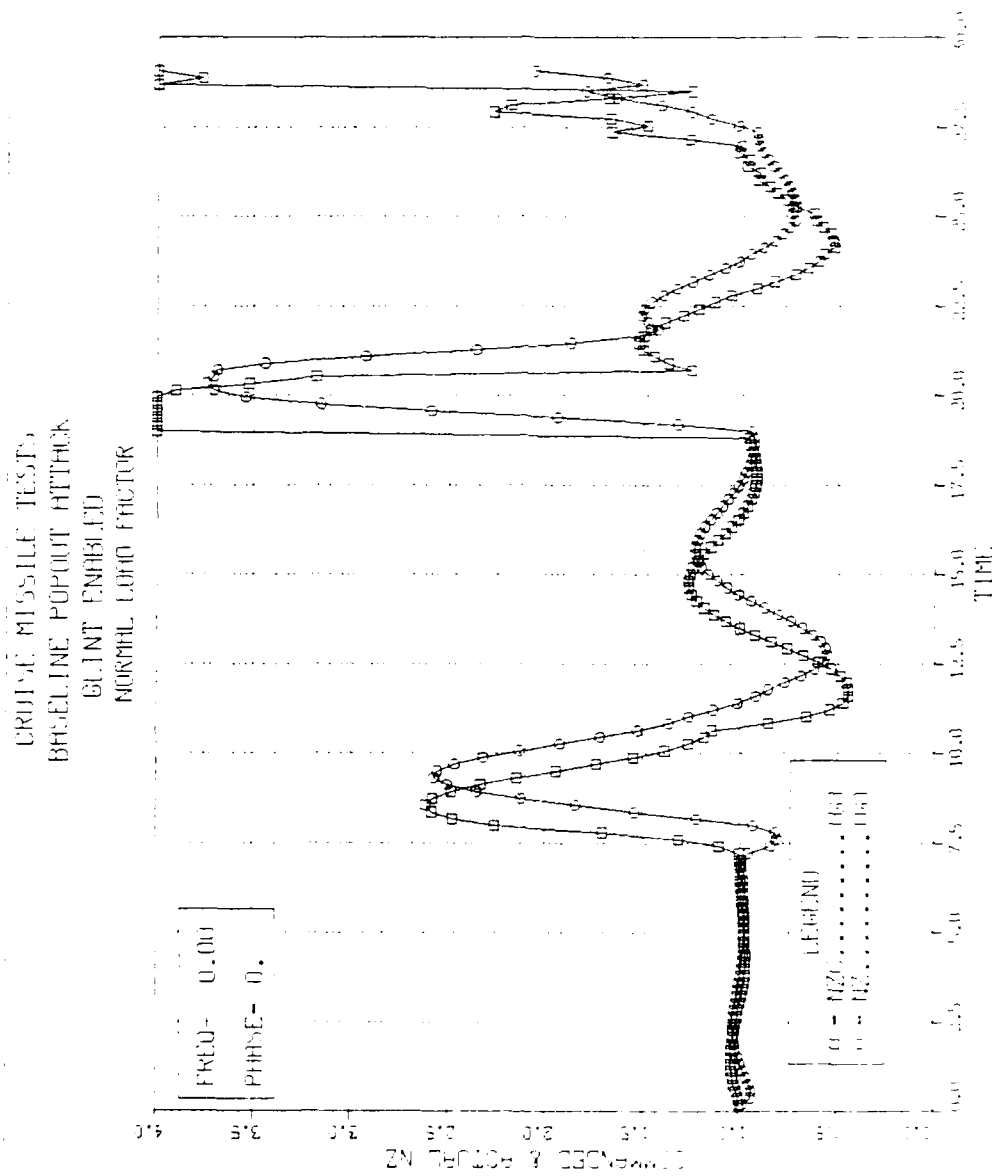


Figure A.54 Baseline with GLINT only - Load Factor.

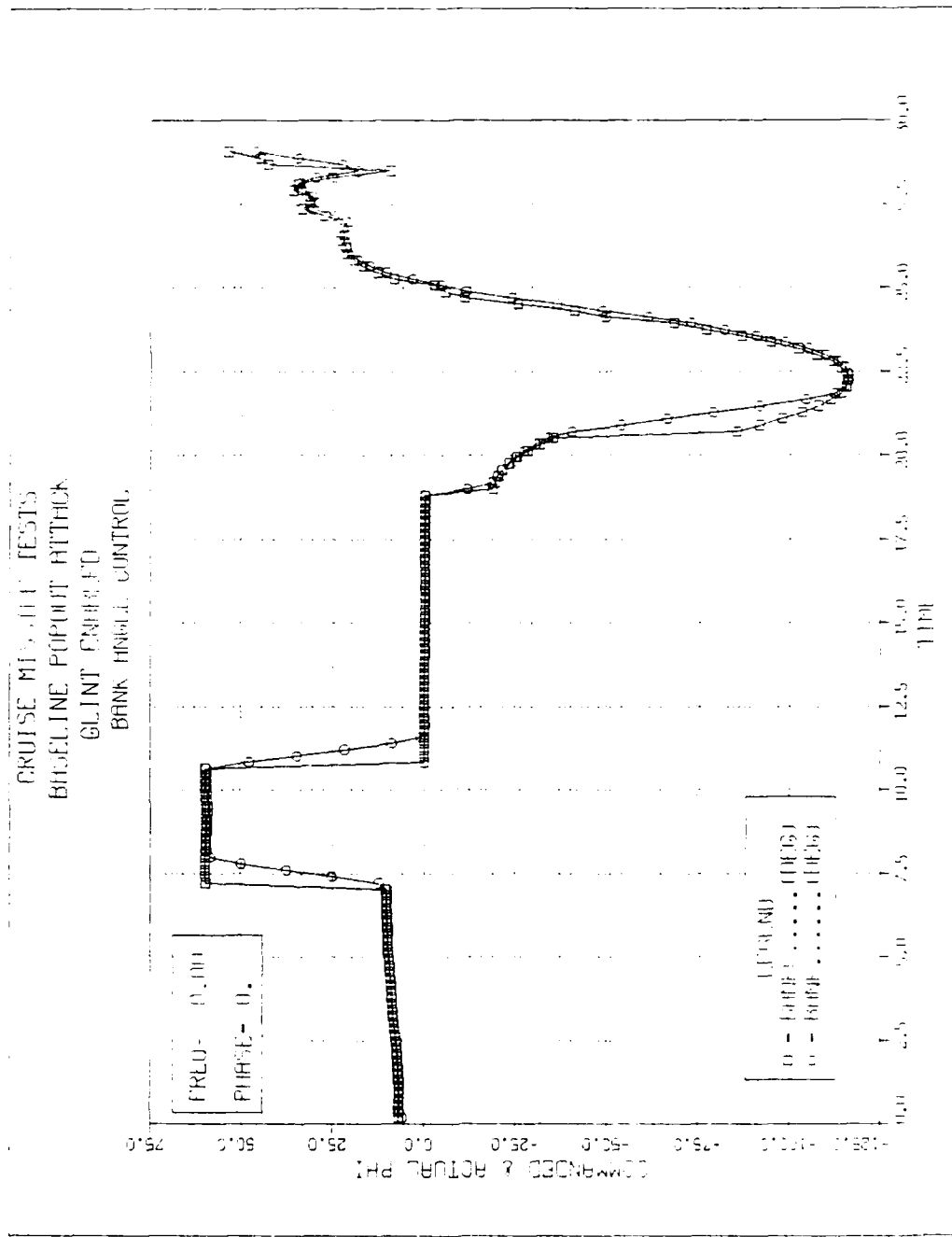


Figure A.55 Easeline with GLINT only - Bank.

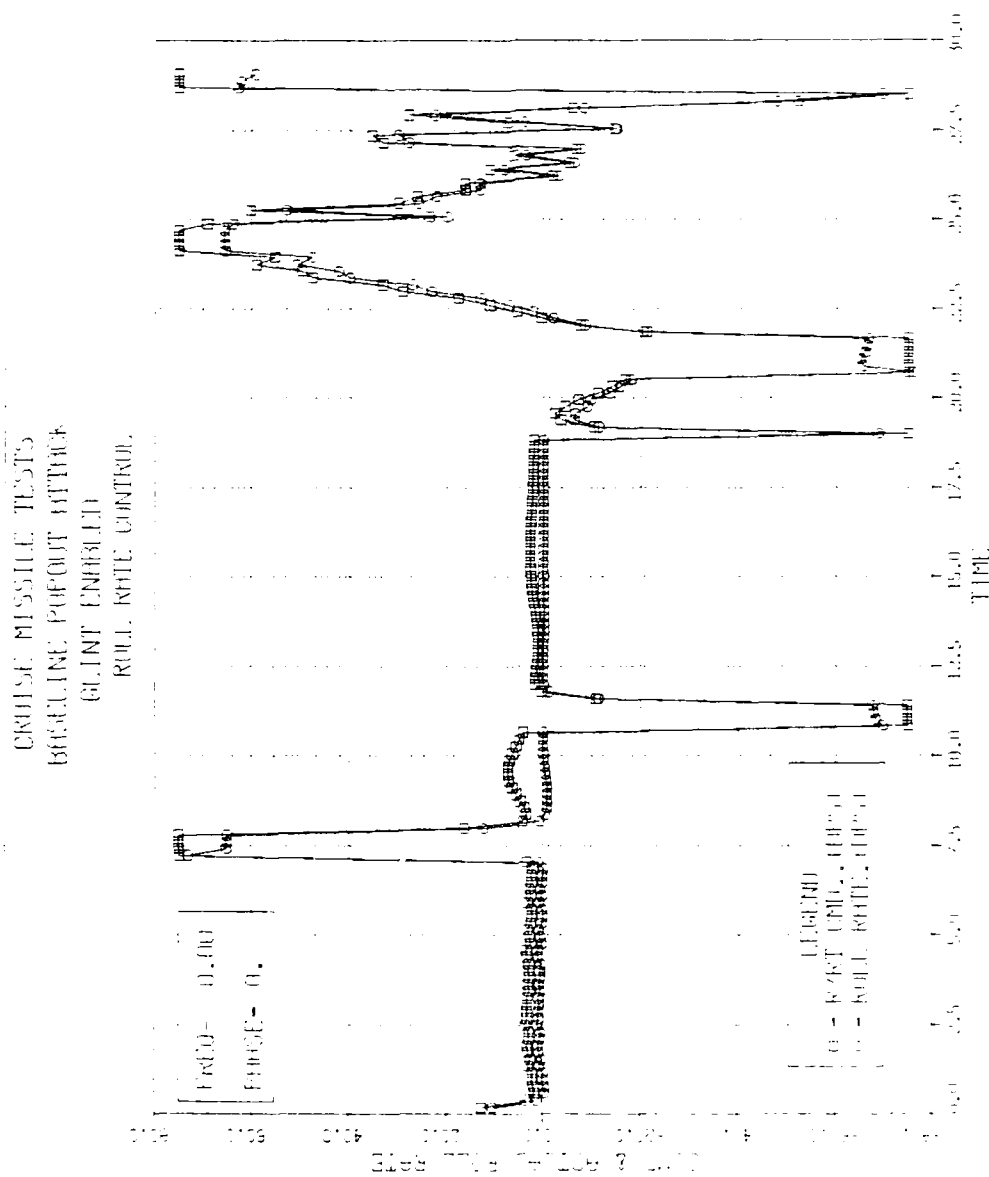


Figure A.56 Baseline with GLINT only - Roll Rate.

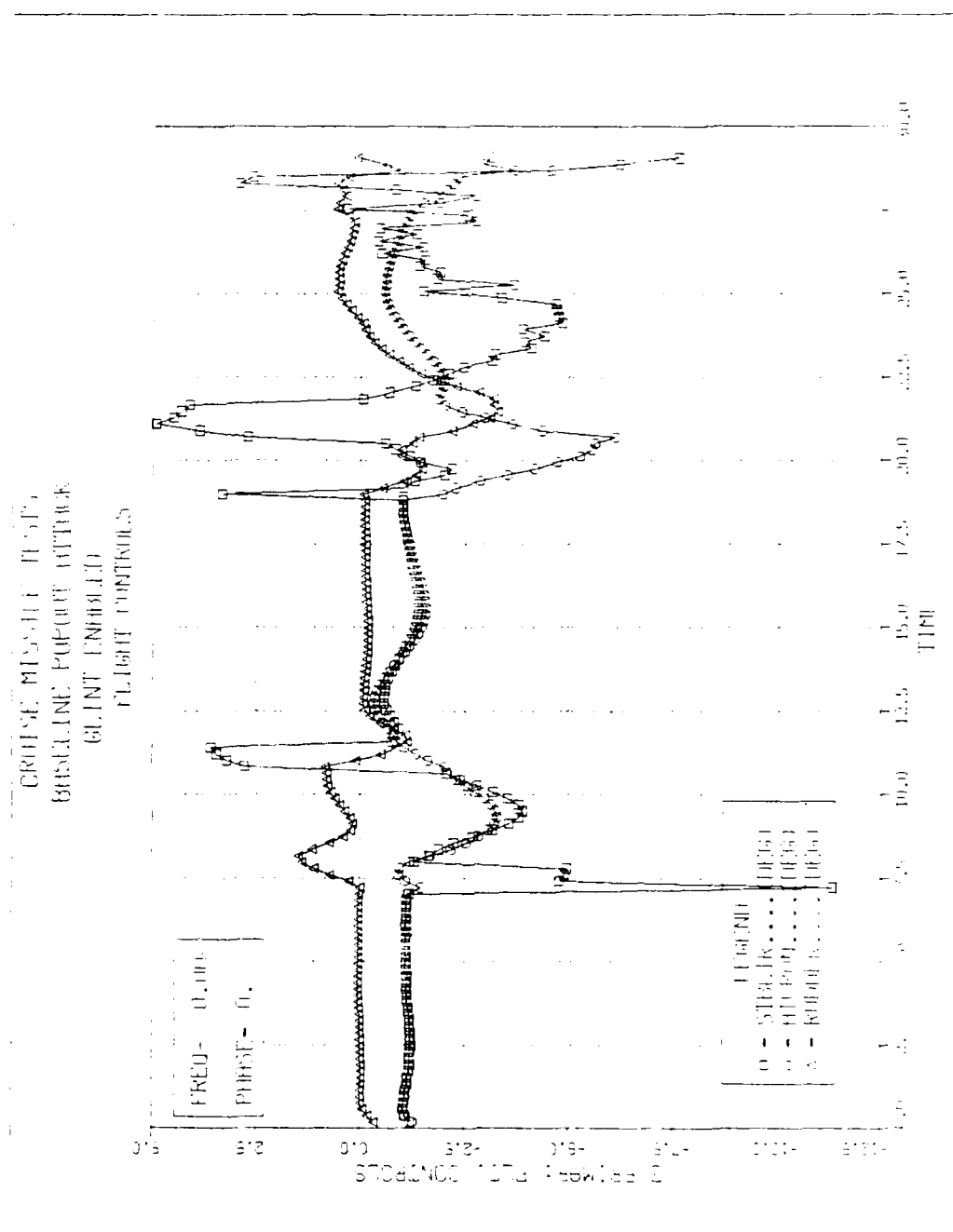


Figure A.57 Baseline with GLINT only - Controls.

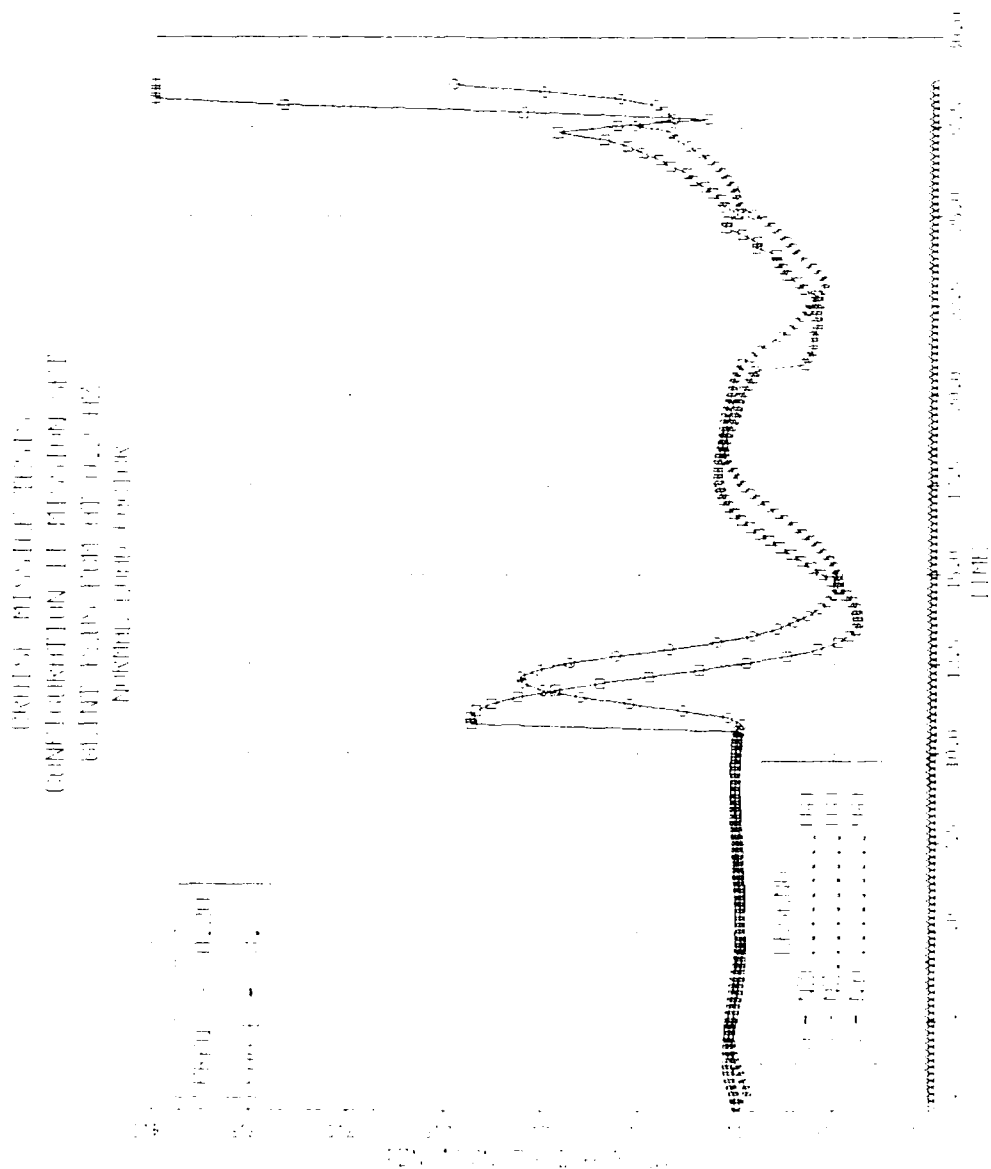


Figure A.58 Conf. II Mission Set - Load Factor.

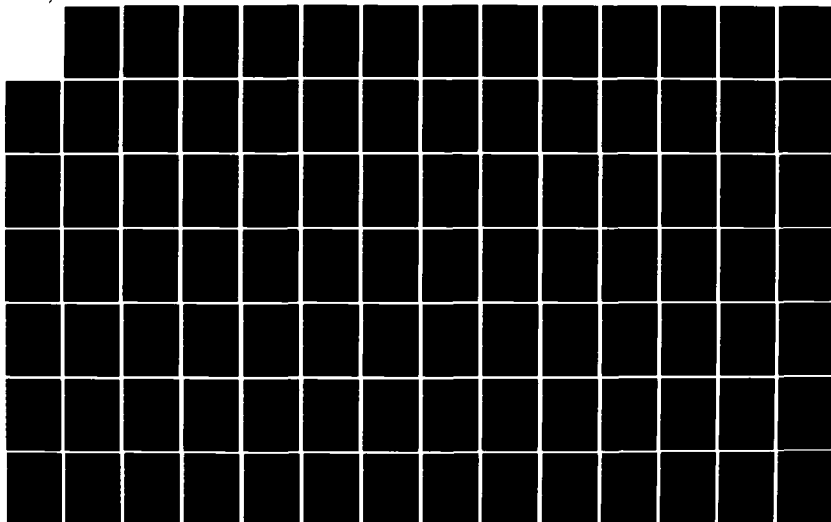
AD-A152 193

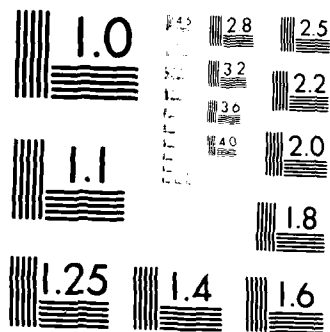
AN INVESTIGATION INTO THE CONTROL LIMITATIONS OF A BANK 2/3
TO TURN MISSILE IN THE TERMINAL HOMING PHASE(U) NAVAL
POSTGRADUATE SCHOOL MONTEREY CA 8 P ANDERSON SEP 84

UNCLASSIFIED

F/G 17/7

NL





MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

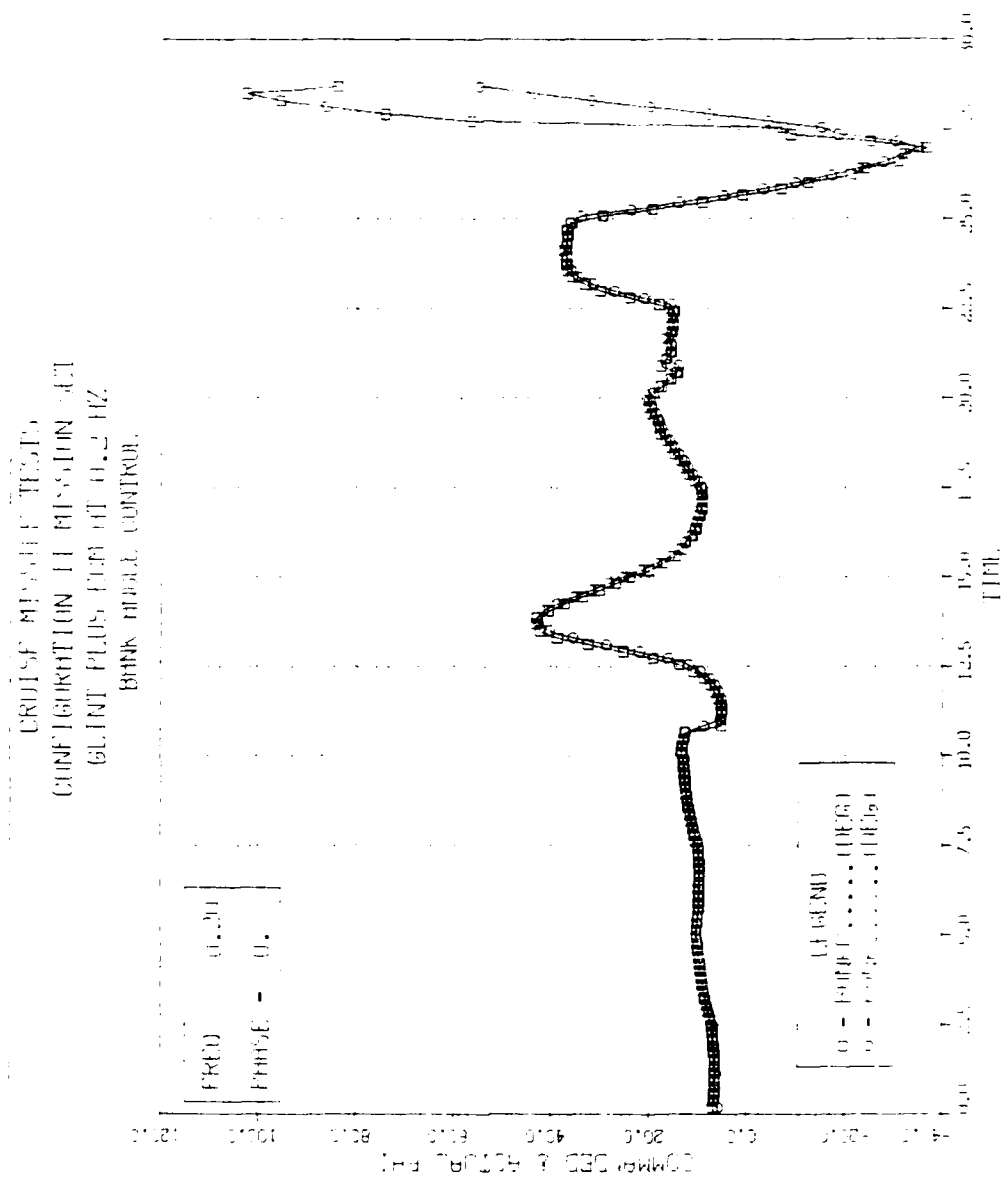


Figure A.59 Conf. II Mission Set - Bank.

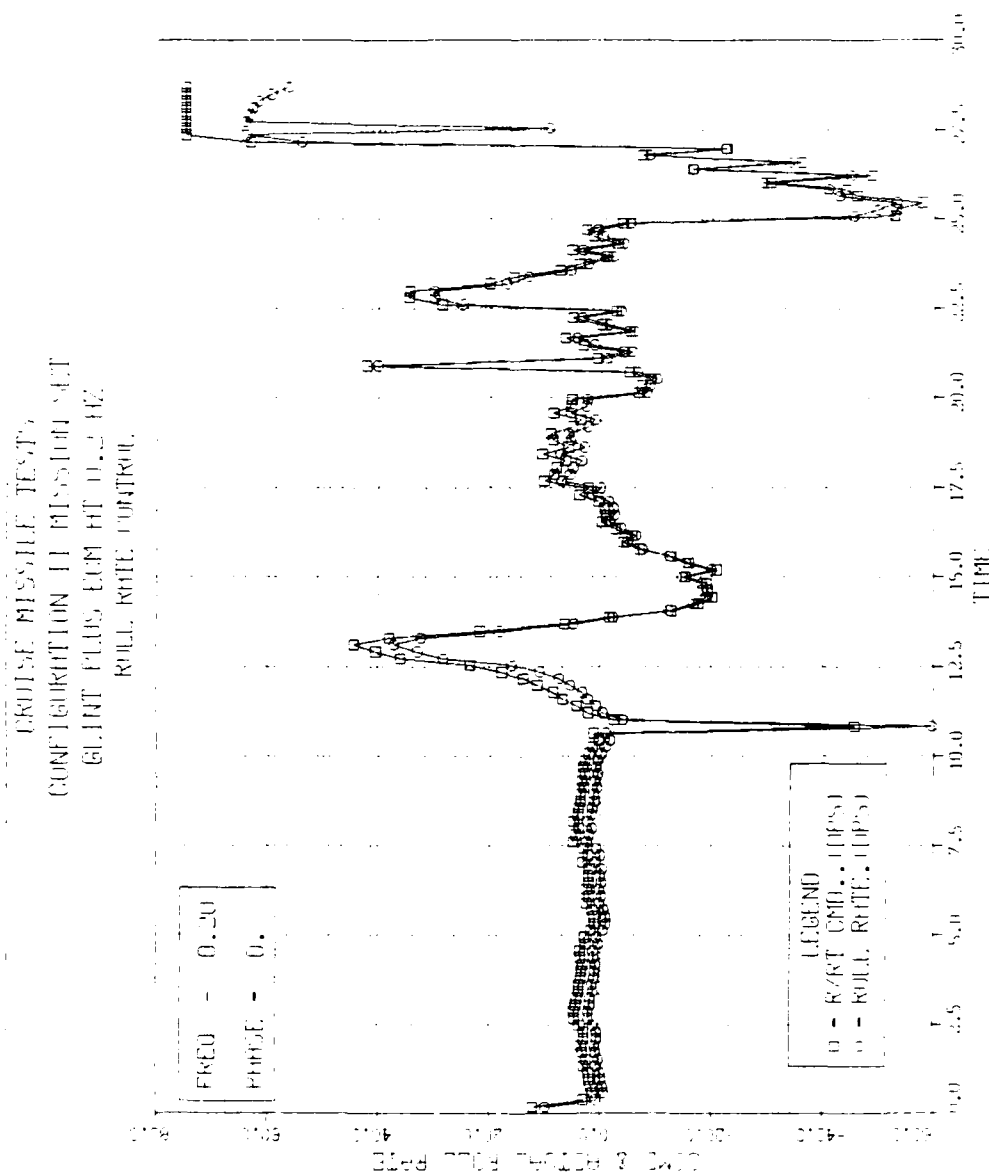


Figure A.60 Conf. II Mission Set - Roll Rate.

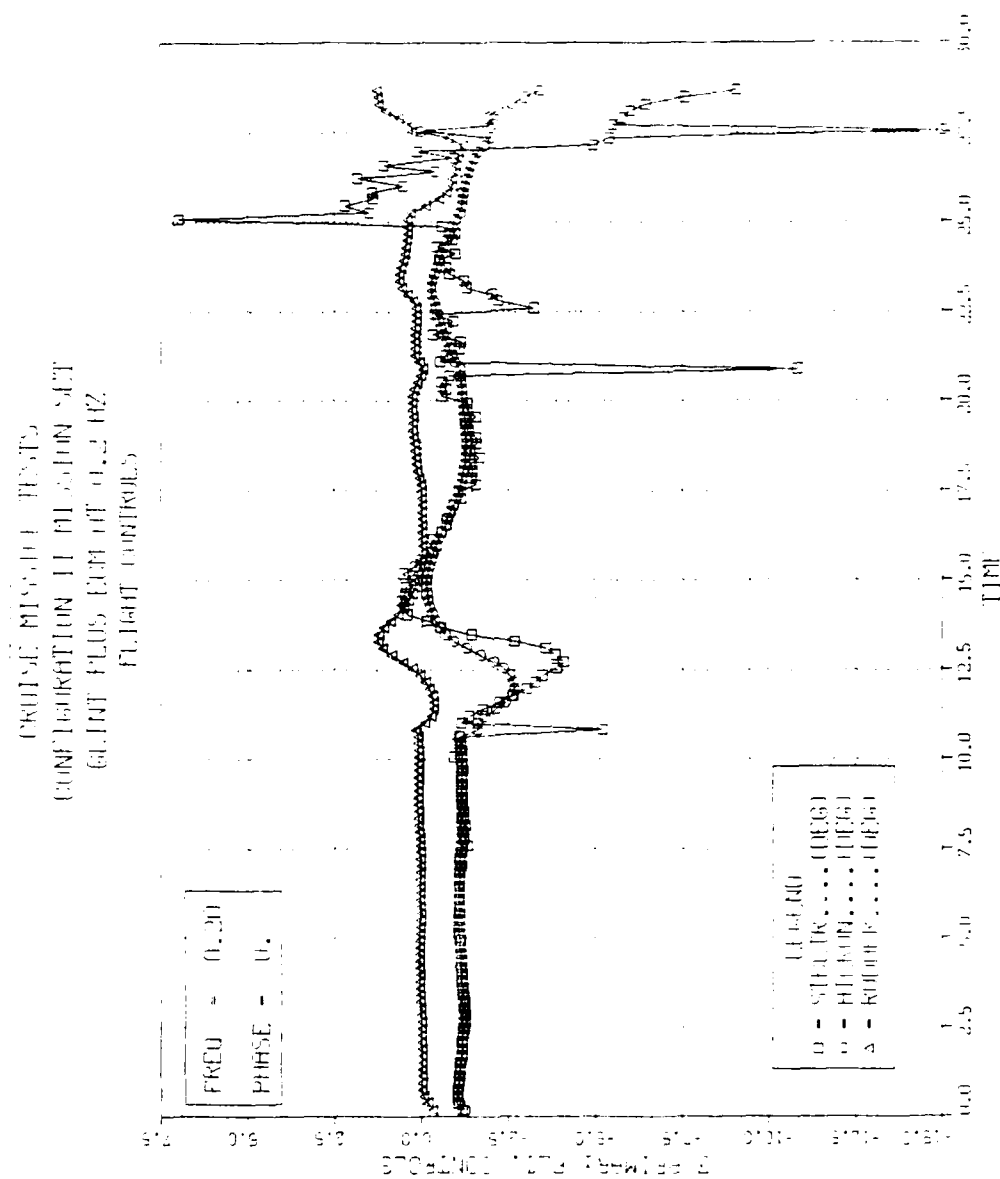


Figure A.61 Conf. II Mission Set - Controls.

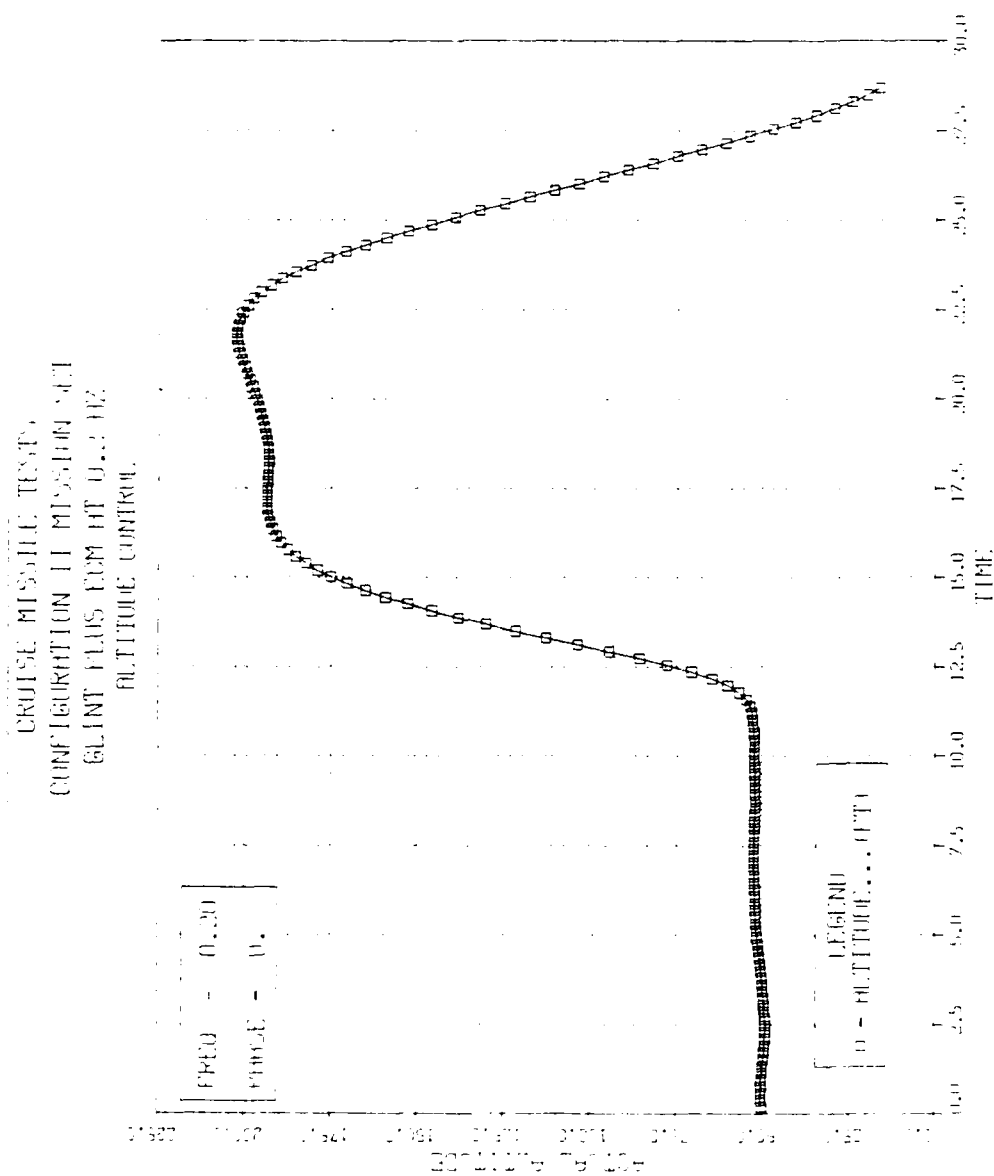


Figure A.62 Conf. II Mission Set - Altitude.

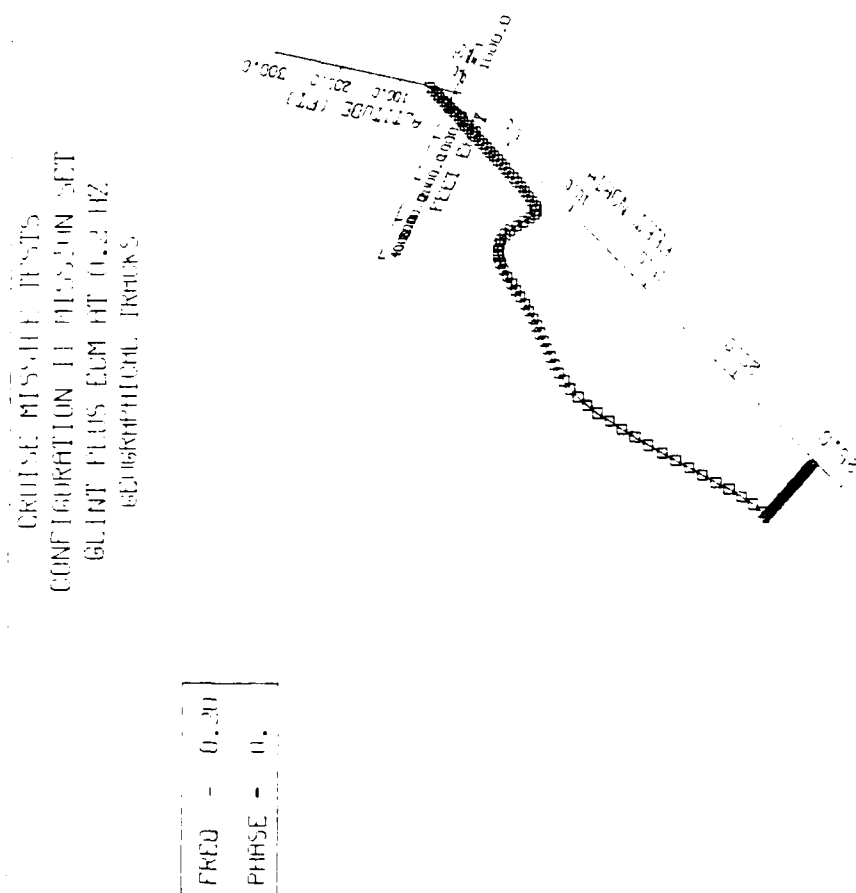


Figure A.63 Conf. II Mission Set - Geo Plot.

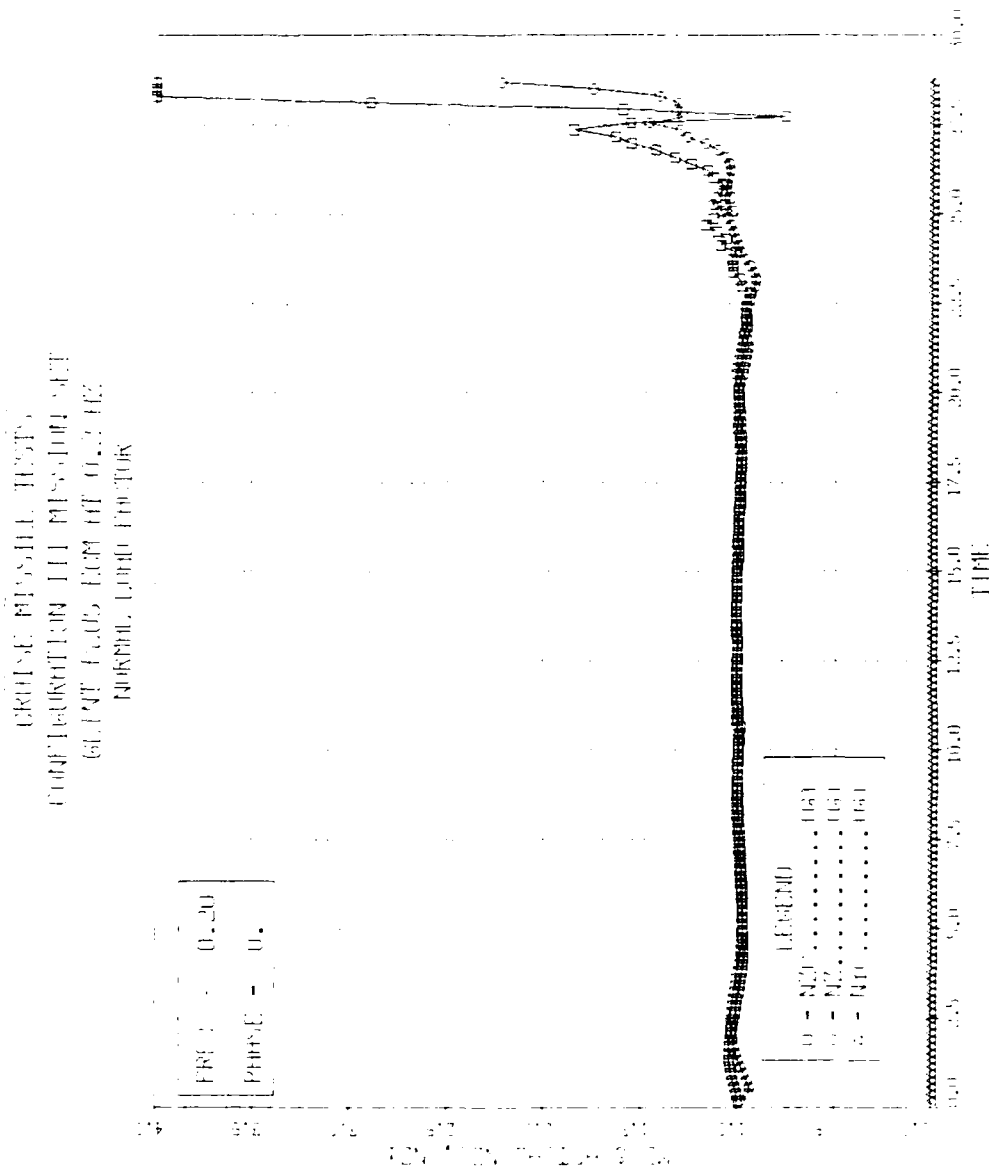


Figure A.64 Conf. III Mission Set - Load Factor.

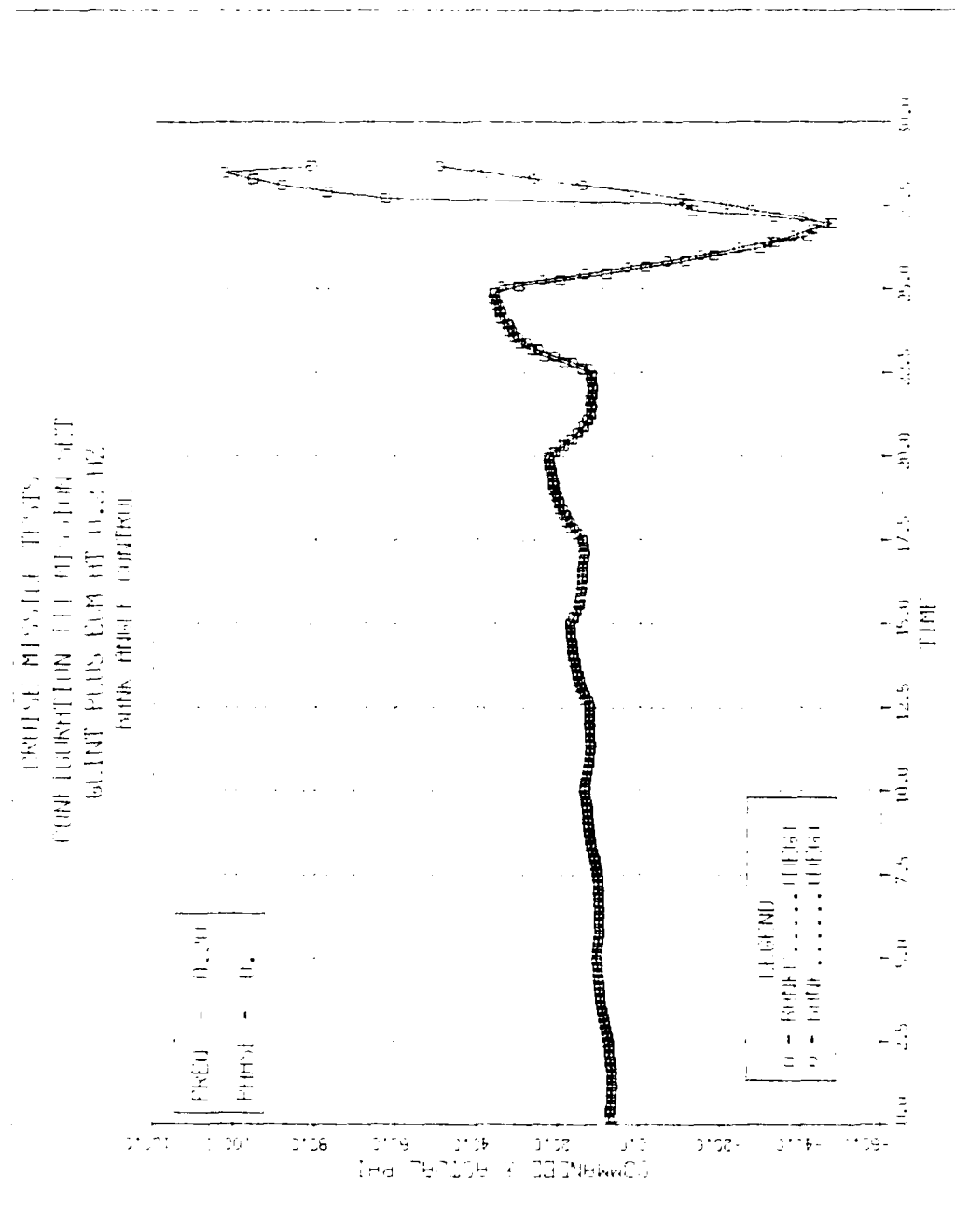


Figure A.65 Conf. III Mission Set - Bank.

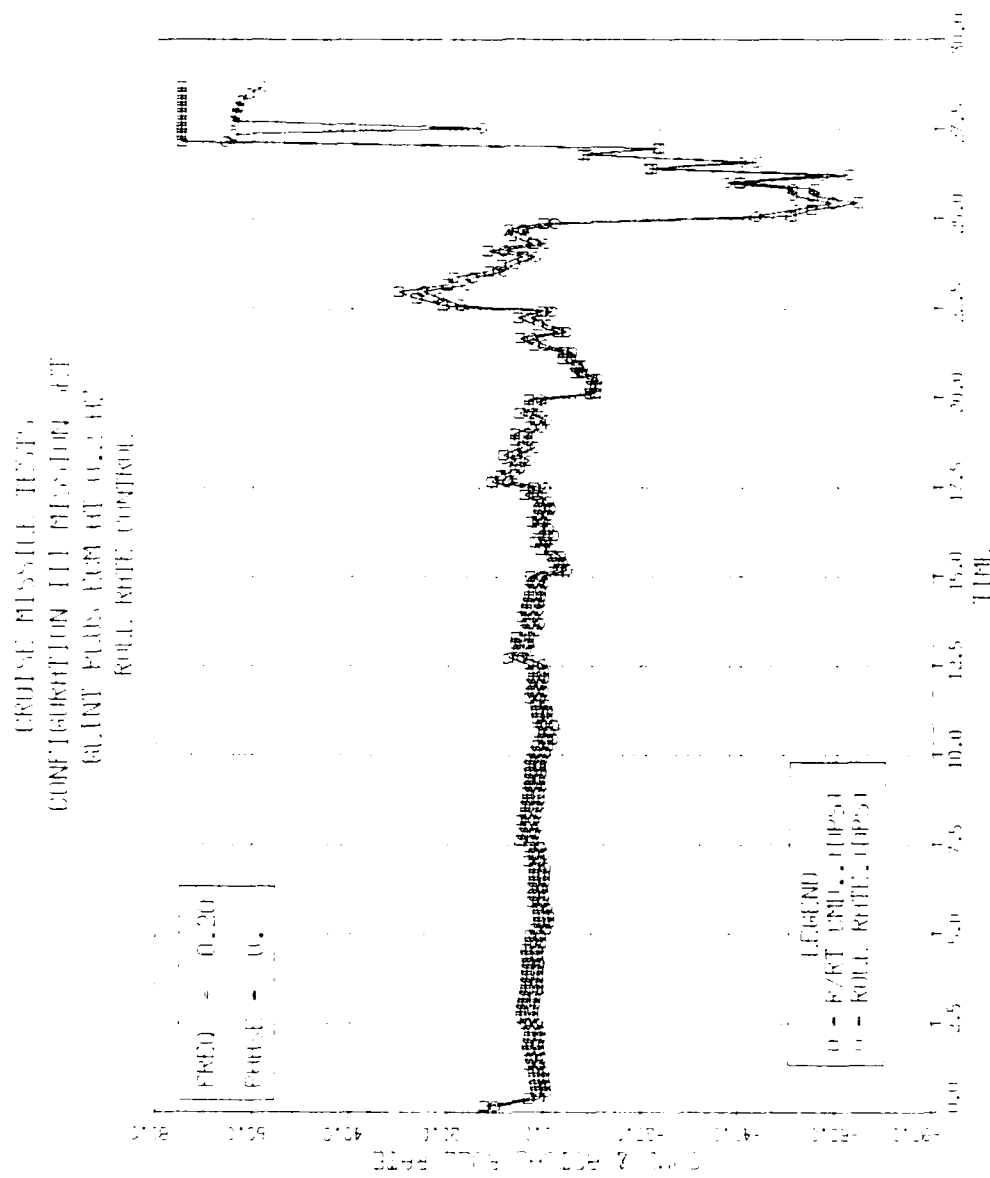


Figure A.66 Conf. III Mission Set - Roll Rate.

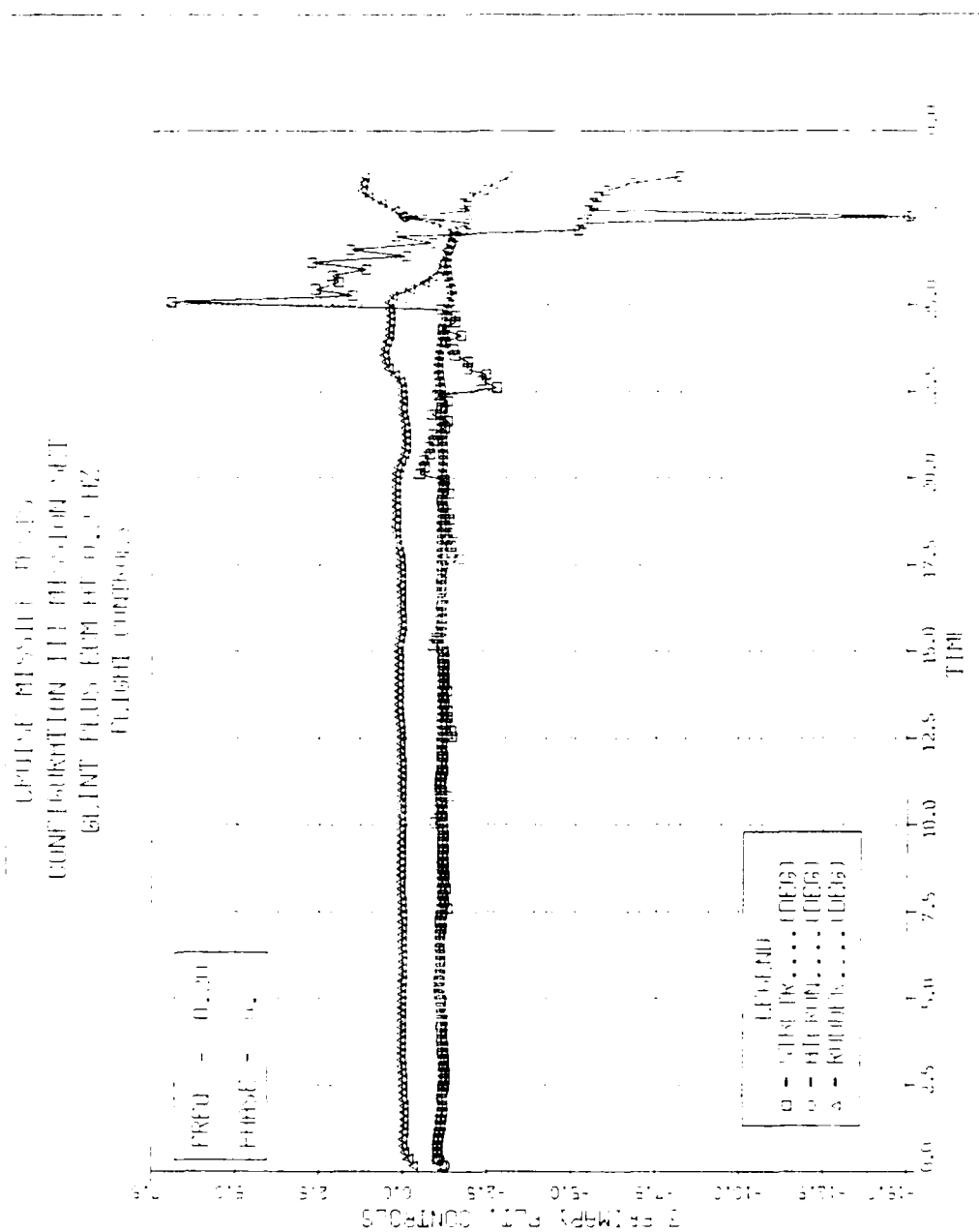


Figure A.67 Conf. III Mission Set - Controls.

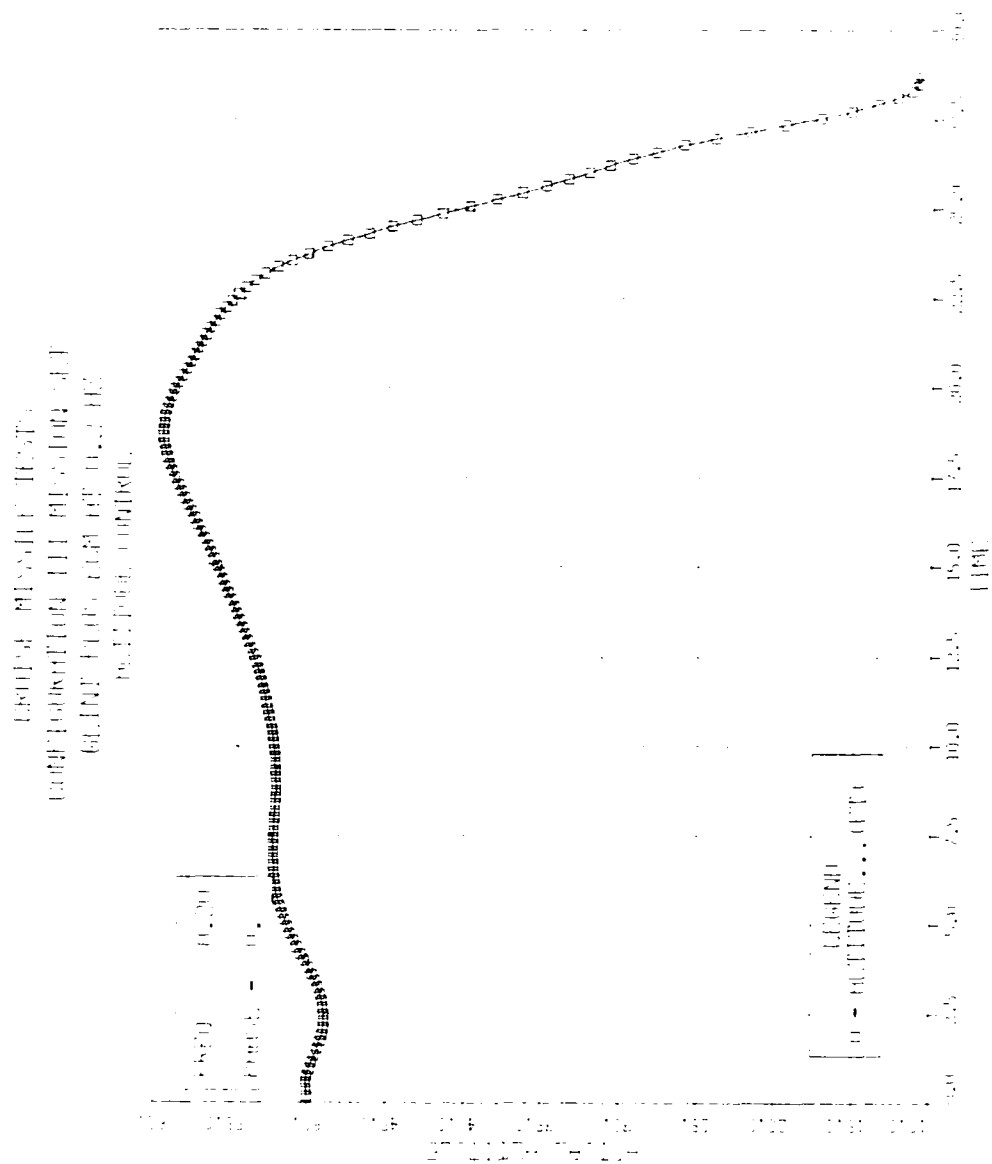


Figure A.68 Ccnf. III Mission Set - Altitude.

CRUISE RESULTS PLOTS
 CONFIGURATION III MISSION SET
 COUNT PLUS ALTITUDE TRACK

TIME	11.20
ALTITUDE	0.

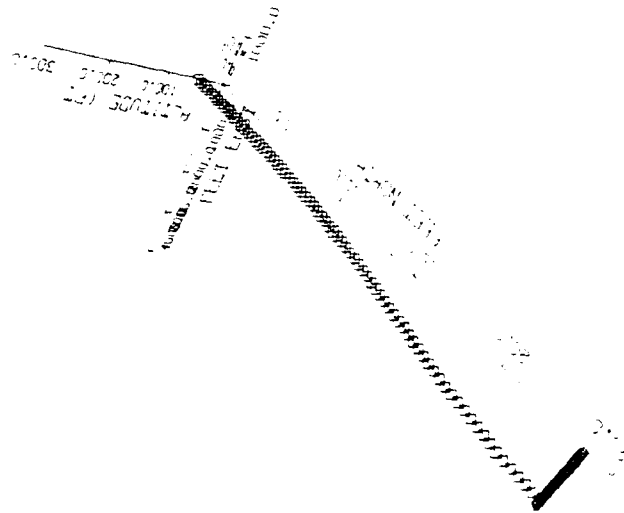


Figure A.69 Conf. III Mission Set - Geo Plot.

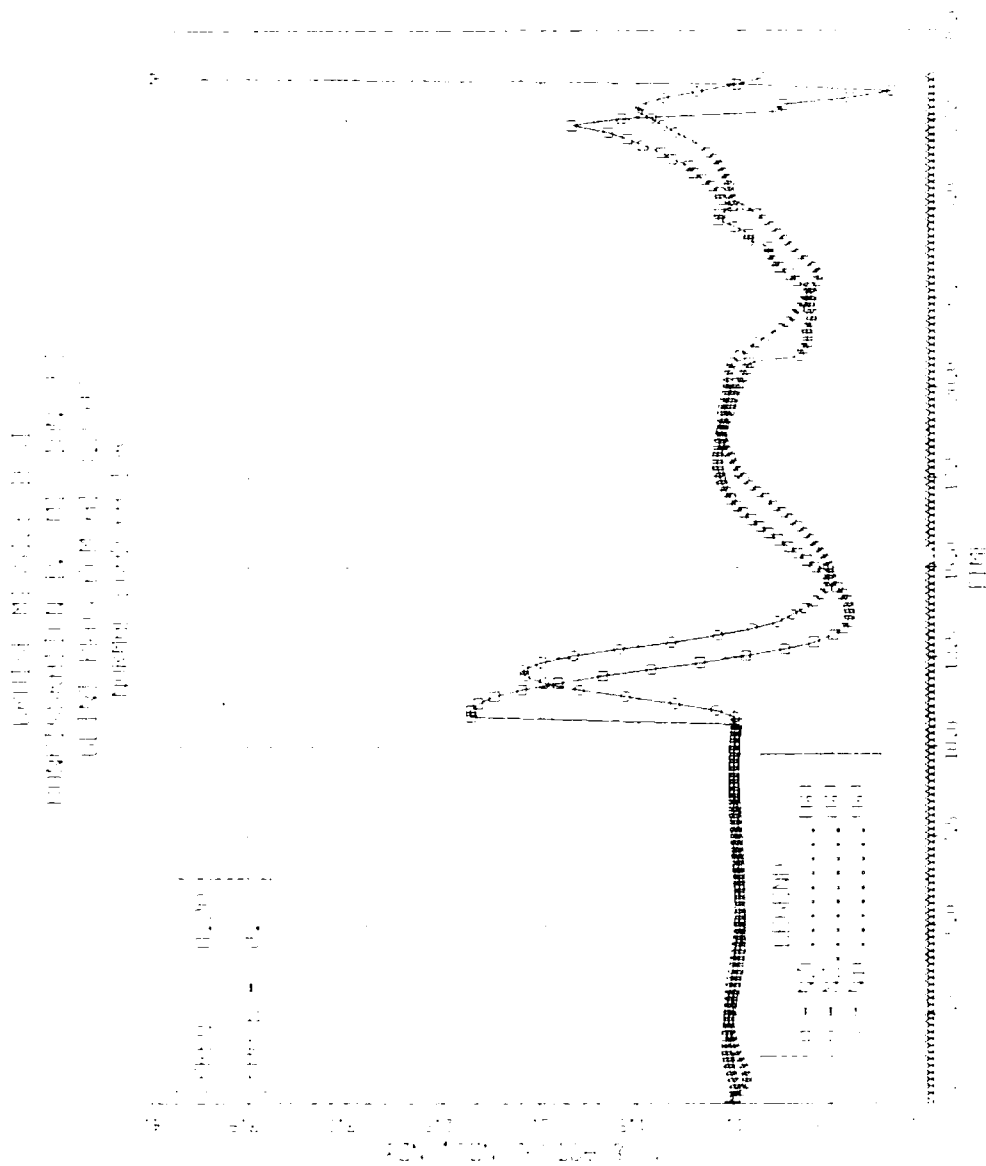


Figure A.70 Conf. IV Mission Set - Load Factor.

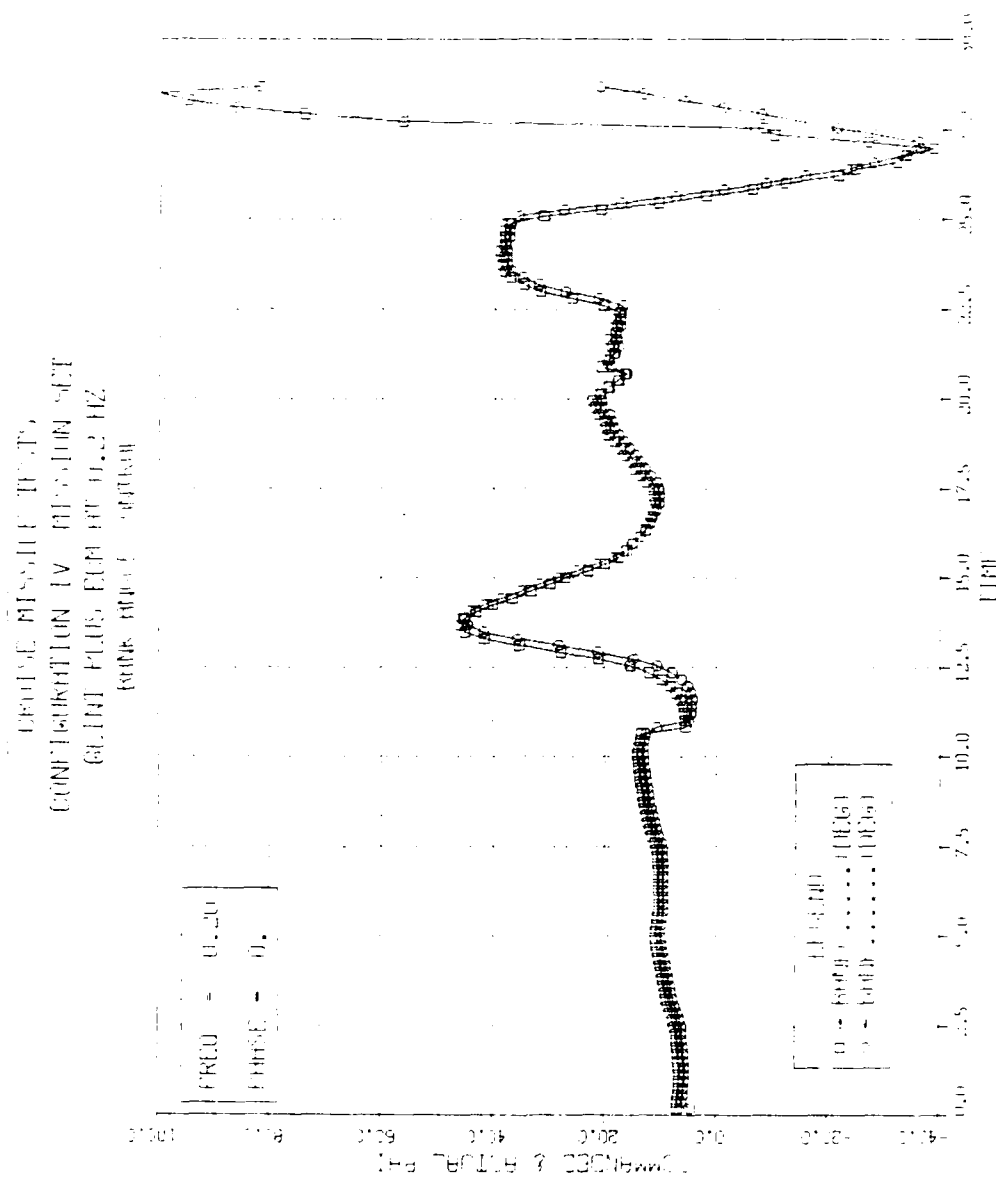


Figure A.71 Conf. IV Mission Set - Bank.

CRUISE MISSILE TESTS
 CONFIGURATION IV MISSION SET
 GLIDE FLIPS EUM HT 0.2 HZ
 ROLL RATE CONTROL

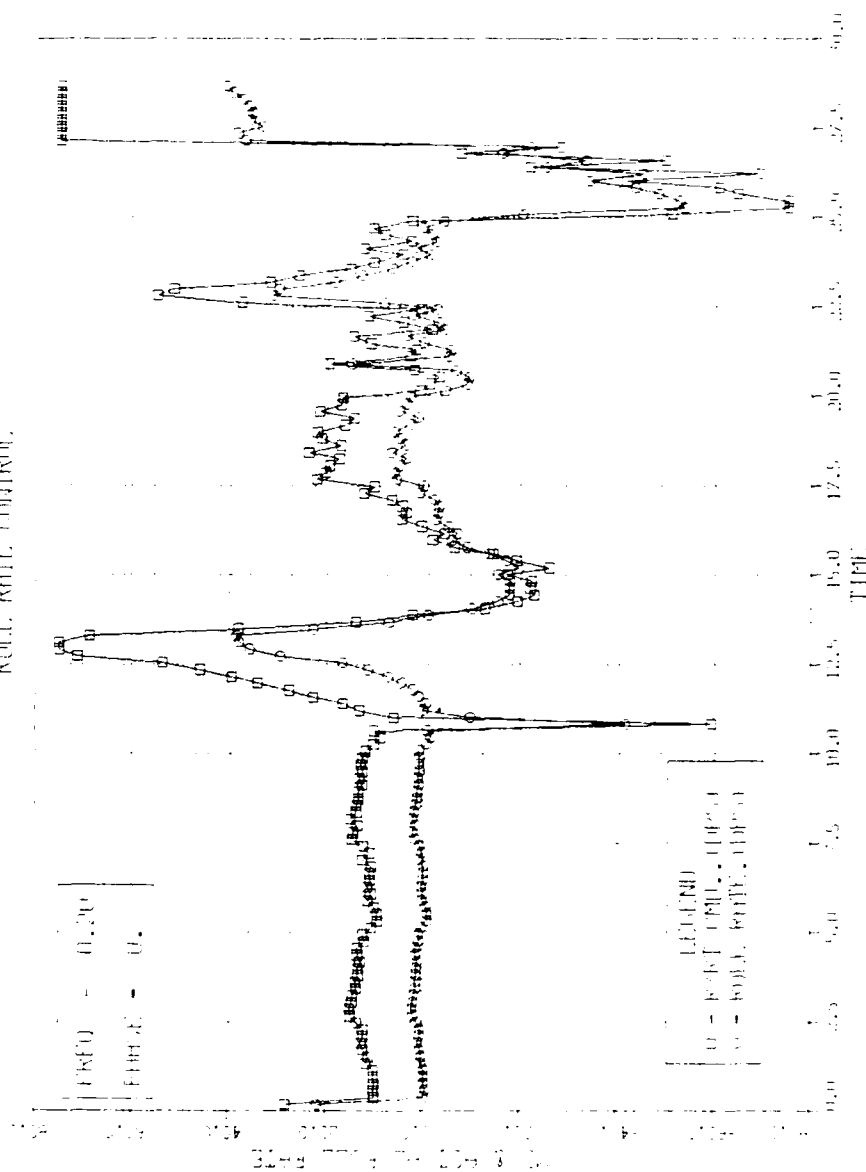


Figure A.72 Ccnf. IV Mission Set - Roll Rate.

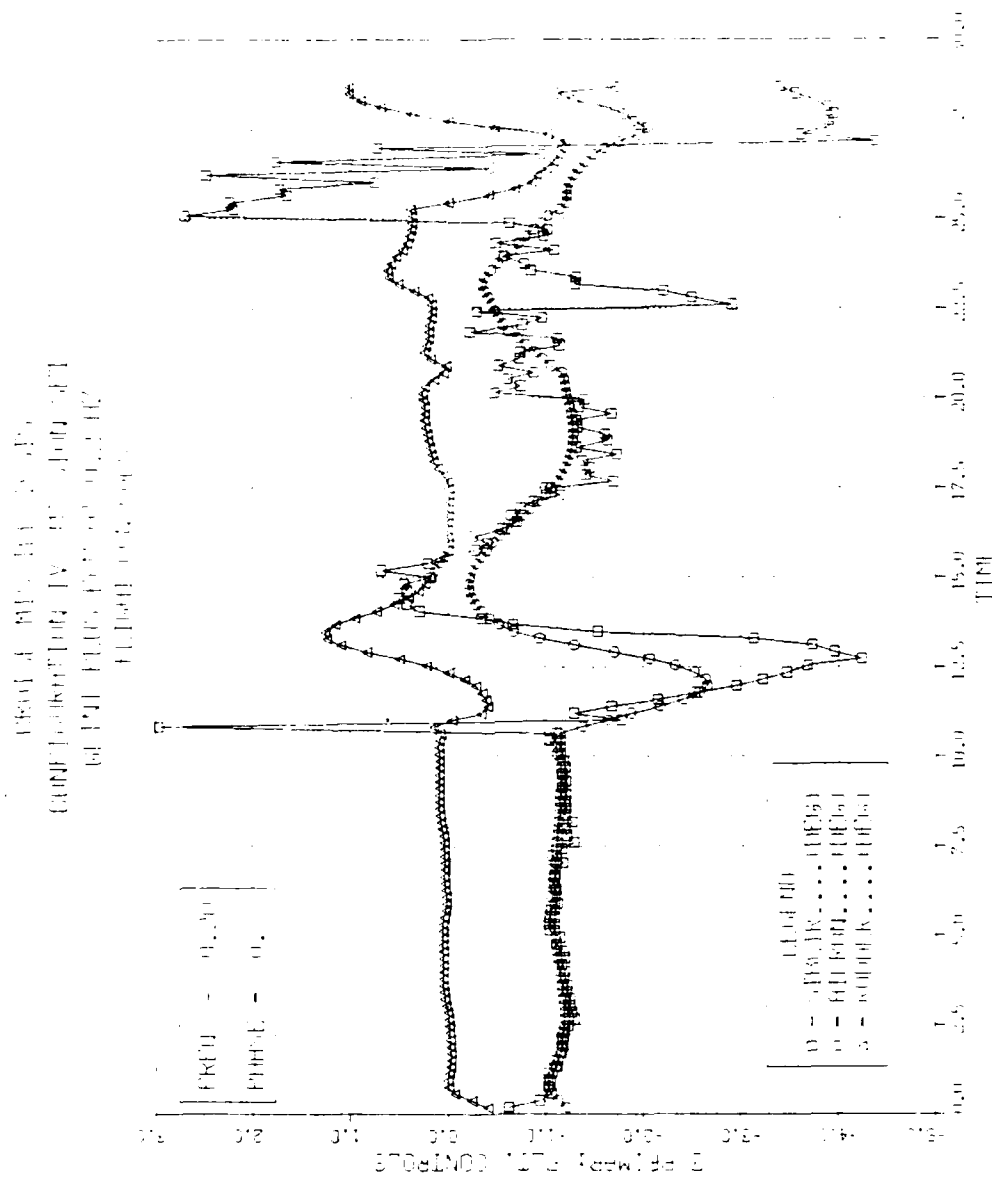


Figure A.73 Conf. IV Mission Set - Controls.

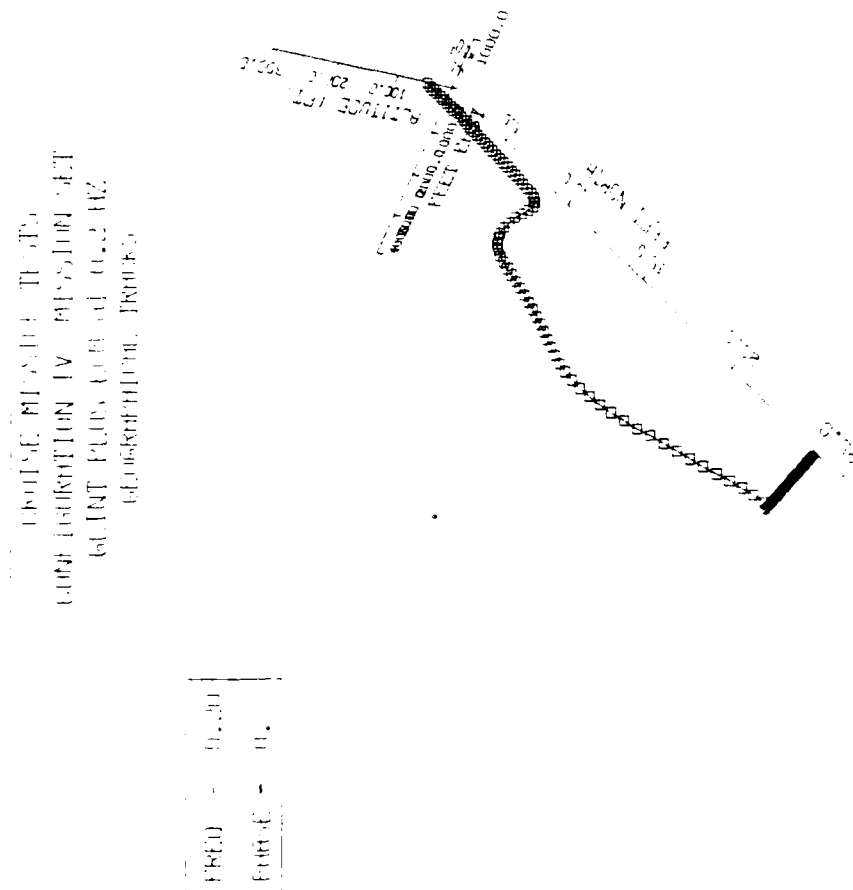


Figure A.75 Conf. IV Mission Set - Geo Plot.

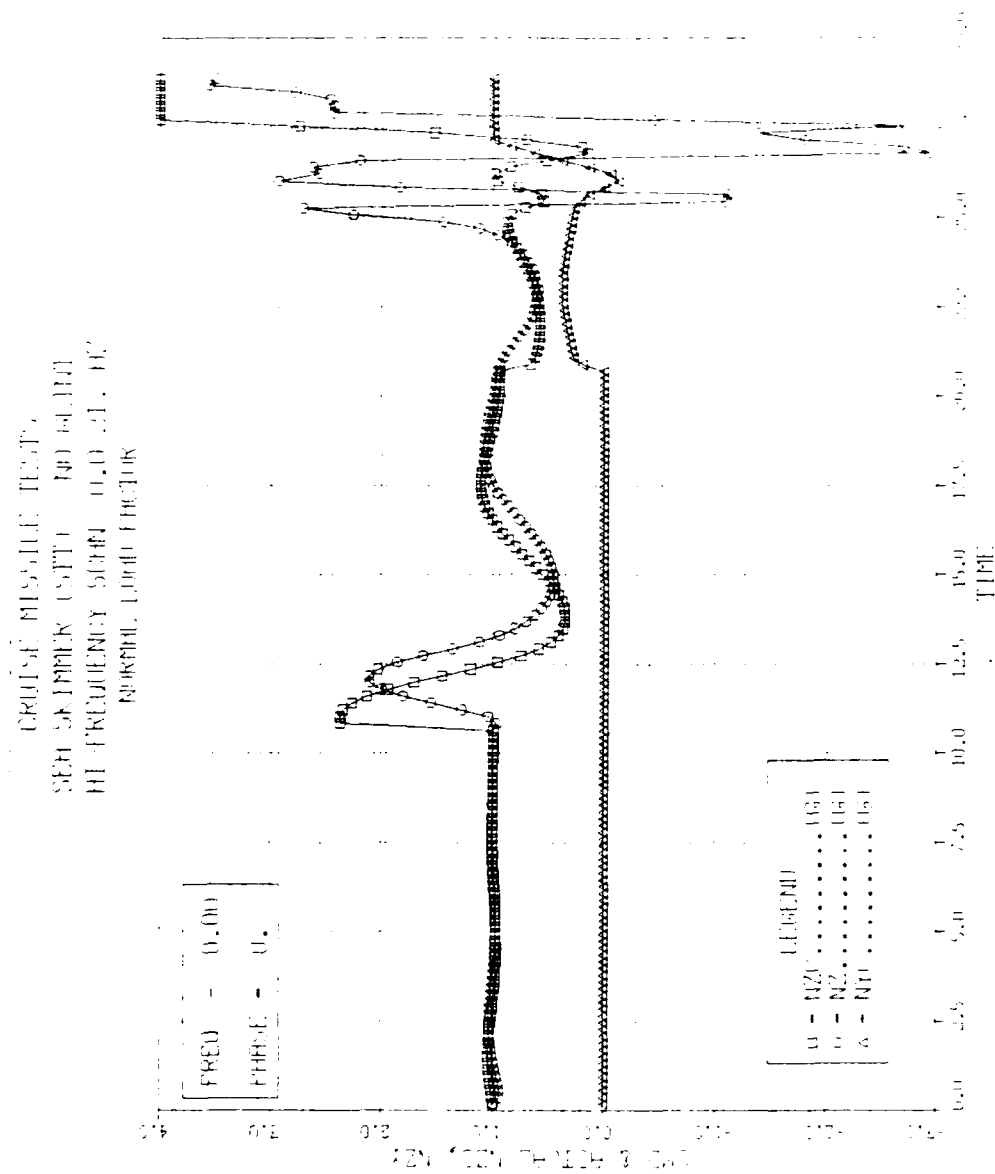


Figure A.76 Ccnf. V Mission Set - Load Factor.

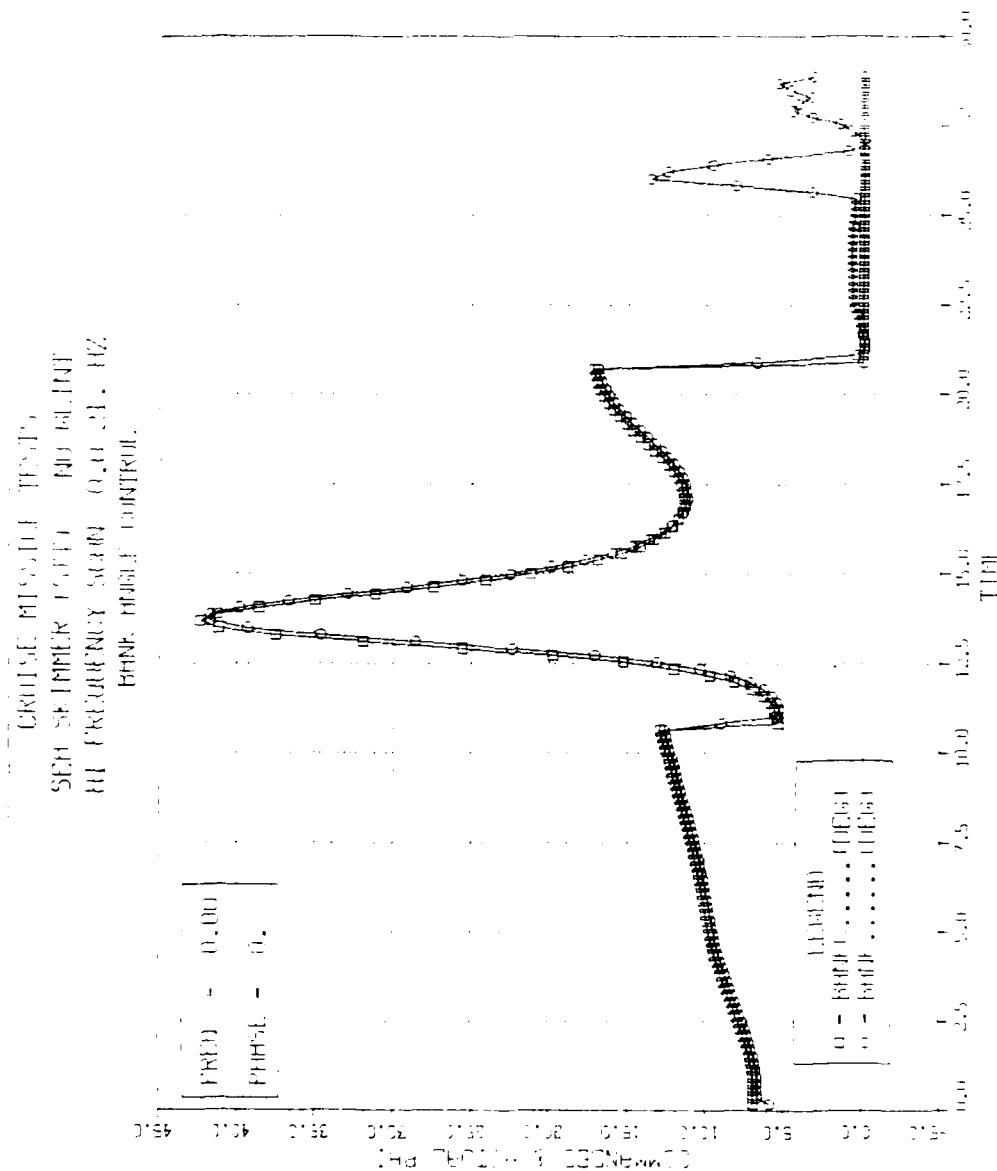


Figure A.77 Conf. V Mission Set - Bank.

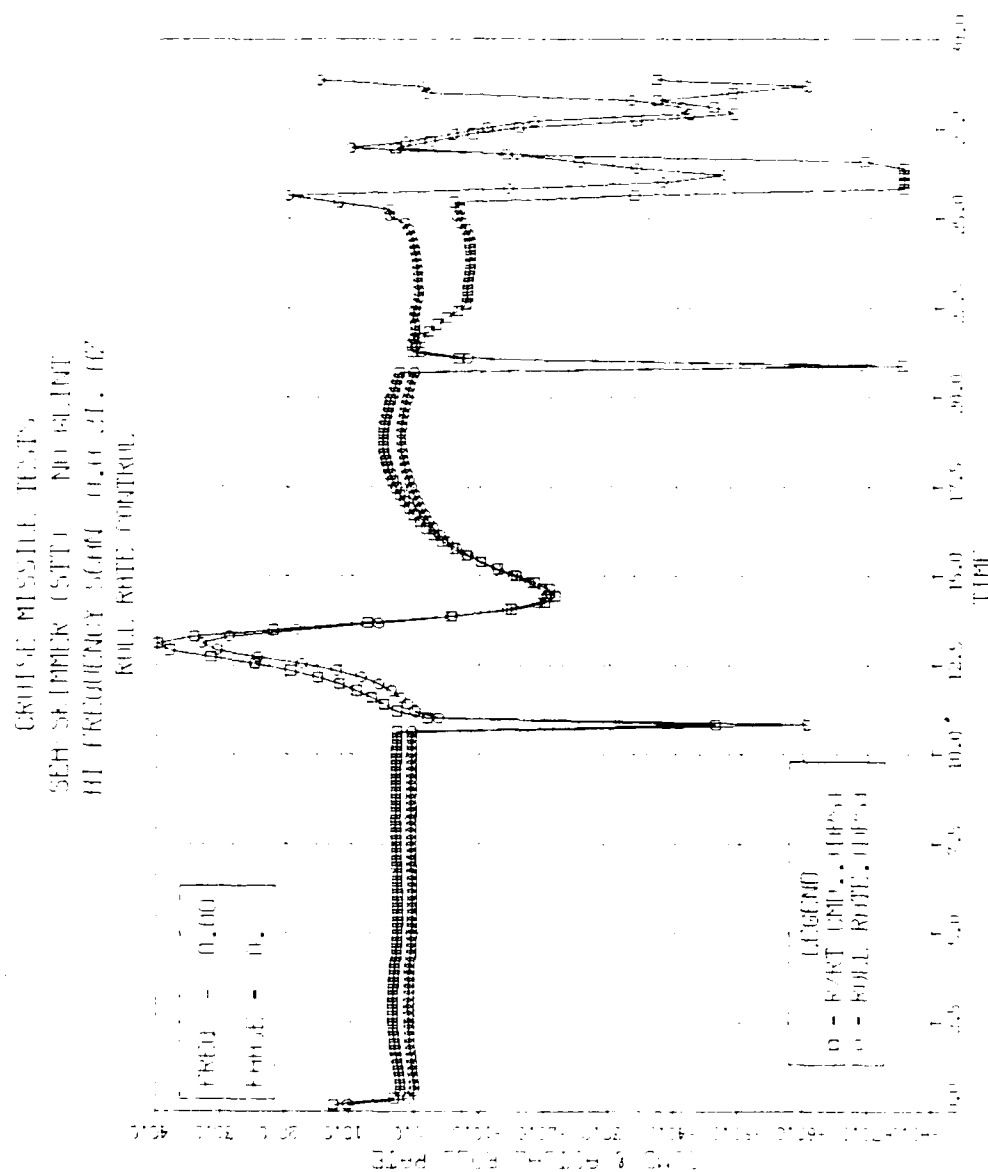


Figure A.78 Conf. V Mission Set - Roll Rate.

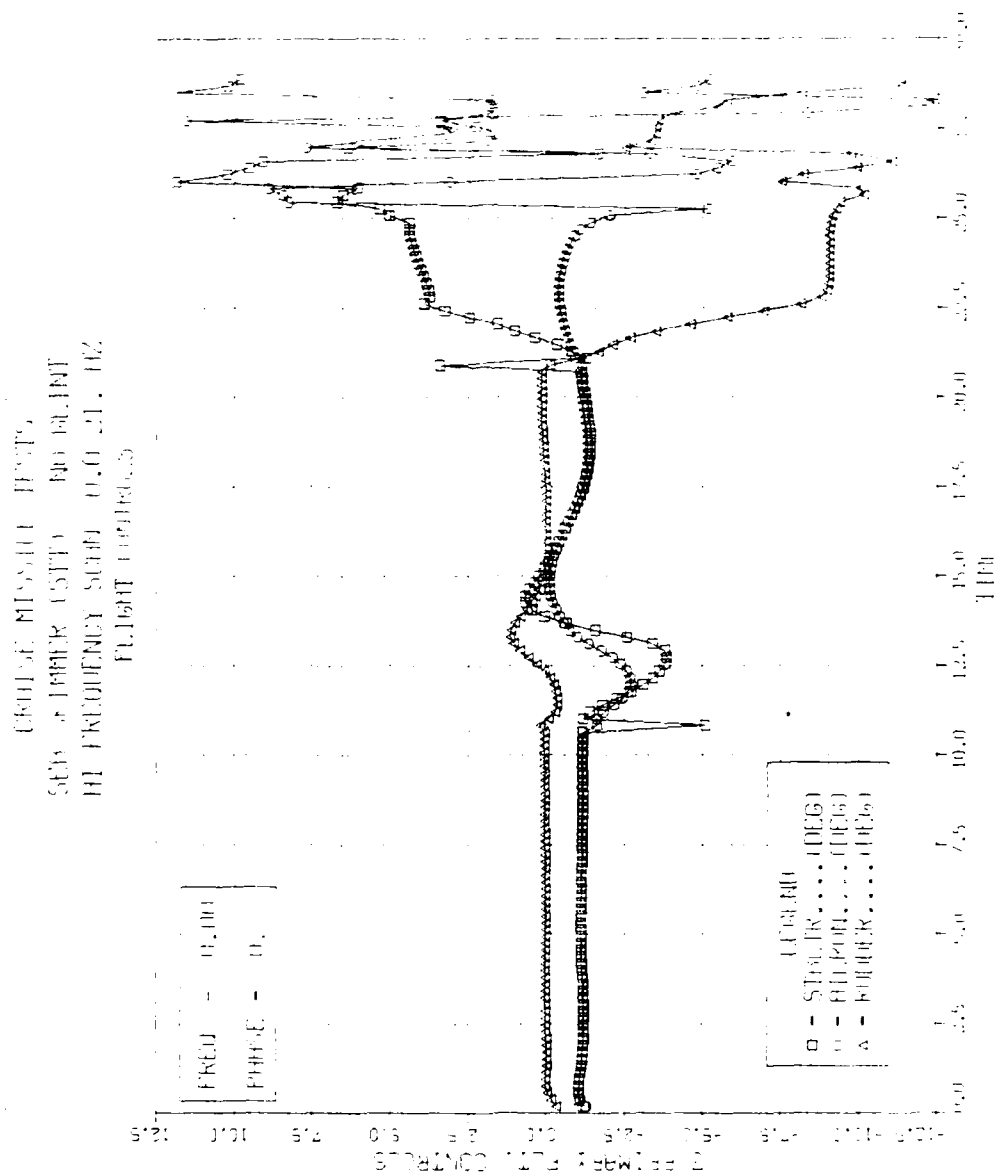


Figure A.79 Conf. V Mission Set - Controls.

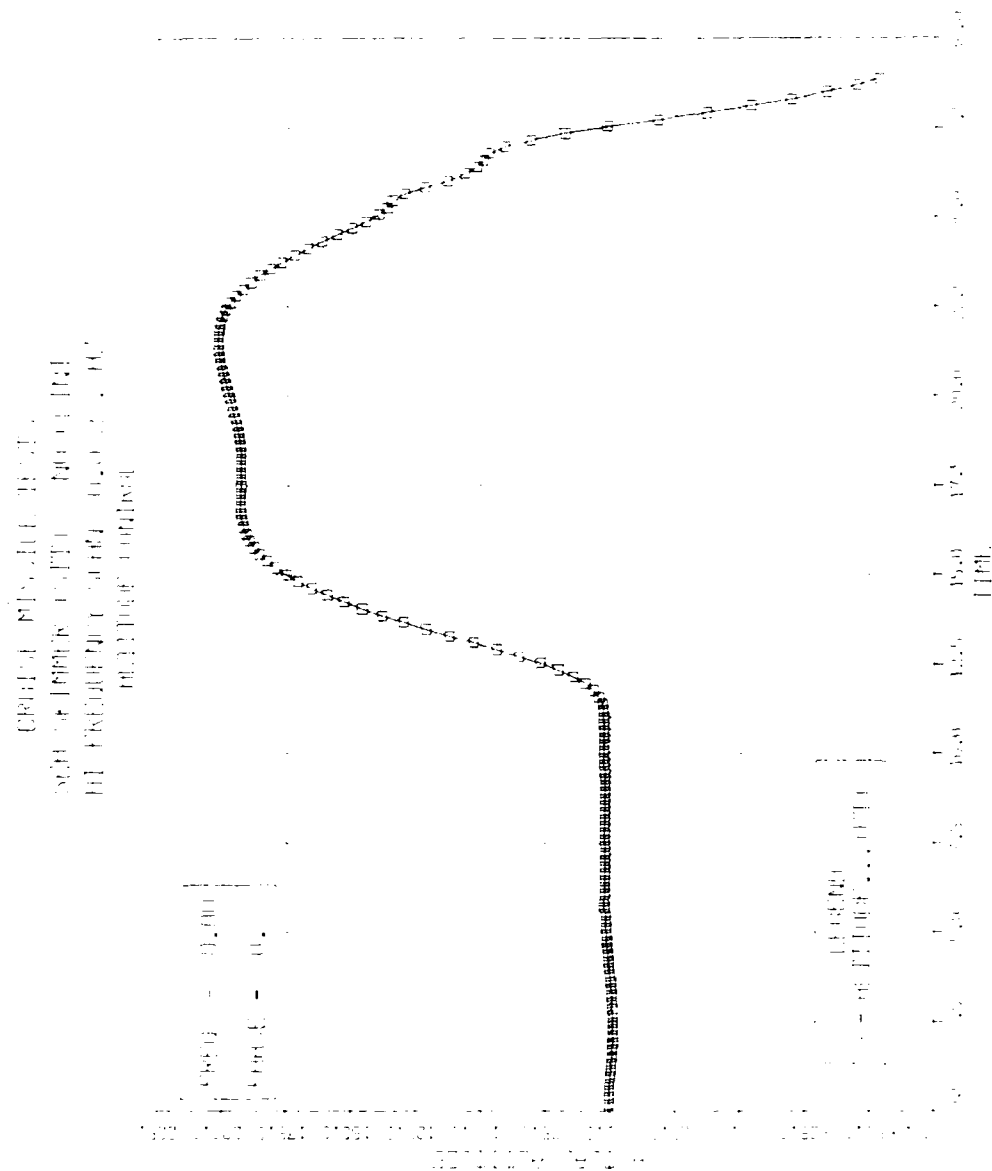


Figure A.80 Conf. V Mission Set - Altitude.

CONFIDENTIAL
 SET OF LINES - 1000
 HI FREQUENCY - 1000
 GEOMETRIC TRUCKS

1000	0.100
1000	0.

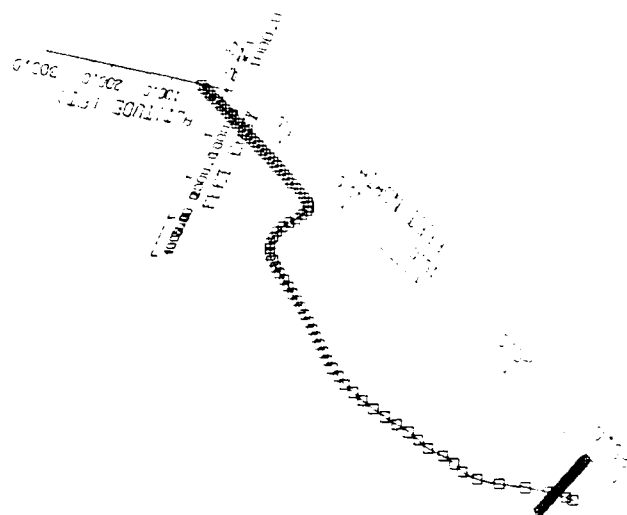


Figure A.81 Conf. V Mission Set - Geo Plot.

CONF. VI, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49, 50, 51, 52, 53, 54, 55, 56, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100, 101, 102, 103, 104, 105, 106, 107, 108, 109, 110, 111, 112, 113, 114, 115, 116, 117, 118, 119, 120, 121, 122, 123, 124, 125, 126, 127, 128, 129, 130, 131, 132, 133, 134, 135, 136, 137, 138, 139, 140, 141, 142, 143, 144, 145, 146, 147, 148, 149, 150, 151, 152, 153, 154, 155, 156, 157, 158, 159, 160, 161, 162, 163, 164, 165, 166, 167, 168, 169, 170, 171, 172, 173, 174, 175, 176, 177, 178, 179, 180, 181, 182, 183, 184, 185, 186, 187, 188, 189, 190, 191, 192, 193, 194, 195, 196, 197, 198, 199, 200, 201, 202, 203, 204, 205, 206, 207, 208, 209, 210, 211, 212, 213, 214, 215, 216, 217, 218, 219, 220, 221, 222, 223, 224, 225, 226, 227, 228, 229, 230, 231, 232, 233, 234, 235, 236, 237, 238, 239, 240, 241, 242, 243, 244, 245, 246, 247, 248, 249, 250, 251, 252, 253, 254, 255, 256, 257, 258, 259, 260, 261, 262, 263, 264, 265, 266, 267, 268, 269, 270, 271, 272, 273, 274, 275, 276, 277, 278, 279, 280, 281, 282, 283, 284, 285, 286, 287, 288, 289, 290, 291, 292, 293, 294, 295, 296, 297, 298, 299, 300, 301, 302, 303, 304, 305, 306, 307, 308, 309, 310, 311, 312, 313, 314, 315, 316, 317, 318, 319, 320, 321, 322, 323, 324, 325, 326, 327, 328, 329, 330, 331, 332, 333, 334, 335, 336, 337, 338, 339, 340, 341, 342, 343, 344, 345, 346, 347, 348, 349, 350, 351, 352, 353, 354, 355, 356, 357, 358, 359, 360, 361, 362, 363, 364, 365, 366, 367, 368, 369, 370, 371, 372, 373, 374, 375, 376, 377, 378, 379, 380, 381, 382, 383, 384, 385, 386, 387, 388, 389, 390, 391, 392, 393, 394, 395, 396, 397, 398, 399, 400, 401, 402, 403, 404, 405, 406, 407, 408, 409, 410, 411, 412, 413, 414, 415, 416, 417, 418, 419, 420, 421, 422, 423, 424, 425, 426, 427, 428, 429, 430, 431, 432, 433, 434, 435, 436, 437, 438, 439, 440, 441, 442, 443, 444, 445, 446, 447, 448, 449, 450, 451, 452, 453, 454, 455, 456, 457, 458, 459, 460, 461, 462, 463, 464, 465, 466, 467, 468, 469, 470, 471, 472, 473, 474, 475, 476, 477, 478, 479, 480, 481, 482, 483, 484, 485, 486, 487, 488, 489, 490, 491, 492, 493, 494, 495, 496, 497, 498, 499, 500, 501, 502, 503, 504, 505, 506, 507, 508, 509, 510, 511, 512, 513, 514, 515, 516, 517, 518, 519, 520, 521, 522, 523, 524, 525, 526, 527, 528, 529, 530, 531, 532, 533, 534, 535, 536, 537, 538, 539, 540, 541, 542, 543, 544, 545, 546, 547, 548, 549, 550, 551, 552, 553, 554, 555, 556, 557, 558, 559, 560, 561, 562, 563, 564, 565, 566, 567, 568, 569, 570, 571, 572, 573, 574, 575, 576, 577, 578, 579, 580, 581, 582, 583, 584, 585, 586, 587, 588, 589, 590, 591, 592, 593, 594, 595, 596, 597, 598, 599, 600, 601, 602, 603, 604, 605, 606, 607, 608, 609, 610, 611, 612, 613, 614, 615, 616, 617, 618, 619, 620, 621, 622, 623, 624, 625, 626, 627, 628, 629, 630, 631, 632, 633, 634, 635, 636, 637, 638, 639, 640, 641, 642, 643, 644, 645, 646, 647, 648, 649, 650, 651, 652, 653, 654, 655, 656, 657, 658, 659, 660, 661, 662, 663, 664, 665, 666, 667, 668, 669, 670, 671, 672, 673, 674, 675, 676, 677, 678, 679, 680, 681, 682, 683, 684, 685, 686, 687, 688, 689, 690, 691, 692, 693, 694, 695, 696, 697, 698, 699, 700, 701, 702, 703, 704, 705, 706, 707, 708, 709, 710, 711, 712, 713, 714, 715, 716, 717, 718, 719, 720, 721, 722, 723, 724, 725, 726, 727, 728, 729, 730, 731, 732, 733, 734, 735, 736, 737, 738, 739, 740, 741, 742, 743, 744, 745, 746, 747, 748, 749, 750, 751, 752, 753, 754, 755, 756, 757, 758, 759, 760, 761, 762, 763, 764, 765, 766, 767, 768, 769, 770, 771, 772, 773, 774, 775, 776, 777, 778, 779, 780, 781, 782, 783, 784, 785, 786, 787, 788, 789, 790, 791, 792, 793, 794, 795, 796, 797, 798, 799, 800, 801, 802, 803, 804, 805, 806, 807, 808, 809, 810, 811, 812, 813, 814, 815, 816, 817, 818, 819, 820, 821, 822, 823, 824, 825, 826, 827, 828, 829, 830, 831, 832, 833, 834, 835, 836, 837, 838, 839, 840, 841, 842, 843, 844, 845, 846, 847, 848, 849, 850, 851, 852, 853, 854, 855, 856, 857, 858, 859, 860, 861, 862, 863, 864, 865, 866, 867, 868, 869, 870, 871, 872, 873, 874, 875, 876, 877, 878, 879, 880, 881, 882, 883, 884, 885, 886, 887, 888, 889, 890, 891, 892, 893, 894, 895, 896, 897, 898, 899, 900, 901, 902, 903, 904, 905, 906, 907, 908, 909, 910, 911, 912, 913, 914, 915, 916, 917, 918, 919, 920, 921, 922, 923, 924, 925, 926, 927, 928, 929, 930, 931, 932, 933, 934, 935, 936, 937, 938, 939, 940, 941, 942, 943, 944, 945, 946, 947, 948, 949, 950, 951, 952, 953, 954, 955, 956, 957, 958, 959, 960, 961, 962, 963, 964, 965, 966, 967, 968, 969, 970, 971, 972, 973, 974, 975, 976, 977, 978, 979, 980, 981, 982, 983, 984, 985, 986, 987, 988, 989, 990, 991, 992, 993, 994, 995, 996, 997, 998, 999, 1000

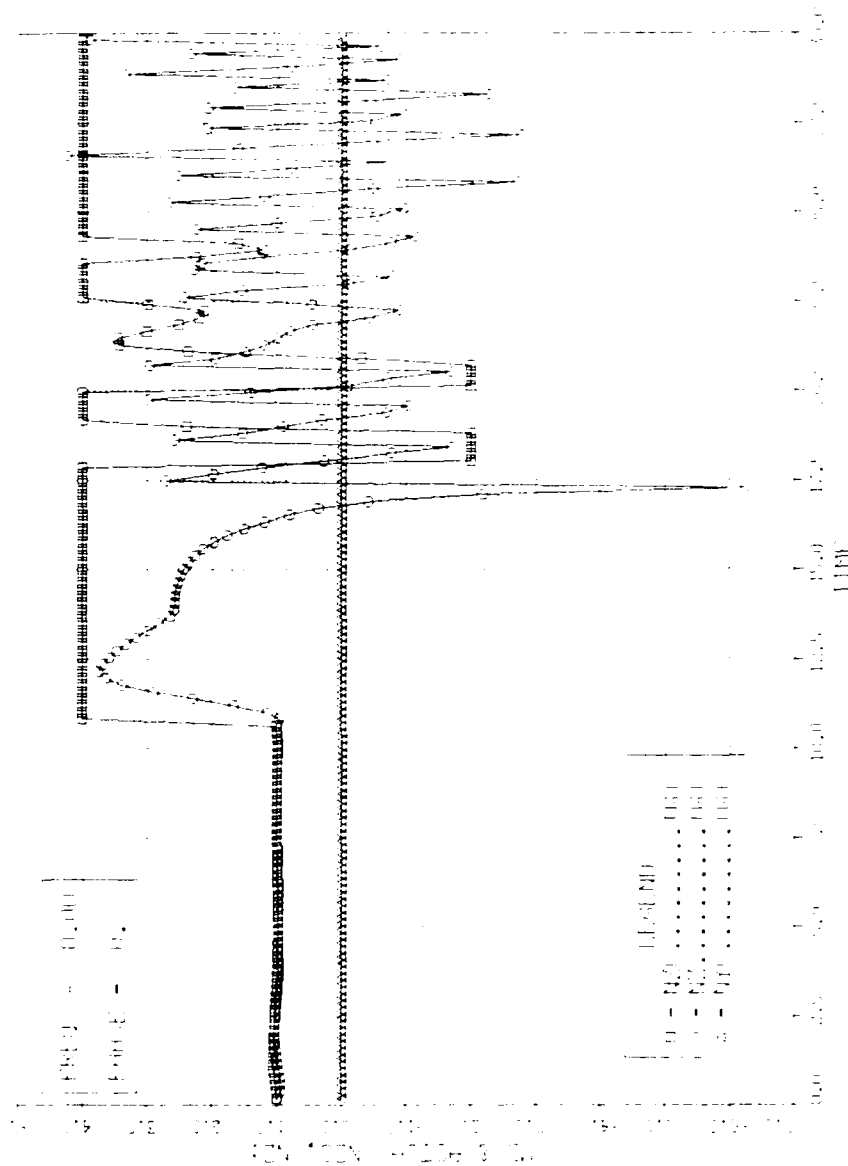


Figure A.82 Conf. VI Mission Set - Load Factor.

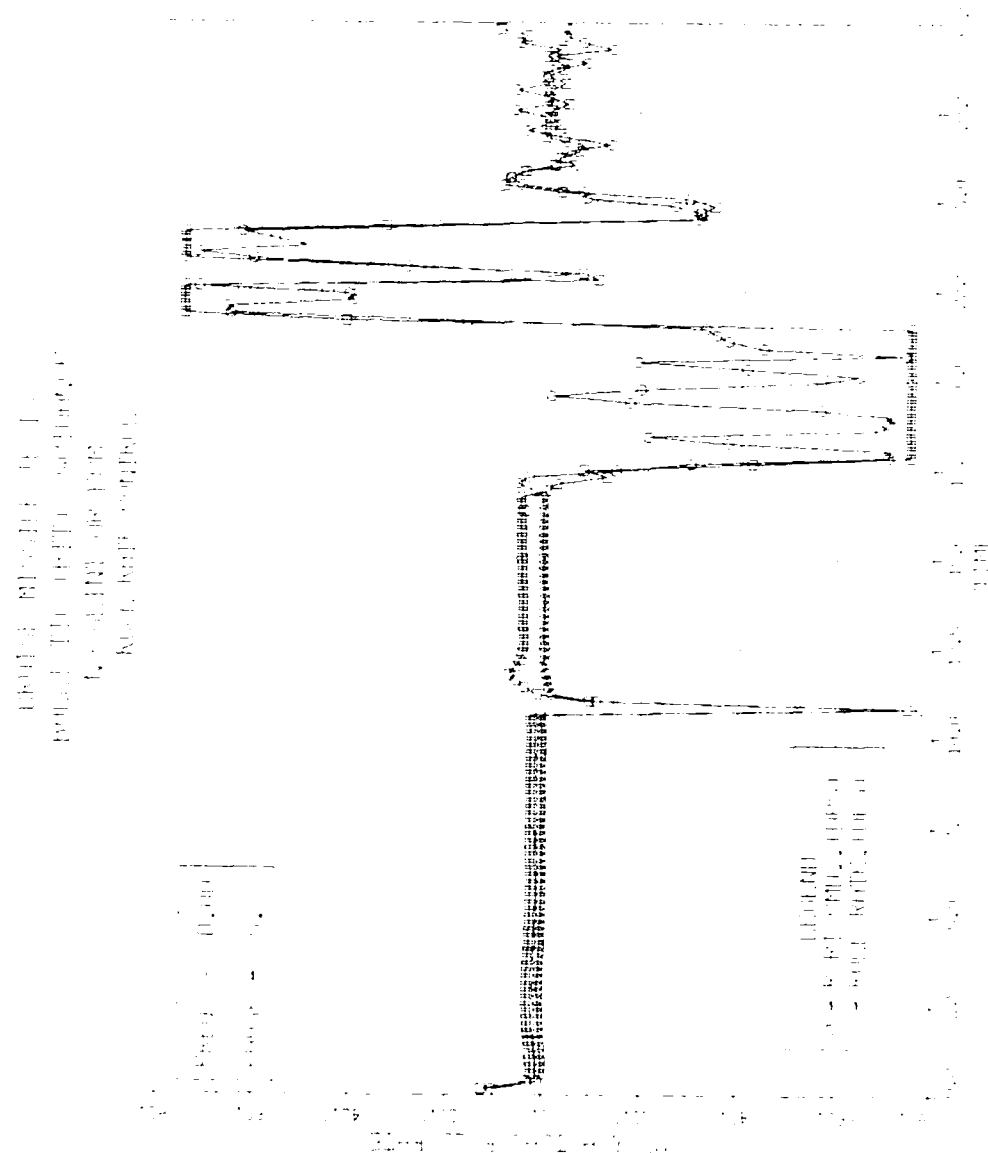


Figure A.84 Conf. VI Mission Set - Roll Rate.

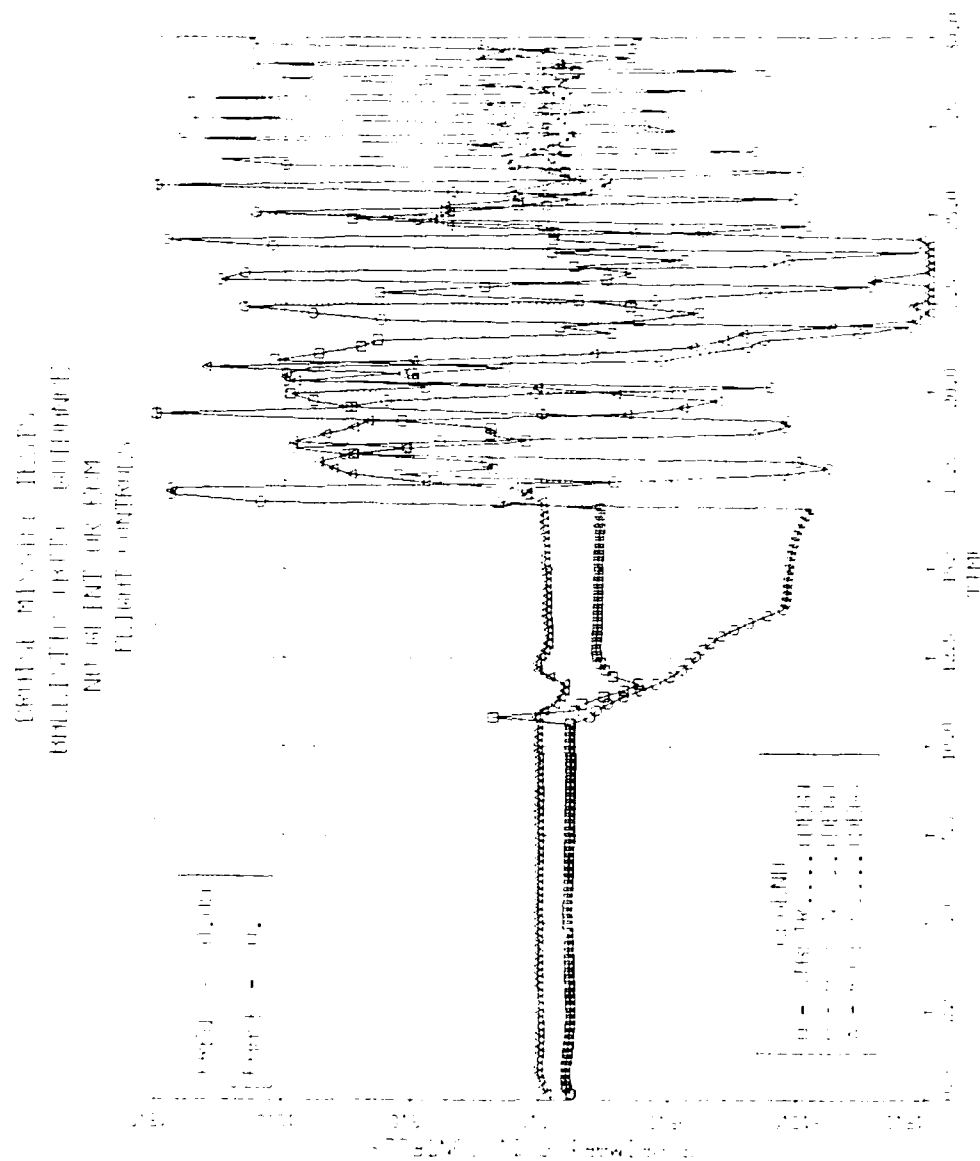


Figure A.85 Conf. VI Mission Set - Controls.

APPENDIX B

SIMULATION PROGRAM TABULAR DATA OUTPUT

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 FZ
 9-19-84

SIMULATION TERMINATED DUE TO CPA
 *** BLINKER FREQUENCY = 0.20
 *** BLINKER PHASE 0.

MISS DISTANCE	* BANK	* 0.20466	* 0.11202	* 0.03046	* ELEVATION
42.87372					0.00866

***** RANGES FOR ALL SAVED VARIABLES *****

	MINIMUM	MAXIMUM
TIME..... (SEC)	0.190000	29.061737
NZC..... (G)	0.289882	4.000000
NZ..... (G)	0.551692	3.750864
BANK..... (DEG)	-115.634293	92.840149
BANK..... (DEG)	-115.765106	84.187943
R/RT CMG..... (DPS)	-74.999985	74.999985
RCIL RATE..... (DPS)	-73.526184	73.167145
ECM SHIF..... (FT)	-75.000000	75.000000
GLINT SHIF..... (FT)	-47.524835	47.070313
STULTR..... (DLS)	-15.000000	7.934396
AIRLN..... (DEG)	-6.261881	0.000000

RUDDER.....(DEG)
 ALTITUDE.....(FT)
 XM.....(FT NORTH)
 YM.....(FT NORTH)
 XT.....(FT EAST)
 XM.....(FT EAST)
 RANCE.....(FT)
 PHASE MARKER

-3.440085
 13.361130
 159.440155
 -3.520452
 24000.000000
 6.649955
 110.888184
 0.000000

2.952714
 250.106537
 23887.324200
 1771.405030
 24000.000000
 1017.160640
 23840.589800
 4.000000

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 Hz
 9-19-84

*** BLINKER FREQUENCY=

0.20

DATA SET NUMBER 1 OF 4

TIME.....(SEC)	NZC.....(G)	NZ.....(G)	BANK.....(DEG)	BANK.....(DEG)
0.190070	*	0.996454	*	0.838765
0.380000	*	1.002067	*	6.808969
0.570000	*	1.012286	*	6.645293
0.759999	*	1.022474	*	6.546911
0.949999	*	1.030748	*	6.503017
1.139989	*	1.036386	*	6.458877
1.329975	*	1.039639	*	6.585023
1.519961	*	1.040093	*	6.806047
1.709948	*	1.038448	*	6.744779
1.899934	*	1.034911	*	6.918423
2.089920	*	1.029593	*	7.007813
2.279906	*	1.023017	*	7.091106
2.469893	*	1.015957	*	7.323308
2.659879	*	1.008910	*	7.690206
2.849865	*	1.002075	*	8.092773
3.039851	*	0.995503	*	8.427508
3.229837	*	0.989945	*	8.744263
3.419824	*	0.983682	*	8.969087
3.609810	*	0.975212	*	9.224430
3.799796	*	0.972487	*	9.405898
3.989782	*	0.970403	*	9.605278
4.179769	*	0.970192	*	9.752930
4.369755	*	0.965642	*	9.988882
5.825313	*	0.984984	*	0.838765
6.542444	*	0.939250	*	6.808969
6.510144	*	0.935853	*	6.645293
6.556442	*	0.946945	*	6.546911
6.527555	*	0.962120	*	6.503017
6.279075	*	0.977738	*	6.458877
6.320140	*	0.951862	*	6.585023
6.580812	*	1.004217	*	6.806047
6.470833	*	1.014323	*	6.744779
6.623720	*	1.021769	*	6.918423
6.747380	*	1.027047	*	7.007813
6.854517	*	1.030146	*	7.091106
7.001084	*	1.030588	*	7.323308
7.254130	*	1.028598	*	7.690206
7.688924	*	1.024992	*	8.092773
8.050653	*	1.020577	*	8.427508
8.517364	*	1.015759	*	8.744263
8.645078	*	1.010625	*	8.969087
8.392548	*	1.005136	*	9.224430
9.108009	*	0.995566	*	9.405898
9.502847	*	0.994111	*	9.605278
9.474053	*	0.988990	*	9.752930
9.074053	*	0.984181	*	9.988882

4.555741	0.969938	0.979871	10.235960	9.915122
4.745727	0.970555	0.976926	10.229715	10.058768
4.935713	0.972024	0.977490	10.223241	10.101740
5.129700	0.973334	0.977364	10.384534	10.226965
5.319686	0.974787	0.977396	10.169158	10.063795
5.509672	0.976223	0.977441	9.974529	9.865085
5.699658	0.977961	0.977467	9.844348	9.706358
5.889645	0.980385	0.977463	9.897495	9.076970
6.079631	0.982658	0.975111	9.851146	9.668716
6.269617	0.985226	0.976146	9.896841	9.074454
6.459603	0.987471	0.977097	9.856885	9.069850
6.649590	0.989611	0.977564	9.846107	9.047773
6.839576	0.991370	0.981773	9.794549	9.013314
7.029562	0.993606	0.983401	9.991575	9.700086
7.219548	0.995817	0.985411	59.999954	11.834124
7.409534	1.097366	0.983417	59.999954	24.587097
7.599521	1.299035	0.803401	59.999954	37.007508
7.789507	1.677993	0.811473	59.999954	45.419754
7.979493	2.247480	0.916378	59.999954	58.482132
8.169479	2.473261	1.204178	59.999954	59.001837
8.359466	2.579926	1.523088	59.999954	55.080084
8.549452	2.618698	1.830282	59.999954	59.036536
8.739438	2.585437	1.115276	59.999954	55.560257
8.929424	2.495302	2.347334	59.999954	59.475677
9.119411	2.347077	2.504561	59.999954	59.397044
9.309397	2.161033	2.576695	59.999954	59.342728
9.499383	1.955719	2.563868	59.999954	55.316010
9.689369	1.749104	2.477899	59.999954	55.314651
9.879355	1.557662	2.332685	59.999954	55.346558
10.069342	1.354344	2.146254	59.999954	59.401413
10.259328	1.268420	1.938939	59.999954	55.469284
10.449314	1.184954	1.730132	59.999954	55.540421
10.639300	1.144872	1.536979	59.999954	59.065598
10.829287	1.150376	1.371496	0.000000	47.870846
11.019273	0.654307	1.266437	0.000000	34.769897
11.209255	0.533505	1.138158	0.000000	21.753655
11.399245	0.404801	1.010703	0.000000	8.865244
11.589231	0.440540	0.917152	0.000000	0.877188
11.779218	0.437432	0.851573	0.000000	-0.043441

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 FZ
 9-19-84

*** BLINKER FREQUENCY=

0.20

DATA SET NUMBER 1 OF 4

TIME.....(SEC) NZC.....(G) NZ.....(G) BANK.....(DEG)

11.969204	0.450394	0.768242	0.000000	0.000000	0.161884
12.159190	0.482046	0.685690	0.000000	0.000000	0.162543
12.349176	0.5131986	0.614517	0.000000	0.000000	0.135814
12.539163	0.557679	0.565422	0.000000	0.000000	0.120245
12.729145	0.674333	0.551692	0.000000	0.000000	0.108407
12.919135	0.757205	0.557850	0.000000	0.000000	0.104236
13.109121	0.844995	0.584029	0.000000	0.000000	0.105790
13.299108	0.924948	0.626355	0.000000	0.000000	0.111587
13.489094	1.002845	0.679794	0.000000	0.000000	0.119782
13.679080	1.073686	0.738611	0.000000	0.000000	0.132744
13.869066	1.135511	0.804878	0.000000	0.000000	0.148205
14.059052	1.186506	0.874575	0.000000	0.000000	0.164887
14.249035	1.225576	0.943393	0.000000	0.000000	0.181834
14.439025	1.252302	1.009762	0.000000	0.000000	0.198240
14.629011	1.269832	1.065501	0.000000	0.000000	0.213442
14.818997	1.261657	1.123638	0.000000	0.000000	0.226920
15.008984	1.243847	1.165641	0.000000	0.000000	0.238204
15.198970	1.218340	1.203627	0.000000	0.000000	0.246988
15.388956	1.187195	1.235422	0.000000	0.000000	0.253153
15.578942	1.152465	1.234756	0.000000	0.000000	0.256717
15.768925	1.116103	1.224596	0.000000	0.000000	0.253706
15.958915	1.079892	1.182526	0.000000	0.000000	0.245153
16.148834	1.045580	1.154176	0.000000	0.000000	0.243445
16.338730	1.013837	1.123310	0.000000	0.000000	0.239122
16.528625	0.986244	1.092164	0.000000	0.000000	0.233170
16.718521	0.963268	1.063370	0.000000	0.000000	0.226391
16.908417	0.944965	1.036421	0.000000	0.000000	0.219006
17.098312	0.931297	1.011223	0.000000	0.000000	0.215910
17.288208	0.922266	0.988825	0.000000	0.000000	0.210300
17.478104	0.917679	0.965775	0.000000	0.000000	0.204210
17.667995	0.917206	0.944433	0.000000	0.000000	0.199162
17.857895	0.920379	0.935418	0.000000	0.000000	0.194973
18.047791	0.923043	0.933596	0.000000	0.000000	0.191712
18.237686	0.935383	0.931596	0.000000	0.000000	0.189403
18.427582	0.945946	0.931231	0.000000	0.000000	0.187925
18.617477	0.957685	0.933928	0.000000	0.000000	0.187027
18.807373	0.969778	0.935664	0.000000	0.000000	0.186014
18.997265	0.982247	0.935664	0.000000	0.000000	0.186014
19.187164	4.000000	0.935664	0.000000	0.000000	0.186014
19.377060			-19.212936		

TIME.....(SEC)	NZC.....(G)	NZ.....(G)	DATA SET NUMBER	1 OF 4	BANK.....(DEG)	LEG
19.56956	*	*	1.336203	*	-19.645432	*
19.56851	*	*	1.903647	*	-20.514221	*
19.946747	*	*	2.603067	*	-21.803818	*
20.136642	*	*	3.165137	*	-23.917558	*
20.326538	*	*	3.547853	*	-26.628387	*
20.516434	*	*	3.707685	*	-29.875137	*
20.706325	*	*	3.750864	*	-33.380920	*
20.896225	*	*	3.655785	*	-37.201050	*
21.086121	*	*	3.743388	*	-46.270721	*
21.276016	*	*	3.527078	*	-91.988892	*
21.465912	*	*	3.080334	*	-97.266113	*
21.655807	*	*	2.546545	*	-102.053802	*
21.845703	*	*	2.077121	*	-106.587250	*
22.035595	*	*	2.733549	*	-109.873548	*
22.225494	*	*	1.687409	*	-111.873642	*
22.415350	*	*	1.724775	*	-113.150738	*
22.605286	*	*	1.736968	*	-114.502014	*
22.795181	*	*	1.709265	*	-115.634293	*
22.985077	*	*	1.647637	*	-115.255144	*
23.174973	*	*	1.550969	*	-114.066710	*
23.364868	*	*	1.428517	*	-110.889008	*
23.554764	*	*	1.257051	*	-106.212891	*
23.744655	*	*	1.162587	*	-98.385605	*
23.934555	*	*	1.033371	*	-87.793304	*
24.124451	*	*	0.913162	*	-61.075912	*

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 9-19-84

*** BLINKER FREQUENCY= 0.20

TIME.....(SEC) NZC.....(G) NZ.....(G) BANK.....(DEG)

24.314346	*	*	0.312690	*	-41.207794	*
24.504242	*	*	0.289882	*	-12.722109	*
24.694138	*	*	0.323168	*	7.391577	*
24.884033	*	*	0.411515	*	14.987059	*
25.073925	*	*	0.560545	*	13.566058	*
25.263824	*	*	0.793154	*	11.106000	*
25.453720	*	*	1.025800	*	-68.765150	*
25.643616	*	*	1.258446	*	-56.286392	*
25.833512	*	*	1.491092	*	-43.769882	*
26.023408	*	*	1.723738	*	-31.229416	*
26.213304	*	*	1.956384	*	-18.679732	*
26.403200	*	*	2.189030	*	-6.130111	*

TIME.....(SEC)	R/RT CMD..(DPS)	ROLL RATE..(DPS)	ECM SHIFT..(FT)	GLINT SHIFT(FT)
25.453720	0.933357	0.581695	7.270296	5.453405
25.833616	1.042595	0.699352	5.325726	5.767002
25.833611	1.131395	0.796295	3.147260	3.985222
26.023407	1.231064	0.873536	2.354088	2.606244
26.213303	1.275287	0.949175	-1.190448	0.250407
26.403158	1.373239	1.020734	-1.089107	-1.234868
26.593094	1.474258	1.053145	-3.873116	-2.833504
26.782990	1.498616	1.170446	-3.584943	-3.880577
26.972885	1.534853	1.246133	-5.245676	-4.724376
27.162781	1.728691	1.302967	-1.781992	-1.055412
27.352676	2.026227	1.332957	10.870007	6.405855
27.542572	1.853992	1.533800	14.333593	8.333620
27.732468	2.105669	1.368543	48.266494	15.853433
27.922363	3.284542	1.460158	64.898895	31.915710
28.112259	4.000000	1.654933	70.102646	43.756592
28.302155	4.000000	2.015216	85.941116	55.250161
28.492050	4.000000	2.458335	92.840149	66.378754
28.681946	4.000000	2.864714	84.516556	77.037064
28.871841	4.000000	3.297837	87.914276	84.187943
29.061737	4.000000	3.747063	78.001495	81.152344

CRUISE MISSILE TESTS
BASELINE MISSION SET
GLINT PLUS ECM AT 0.2 Hz
9-19-84

*** BLINKER FREQUENCY= 0.20

DATA SET NUMBER 2 OF 4

TIME.....(SEC) R/RT CMD..(DPS) ROLL RATE..(DPS) ECM SHIFT..(FT) GLINT SHIFT(FT)

0.150000	12.067198	9.865781	-75.000000	19.921875
0.380000	2.970557	0.744763	-75.000000	47.070313
0.570000	1.389124	-0.660753	-75.000000	-43.310547
0.759995	1.571068	-0.488012	-75.000000	-25.952148
0.949999	1.868235	-0.235456	-75.000000	-15.886760
1.139985	1.916773	-0.222514	-75.000000	-47.524805
1.329975	2.881227	0.608558	-75.000000	45.671082
1.519961	2.381867	0.131125	-75.000000	-43.750000
1.709948	3.031882	0.885417	-75.000000	15.897461
1.899934	3.278272	0.850394	-75.000000	32.354405
2.089920	2.867801	0.508725	-75.000000	-27.555065

*	11.399245	*	-74.995985	*	-67.782478	*	-75.000000	*	-24.087524
*	11.589231	*	-10.854013	*	-11.366899	*	-75.000000	*	42.175767
*	11.779218	*	0.305608	*	-1.175964	*	-75.000000	*	-10.717775

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 FZ
 9-19-84

*** BLINKER FREQUENCY= 0.20

DATA SET NUMBER 2 UF 4

TIME.....(SEC) R/RT CMD..(DPS) ROLL RATE..(DPS) ECM SHIFT..(FT) GLINT SHIFT(FI)

*	11.969204	*	1.725770	*	-0.077368	*	-75.000000	*	21.820172
*	12.159190	*	1.766047	*	0.153380	*	-75.000000	*	-22.363281
*	12.345176	*	1.522800	*	0.138551	*	-75.000000	*	-15.866780
*	12.535163	*	1.307845	*	0.090493	*	75.000000	*	-47.924805
*	12.729145	*	1.175968	*	0.044148	*	75.000000	*	45.671082
*	12.919135	*	1.126412	*	0.008935	*	75.000000	*	-43.750000
*	13.109121	*	1.140405	*	-0.015377	*	75.000000	*	15.857401
*	13.299108	*	1.198962	*	-0.031489	*	75.000000	*	32.354405
*	13.485094	*	1.287829	*	-0.049077	*	75.000000	*	-27.339063
*	13.679080	*	1.425424	*	-0.068103	*	75.000000	*	-42.953164
*	13.869090	*	1.591445	*	-0.075865	*	75.000000	*	37.622070
*	14.055052	*	1.771146	*	-0.078154	*	75.000000	*	-5.271912
*	14.245039	*	1.954254	*	-0.075742	*	75.000000	*	2.807017
*	14.435025	*	2.131940	*	-0.069467	*	75.000000	*	-5.204102
*	14.625011	*	2.256958	*	-0.060213	*	75.000000	*	-0.720215
*	14.818997	*	2.436211	*	-0.048663	*	75.000000	*	33.415748
*	15.008984	*	2.568422	*	-0.035191	*	-75.000000	*	-5.082373
*	15.198970	*	2.63178	*	-0.021065	*	-75.000000	*	33.227535
*	15.388956	*	2.731251	*	-0.007072	*	-75.000000	*	-14.042664
*	15.578942	*	2.771195	*	0.006111	*	-75.000000	*	31.372070
*	15.768925	*	2.784501	*	0.017965	*	-75.000000	*	22.955322
*	15.958915	*	2.773720	*	0.028139	*	-75.000000	*	43.412781
*	16.148834	*	2.742187	*	0.036394	*	-75.000000	*	-14.065247
*	16.338730	*	2.653789	*	0.042625	*	-75.000000	*	2.099605
*	16.528625	*	2.63655	*	0.046833	*	-75.000000	*	31.255770
*	16.718521	*	2.565117	*	0.045088	*	-75.000000	*	-12.055313
*	16.908417	*	2.489133	*	0.049557	*	-75.000000	*	-26.857422
*	17.098312	*	2.414101	*	0.048846	*	-75.000000	*	-24.087524

17.288208	2.340792	0.046959	75.000000	42.173707
17.478104	2.271522	0.044037	75.000000	-10.717773
17.667999	2.208578	0.040282	75.000000	-21.826172
17.857895	2.153597	0.035907	75.000000	-22.363281
18.047791	2.107845	0.031138	75.000000	-15.886780
18.237686	2.072085	0.026206	75.000000	-47.524605
18.427582	2.046605	0.021321	75.000000	45.071082
18.617477	2.031211	0.016687	75.000000	-43.750000
18.807373	2.025372	0.012457	75.000000	19.897461
18.997265	2.028170	0.008771	75.000000	32.354405
19.187164	2.038470	0.005110	75.000000	-27.539005
19.377060	2.049985	0.001975	75.000000	-42.553104
19.566956	2.061747	0.000503	75.000000	37.622370
19.756851	2.073731	-0.000510	75.000000	-5.271912
19.946747	2.085915	-0.000510	75.000000	2.807617
20.136642	2.098354	-0.000510	75.000000	-5.204102
20.326538	2.110894	-0.000510	75.000000	-0.720215
20.516434	2.123555	-0.000510	75.000000	-33.416748
20.706329	2.136285	-0.000510	75.000000	-5.682373
20.896225	2.149028	-0.000510	75.000000	-33.227555
21.086121	2.161785	-0.000510	75.000000	-14.042604
21.276016	2.174546	-0.000510	75.000000	31.572070
21.465912	2.187313	-0.000510	75.000000	22.955222
21.655807	2.200085	-0.000510	75.000000	43.412781
21.845703	2.212856	-0.000510	75.000000	-34.065247
22.035599	2.225628	-0.000510	75.000000	2.099605
22.225494	2.238400	-0.000510	75.000000	31.255776
22.415390	2.251171	-0.000510	75.000000	-12.655515
22.605286	2.263942	-0.000510	75.000000	-28.857422
22.795181	2.276713	-0.000510	75.000000	-24.087524
22.985077	2.289484	-0.000510	75.000000	42.173707
23.174972	2.302255	-0.000510	75.000000	-10.717773
23.364868	2.315026	-0.000510	75.000000	-21.826172
23.554764	2.327797	-0.000510	75.000000	-22.363281
23.744659	2.340568	-0.000510	75.000000	-15.886780
23.934555	2.353339	-0.000510	75.000000	-47.524605
24.124451	2.366110	-0.000510	75.000000	45.071082

CRUISE MISSILE TESTS
BASELINE MISSION SET
GLINT PLUS ECM AT 0.2 HZ
9-19-84

*** BLINKER FREQUENCY= 0.20 DATA SET NUMBER 2 OF 4

TIME.....(SEC) R/RT CME...(CPS) ROLL RATE...(CPS) ECM SHIFT...(FT) GLINT SHIFT(FT)

24.314346	*	74.955985	*	65.262851	*	75.000000	*	-43.700000	*
24.504242	*	74.955985	*	65.786815	*	75.000000	*	15.997401	*
24.654138	*	74.955985	*	65.964462	*	75.000000	*	32.354405	*
24.884033	*	74.955985	*	66.055204	*	75.000000	*	-27.535065	*
25.073925	*	74.955985	*	66.085938	*	-75.000000	*	-42.953164	*
25.263824	*	74.955985	*	66.059158	*	-75.000000	*	37.622070	*
25.453720	*	22.935425	*	22.956116	*	-75.000000	*	-5.271912	*
25.643616	*	-5.669250	*	-6.440586	*	-75.000000	*	2.807617	*
25.833511	*	-10.200815	*	-10.561381	*	-75.000000	*	-9.204102	*
26.023407	*	-3.224416	*	-4.481498	*	-75.000000	*	-0.720215	*
26.213303	*	-17.724454	*	-17.331482	*	-75.000000	*	-35.416748	*
26.403198	*	-1.460428	*	-0.733393	*	-75.000000	*	-5.682373	*
26.593094	*	-12.043291	*	-13.444024	*	-75.000000	*	-33.227355	*
26.782990	*	3.221104	*	0.505555	*	-75.000000	*	-14.042664	*
26.972885	*	-7.714266	*	33.777487	*	-75.000000	*	-31.372070	*
27.162781	*	40.710358	*	33.784058	*	-75.000000	*	4.955322	*
27.352676	*	53.080215	*	44.755210	*	75.000000	*	45.412781	*
27.542572	*	66.124893	*	25.035751	*	75.000000	*	-34.065247	*
27.732468	*	74.955985	*	63.833176	*	75.000000	*	2.099605	*
27.922363	*	74.955985	*	62.675156	*	75.000000	*	31.255776	*
28.112255	*	74.955985	*	61.318130	*	75.000000	*	-12.655313	*
28.302155	*	74.955985	*	58.976955	*	75.000000	*	-28.857422	*
28.492050	*	74.955985	*	56.136641	*	75.000000	*	-24.087524	*
28.681946	*	74.955985	*	54.246460	*	0.000000	*	42.173707	*
28.871841	*	43.046890	*	24.955106	*	0.000000	*	-10.717773	*
29.061737	*	-38.403168	*	-41.171707	*	0.000000	*	21.060172	*

CRUISE MISSILE TESTS
BASELINE MISSION SET
GLINT PLUS ECM AT 0.2 HZ
9-19-84

*** BLINKER FREQUENCY= 0.20 DATA SET NUMBER 3 OF 4

TIME.....(SEC) STBLTR.....(DEG) AIRLN.....(DEG) RUDDER.....(DEG) ALTITUDE....(FT)

50.04715C
50.089844
50.075516
45.959283
45.873306
45.714288
49.541748
45.370300
49.214798
45.086792
48.954980
48.945496
48.941635
48.983841
45.069855
49.155402
49.355021
45.544617
45.756378
45.984325
50.221985
50.462909
50.701035
50.930740
51.147034
51.346406
51.520535
51.980035
51.825134
51.944421
52.044235
52.124771
52.180001
52.231140
52.260086
52.275726
52.280350
52.280088
52.150152
51.901506
51.305740
50.330307
48.955585
47.333852
45.580222
43.996101
42.555152

209445
182107
056974
005282
002556
001427
002971
002418
002201
001807
001021
000142
000528
000523
001658
003200
004216
005035
005159
005432
005113
005116
005147
005432
005884
005673
005055
005127
003851
002020
002013
002310
002783
003207
003342
003240
003310
003085
002000
002428
107497
108078
107950
107284
004178
002362

72073
095920
048470
054128
104038
125882
152071
170511
184159
193243
198301
199309
155995
189154
180487
171021
160979
150723
140201
130201
120715
112071
104602
058680
095016
052585
092353
093357
094423
095340
096312
098415
101109
104772
110800
112551
144877
065162
090855
095054
154338
647376
157528
253580
200071

179925
038112
017799
034143
055637
071321
142786
122277
177706
155317
177351
182572
228275
275705
264773
233457
233457
199722
207226
171800
172373
149561
171543
166974
108326
130142
045614
032086
037953
055715
110085
076871
110800
084154
097795
080093
164207
136593
777175
486508
941984
221276
607666
860967
228454
650789
104000

190000
380000
700000
075999
094999
139985
229975
359961
709948
899334
899200
279906
498975
658755
849865
029851
225857
419824
798100
997962
179709
355755
557541
749727
935713
129700
315086
505672
695658
889645
075651
269617
455603
645590
839576
029562
219548
409534
759521
778950
975493
169475
359406
544552
735438
925424

TIME.....(SEC)	STBLTR.....(DEG)	AILRON.....(DEG)	KODDER.....(DEG)	ALTITUDE....(FT)
9.115411	3.565754	-3.222716	0.192114	41.088508
9.309397	-3.802303	-3.287125	0.248152	41.537570
9.459383	-3.889286	-3.262568	0.364863	41.000983
9.689365	-3.815103	-3.148677	0.485630	42.413740
9.879355	-3.543250	-2.976035	0.613060	43.850743
10.069342	-3.206109	-2.761302	0.718114	45.777054
10.259328	-2.801994	-2.526126	0.790657	47.981018
10.449314	-2.403330	-2.252121	0.826747	50.565045
10.639300	-2.053359	-2.077678	0.831056	52.159927
10.829287	2.765983	-2.031552	0.837751	53.158740
11.019273	3.203503	-1.638245	0.10612	57.002005
11.209255	3.445302	-1.337570	-0.511520	60.055918
11.399245	3.550609	-1.067041	-0.603214	62.670740
11.589231	-0.761381	-0.860477	-1.135111	65.250515
11.779218	-0.606800	-0.768152	-1.088782	67.755087

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 Hz
 9-19-84

*** BLINKER FREQUENCY= 0.20

CATA SET NUMBER 3 OF 4

TIME.....(SEC) STBLTR.....(DEG) AILRON.....(DEG) KODDER.....(DEG) ALTITUDE....(FT)

11.969204	-0.915540	-0.655329	-0.792145	70.043457
12.159190	-0.818488	-0.529124	-0.461040	72.077484
12.349176	-0.699540	-0.417514	-0.218915	73.742950
12.539163	-0.612691	-0.335986	-0.095435	74.960114
12.729149	-0.56952	-0.305905	-0.054520	75.678207
12.919135	-0.557567	-0.324278	-0.055930	75.877514
13.109121	-0.575181	-0.376057	-0.073167	75.967385
13.299108	-0.611483	-0.457703	-0.095069	74.777695
13.489094	-0.661711	-0.561647	-0.110690	73.928517
13.679080	-0.739960	-0.676090	-0.125492	71.971645
13.869066	-0.826459	-0.795570	-0.138116	70.006105
14.059052	-0.917433	-0.928560	-0.148669	67.978912
14.249039	-1.006072	-1.056622	-0.156873	65.750785
14.439025	-1.094344	-1.177841	-0.162444	63.921967
14.629011	-1.177998	-1.287473	-0.165773	61.128918
14.818997	-1.244513	-1.381750	-0.165945	58.915155

* 24.124451 * -4.849390 * -0.962144 * -0.114661 * 241.418747

CRUISE MISSILE TESTS
BASELINE MISSION SET
GLINT PLUS ECM AT 0.2 HZ
9-19-84

*** BLINKER FREQUENCY= 0.20

DATA SET NUMBER 3 OF 4

TIME.....(SEC) STBLTR.....(DEG) AILRN.....(DEG) RUDDER.....(DEG) ALTITUDE....(FT)

24.314346	* * * * *	-4.733325	* * * * *	-0.741563	* * * * *	0.101332	* * * * *	235.931198
24.504242	* * * * *	-4.620466	* * * * *	-0.578142	* * * * *	0.231385	* * * * *	225.485410
24.884033	* * * * *	-4.527917	* * * * *	-0.456551	* * * * *	0.328916	* * * * *	222.255127
25.073925	* * * * *	-4.474320	* * * * *	-0.353226	* * * * *	0.322519	* * * * *	214.351547
25.263824	* * * * *	-4.457426	* * * * *	-0.346895	* * * * *	0.364436	* * * * *	205.859080
25.453720	* * * * *	-4.467105	* * * * *	-0.351945	* * * * *	0.428672	* * * * *	196.827133
25.643616	* * * * *	-4.274610	* * * * *	-0.358593	* * * * *	0.500631	* * * * *	177.284655
25.833511	* * * * *	-0.232819	* * * * *	-0.348033	* * * * *	0.558074	* * * * *	166.953583
26.023407	* * * * *	-0.198092	* * * * *	-0.756084	* * * * *	0.334308	* * * * *	156.350306
26.213303	* * * * *	-0.650840	* * * * *	-0.927217	* * * * *	0.335595	* * * * *	145.087623
26.403158	* * * * *	0.102798	* * * * *	-1.071691	* * * * *	-0.150439	* * * * *	134.929001
26.593094	* * * * *	-1.248897	* * * * *	-1.217293	* * * * *	-0.305899	* * * * *	124.194458
26.782990	* * * * *	-0.533312	* * * * *	-1.352807	* * * * *	-0.341328	* * * * *	113.584758
26.972885	* * * * *	-1.452764	* * * * *	-1.452980	* * * * *	-0.385506	* * * * *	103.123795
27.162781	* * * * *	-0.769291	* * * * *	-1.620697	* * * * *	-0.369920	* * * * *	92.954556
27.352676	* * * * *	-3.682535	* * * * *	-1.775575	* * * * *	-0.400695	* * * * *	83.127731
27.542572	* * * * *	-4.034552	* * * * *	-1.926140	* * * * *	-0.148369	* * * * *	73.705917
27.732468	* * * * *	-15.000000	* * * * *	0.000000	* * * * *	0.416052	* * * * *	64.775585
27.922363	* * * * *	-5.632820	* * * * *	-2.184797	* * * * *	0.805972	* * * * *	56.263775
28.112255	* * * * *	-6.056888	* * * * *	-2.572707	* * * * *	1.135191	* * * * *	48.184021
28.302155	* * * * *	-6.717966	* * * * *	-2.657307	* * * * *	1.294632	* * * * *	40.573837
28.492050	* * * * *	-7.838568	* * * * *	-2.994135	* * * * *	1.414780	* * * * *	33.465175
28.681946	* * * * *	-9.240601	* * * * *	-3.403696	* * * * *	1.650109	* * * * *	26.756821
28.871841	* * * * *	-10.255377	* * * * *	-3.842335	* * * * *	2.381865	* * * * *	20.155596
29.061737	* * * * *	-8.908066	* * * * *	-4.308064	* * * * *	3.952714	* * * * *	13.561156
29.251633	* * * * *	-1.385018	* * * * *	-5.175614	* * * * *			

CRUISE MISSILE TESTS
BASELINE MISSION SET

GLINT PLUS ELM AT 0.2 FZ 9-19-84

*** BLINKER FREQUENCY=

0.20

DATA SET NUMBER 4 LF 4

TIME.....(SEC) XM....(FT NORTH) YM....(FT EAST) XT....(FT NORTH) XM....(FT EAST)

0.190000	159.440155	-0.009810	*24000.000000	6.049995
0.380000	318.873291	-0.049694	*24000.000000	13.259989
0.570000	478.301758	-0.113570	*24000.000000	15.949982
0.759995	637.728271	-0.201762	*24000.000000	26.559976
0.949995	797.151011	-0.313580	*24000.000000	33.249965
1.139989	956.573486	-0.448021	*24000.000000	35.859977
1.329975	1115.991400	-0.603947	*24000.000000	46.545118
1.519961	1275.407716	-0.779674	*24000.000000	55.158655
1.709948	1434.820310	-0.973391	*24000.000000	59.848160
1.899934	1594.228760	-1.182685	*24000.000000	66.457681
2.089920	1753.632810	-1.404678	*24000.000000	73.147202
2.279906	1913.032470	-1.636795	*24000.000000	79.756707
2.469893	2072.426510	-1.876554	*24000.000000	86.446228
2.659879	2231.814940	-2.120413	*24000.000000	93.055745
2.849865	2391.157750	-2.362842	*24000.000000	99.745270
3.039851	2550.574710	-2.557082	*24000.000000	106.354791
3.229837	2709.944090	-2.816305	*24000.000000	113.044296
3.419824	2869.307860	-3.014300	*24000.000000	119.053817
3.609810	3028.665530	-3.185804	*24000.000000	126.343338
3.799796	3188.016300	-3.326302	*24000.000000	132.952855
3.989782	3347.361530	-3.432030	*24000.000000	139.042380
4.179765	3506.700200	-3.499740	*24000.000000	146.251885
4.369755	3666.032710	-3.526452	*24000.000000	152.941406
4.559741	3825.359620	-3.508787	*24000.000000	159.550927
4.749727	3984.681400	-3.443329	*24000.000000	166.240448
4.939713	4143.984370	-3.327466	*24000.000000	172.859305
5.129700	4303.257810	-3.155135	*24000.000000	179.539490
5.319686	4462.531250	-2.938205	*24000.000000	186.188955
5.509672	4621.804690	-2.666635	*24000.000000	192.838516
5.699658	4781.078120	-2.347534	*24000.000000	199.488037
5.889645	4940.351560	-1.983534	*24000.000000	206.137558
6.079631	5099.625000	-1.575941	*24000.000000	212.787075
6.269617	5258.898440	-1.125271	*24000.000000	219.436584
6.459603	5418.171870	-0.631455	*24000.000000	226.086105
6.649590	5577.444510	-0.094406	*24000.000000	232.735626

TIME.....(SEC)	XM....(FT NORTH)	YM....(FT EAST)	XI....(FT NORTH)	XM....(FT EAST)
6.839576	5736.703120	0.485856	24000.000000	255.385147
7.029562	5895.902340	1.109634	*24000.000000	246.034608
7.219548	6055.101560	1.785213	*24000.000000	252.684174
7.409534	6214.300780	2.594645	*24000.000000	259.333496
7.599521	6373.500300	3.660096	*24000.000000	265.583154
7.789507	6532.699220	5.144712	*24000.000000	272.632568
7.979493	6691.898440	7.223592	*24000.000000	279.282227
8.169479	6851.023440	10.115357	*24000.000000	285.931641
8.359466	7010.148440	14.135207	*24000.000000	292.581055
8.549452	7169.210940	19.605545	*24000.000000	299.230713
8.739438	7328.160160	26.823135	*24000.000000	305.880147
8.929424	7486.953120	36.051483	*24000.000000	312.529785
9.119411	7645.527340	47.457543	*24000.000000	319.179195
9.309397	7803.820310	61.294495	*24000.000000	325.828857
9.499383	7961.785160	77.454766	*24000.000000	332.478271
9.689369	8119.371090	96.073334	*24000.000000	339.127086
9.879355	8276.554690	116.038950	*24000.000000	345.777344
10.069342	8433.333590	139.948761	*24000.000000	352.426758
10.259328	8589.730470	164.924748	*24000.000000	359.076418
10.449314	8745.746090	191.672058	*24000.000000	365.725830
10.639300	8901.429690	219.956425	*24000.000000	372.375488
10.829287	9056.800780	249.667542	*24000.000000	379.024502
11.019273	9211.929690	280.360840	*24000.000000	385.674316
11.209259	9366.850620	311.764160	*24000.000000	392.323975
11.399245	9521.742190	343.555176	*24000.000000	398.973385
11.589231	9676.562500	375.463623	*24000.000000	405.623047
11.779218	9831.382810	407.341797	*24000.000000	412.272401

CRUISE MISSILE TESTS
BASELINE MISSION SET
GLINT PLUS ECM AT 0.2 Hz
9-19-84

*** BLINKER FREQUENCY=	0.20	DATA SET NUMBER	4	OF	4
11.965204	* 9986.203120	* 435.127930	* 24000.000000	* 418.522115	
12.159190	* 10141.523420	* 470.755654	* 24000.000000	* 425.571553	
12.349176	* 10295.845700	* 502.336670	* 24000.000000	* 432.220947	
12.539163	* 10450.663600	* 533.751709	* 24000.000000	* 438.670005	

* * *	27.732468	*22811.261700	*1137.262230	*24000.000000	* * *	970.856230
* * *	27.922363	*22964.343700	*1110.862550	*24000.000000	* * *	977.282715
* * *	28.112255	*23117.585900	*1085.108890	*24000.000000	* * *	983.528955
* * *	28.302155	*23271.027300	*1060.465970	*24000.000000	* * *	990.575195
* * *	28.452050	*23424.718700	*1037.558840	*24000.000000	* * *	997.271680
* * *	28.681946	*23578.683600	*1017.097500	*24000.000000	* * *	1003.897920
* * *	28.871841	*23732.902300	*999.782715	*24000.000000	* * *	1010.514400
* * *	29.061737	*23887.324200	*986.245850	*24000.000000	* * *	1017.160640

TASM SIMULATION PROGRAM NCMENCLATURE

[illegible]

TIME	TIME IN SECONDS	TERMINATION INTERVAL	REASON
DDT	INTEGRATION INTERVAL		
OPDT	OUTPUT		
NPTS	NUMBER OF OUTPUTS		
CCPA	FLAG SET TO INDICATE TERMINATION		
PTS	ARRAY CONTAINING ALL SAVED DATA		
NFFAZE	SETS THE PHASE APPLIED TO ECM BLINKER		
PCFRNG	SETS THE RANGE AT WHICH CLIMB IS COMMENCED		

U,V,W	BODY AXIS LINEAR VELOCITIES (FT/SEC)
UDDT,VDDT,WDDT	BODY AXIS LINEAR ACCELERATIONS
P,Q,R	BODY AXIS ANGULAR VELOCITIES (RAD/SEC)
PRCLLRT,PTCHRT,YAWRT	"
PRCLCT,CDCT,RDCT	BODY AXIS ANGULAR ACCELERATIONS
X,Y,Z	BODY AXIS AERODYNAMIC FORCES (LBS)
L,C	LIFT, DRAG AERODYNAMIC FORCES (LBS)
LA,MA,NA	BODY AXIS AERODYNAMIC MOMENTS (FT-LBS)
PPFI,THETA,SY	EULER ANGLES (RAD)
BANK,PITCH,HEADNG	" (DEG)
PPHFLCT,THEIAD,SYDDT	" RATE OF CHANGE OF
ALFA,BETA	ANGLE OF ATTACK, SLIPSIP (RAD)
ACA,SICESL	" RATE OF CHANGE OF ALPHA, BETA
ALFAUT,BETADT	FLIGHT PATH ANGLE (RAD)
GAMMA	" (DEG)
FLTPTH	LATERAL ACCELERATIONS, LOAD FACTOR (G'S)
WY,NZ	EARTH COORDINATES OF MISSILE (FT)
XXM,YM,ALTUDE	(X-M,NORTH,YM-EAST)
XMCLCT,YMDDT,HMDDT	RATES OF CHANGE OF X, Y, ALTITUDE
VT	TOTAL MISSILE VELOCITY (FT/SEC)
CFGRD,SPAN	MEAN AERODYNAMIC CHORD, SPAN (FT)
CFGRD2,SPAN2	HALF CHORD, HALF SPAN

WT,M,G
T,S
RFC
US
C--
DC--
IAX,IYV,IZZ,IXZ
IA- IK
ELE,AIL,RUD
STBLTR,AIRON,RUDDER
RSTABL,LSTABL
RSTAB,LSTAB
---I
GROSS WEIGHT, MASS, ACCEL DUE TO GRAVITY
THRUST, WING AREA
AIR DENSITY
DYNAMIC PRESSURE X WING AREA
AERODYNAMIC COEFFICIENTS
INCREMENTS IN
MOMENTS AND PRODUCTS OF INERTIA
FUNCTIONS OF
STANDARD CONTROL DEFLECTIONS (DEG)
CONTROL DEFLECTIONS WITH LIMITS
APPLIED (DEG)
TASM UNLIMITED CONTROL DEFLECTIONS (DEG)
TASM LIMITED CONTROL DEFLECTIONS (DEG)
INITIAL CONCITION

AUTCPILLOT

K---
CGARM-
E---
---LIM
---SERI
---SERC
---C
---F,---FF,---FFF
FACCF-,FDCOF-
AUTCPILLOT GAINS
ACCELEROMETER LOCATION WRT CG
COMPARATOR ERRORS
LIMITED VALUES
SERVO INPUTS
SERVO OUTPUTS
COMMANDED VALUES
FILTERED SENSOR VARIABLE
NOTCH FILTER COEFFICIENTS

GUIDANCE

AZC,AYC
XT,YT,HT
XR,YR,HR
XREC,M,YREC,M,HREC,M
XDCTR,YDCTR,HDOTR
XECM,YECM,HECM
XGLNT,YGLNT,HGLNT
RANGE
RNGECM,RGECMT
TSPEED
SYT,THETAT
HEAUT,ELEV
VTANAZ,VTANEL
TRAKAZ,TRAKEL
COMMANDED VERTICAL AND HORIZONTAL
ACCELERATIONS IN EARTH AXES (G,S)
EARTH COORDINATES OF TARGET (FT)
POSITION OF THE TARGET WRT MISSILE IN
EARTH COORDINATES (FT)
POSITION OF RADAR TARGET (XR,YR,HR WITH ECM
AND GLINT ADDED WRT MISSILE (FT)
RATES OF CHANGE OF XREC,M,YREC,M,HREC,M (FT/S)
(RELATIVE VELOCITY OF TGT WRT MISSILE)
INCR. IN TARGET RADAR POSITION DUE TO ECM
INCR. IN TARGET RADAR POSITION DUE TO GLINT
RANGE TO TARGET (FT)
RANGE TO RADAR TARGET (TGT WITH ECM+GLINT)
TARGET SPEED (FT/SEC)
HEADING, ELEV. TC TARGET FROM MISSILE (RAD)
HEADING, ELEV. TC TARGET FROM MISSILE (DEG)
COMPONENT OF RELATIVE VEL. PERPENDICULAR
TO LOS IN AZIMUTH AND ELEVATION (FT/SEC)
COMPONENT OF MISSILE VELOCITY VECTOR IN

AZIMUTH AND ELEVATION (FT/SEC)
 EARTH AZIMUTH, ELEVATION LOS ANGLES (RAD)
 EARTH AZIMUTH, ELEVATION LOS ANGLES (DEG)
 RATES OF CHANGE OF EARTH REFERENCED LOS
 (RAD/SEC)
 SAME AS ABOVE (DEG/SEC)
 FILTERED SIGDAI, SIGDET (RAD/SEC)
 FILTERED DSGCAI, CSGDET (DEG/SEC)
 PROPORTIONAL NAVIGATION CONSTANTS
 FREQUENCY OF ECM BLINKING
 DISTANCE OF ECM BLINKER FROM TARGET AIM
 POINT (FT)
 BURN-THROUGH RANGE
 AZIMUTH AND ELEVATION NAVIGATION FILTER
 CONSTANTS

SIGAZ, SIGEL
 DSGAZ, DSGEL
 SIGDAZ, SIGDEL
 DSGCAZ, DSGDEL
 SICCAF, SIGDEF
 DSGCAF, DSGDEF
 LAMCAZ, LAMDEL
 FREQ
 SFIFTY, SHIFT
 BRNTHR
 KNFAZ, KNFEL

APPENDIX D
MAIN PROGRAM LISTING
FOR
TACTICAL CRUISE MISSILE SIMULATION

TRANSLATED BY
CDR BARTEN P. ANDERSON, USN

NAVY POSTGRADUATE SCHOOL
DEPARTMENT OF AERONAUTICAL ENGINEERING
MCNTEREY, CA 95943

TRANSLATED FROM CSMP PROGRAM BY
DR. MARLE HEWETT
LCDR KENT WATTERSON, USN

9-10-84

PROGRAM TCMC

CONTROLS THE OVERALL EXECUTION OF THE SIMULATION. CALLS THE
NECESSARY SUBROUTINES, DETERMINES WHEN THE DATA MUST BE STORED
FOR OUTPUT AND WHEN THE RUN HAS COMPLETED DUE TO CPA OR FINTIM.

IMPLICIT REAL (A-Z)
INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NULT,PCOUNT,NFAZE

COMMON BLOCK /A/: MISCELLANEOUS CONSTANTS

COMMON /A/ TIME , FINTIM,DT ,CPUT ,NUT ,NPTS ,CPA ,PCOUNT,
IXX ,IYY ,RHO ,PI ,PII ,MASS ,WT ,S ,
ID ,IE ,IZZ ,IXZ ,IA ,IB ,IC ,
CHORD2,CHORD ,SPAN2,SPAN ,NFAZE ,IJ ,IK ,

COMMON BLOCK /H/: ECM/GLINT PARAMETERS

[illegible]

```

C      CALL MISSN1
C
C      *** GENERATE CONTROL MOVEMENTS: STBLTR, AILKON, RUDDER
C      CALL APILOT
C
C      *** GENERATE MISSILE MOTION AND POSITION
C      CALL AERO
C
C      *** GENERATE APPARENT RADAR TARGET POSITION & MOTION
C      CALL TGTNAV
C
C      *** STORE REQUIRED PLOT DATA IN THE PTS ARRAY.
C      IF (PCOUNT.LT.NCUT) GO TO 50
C      CALL PREPAR
C      PCOUNT = 0.0
C      5C CONTINUE
C      GC TO 10
C      10C CONTINUE
C      *** END DYNAMIC SIMULATION *****
C      *** INVOKE DISSPLA AND TABULAR OUTPUT ROUTINES
C      CALL CLTPUT(NPTS,CPA)
C      ***** TESTPATCH TO BYPASS ITERATIONS (KTEST = 1)
C      KTEST = 0
C      IF (KTEST.EQ.1) GC TO 150
C      ***** ENDTEST
C      *** ITERATE THE PHASE VARIABLE IN THE ECM PACKAGE
C      NFAZE = NFAZE + 1
C      IF (NFAZE.LE.4) GO TO 1
C      NFAZE = 1

```



```

C *** ITERATE THE BLINKER FREQUENCY
C
C      FREQ = FREQ +5.0
C      IF (FREQ-LE-30.0) GC IC 1
C      CALL CCNEPL
C
C      STOP
C      END
C
C      ***** 9-07-84 *****
C      SUBROUTINE INIT
C      *****
C      BLCCCK DATA
C      *****
C      CONTAINS DATA STATEMENTS AND ASSIGNMENT STATEMENTS FOR
C      VARIABLES NOT INITIALIZED IN THE BLCCCK DATA SUBPROGRAM BELOW.
C      ALSO REINITIALIZES INITIAL CONDITIONS FOR MORE THAN ONE RUN.
C      *****
C      IMPLICIT REAL(A-Z)
C      INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NULT,PCOUNT,NFAZE
C
C      COMMON /A/ TIME , FLWTIM,DT , CPDT , NULT , NPTS , CPA , PCOUNT,
C      * IXX , IYY , IZZ , IXXZ , IYXZ , IYXZ , IYXZ , IYXZ ,
C      * ID , IF , IF , IF , IF , IF , IF , IF , IF , IF , IF ,
C      * CHUR02,CHURC , SPAN2,SPAN ,NFAZE
C
C      COMMON /C/ KPTCHR , KROLLR , KYAWRT , CGARML , KBANK ,
C      * KRTLLM , PLIM , KNY , KNY , KNY , KNY , KNY , KNY , KNY , KNY ,
C      * ATLRON , STBLTR , RUCLLR , NYSEK , CGARML , KNY , KNY , KNY , KNY ,
C      * BSEK , NZSEK , NYSEK , NYSEK , NYSEK , NYSEK , NYSEK , NYSEK ,
C
C      COMMON /G/ ALFA , BETA , VT , W , THETA , CL , P , BETA ,
C      * U , GAMMA , CL , P , BETA , NZ , XMDLT ,
C      * CU , CM , CN , ALFADT , NZ , XMDLT ,
C      * R , QOUT , RDLT , YM ,
C      * X4
C
C      COMMON /E/ XMI , PITCHI , YMI , BANKI , ALTUOI , HELAGI ,
C      * SIUESI

```

[illegible]

```

C      NPTS = C
DU 100 I=1,300
DC 50 J=1,20
      PTS(I,J) = 0.0
      CCNTINLE
5C CONTINUE
10C
C      U = LI
      W = LI*TAN(AOAL/PII)
      V = Sqrt(U**2+W**2)*TAN(SIDESL/PII)
      VT = Sqrt(U**2+V**2)
      QS = 12.0*RH0*(VT**2)/2.0
C
C      P = RCLLRL/PII
      Q = FTCHRL/PII
      R = VAWRL/PII
C
C      PDCT = 0.0
      QDCT = 0.0
      RDOT = 0.0
C
C      THETA = PITCHI/PII
      PHI = BANKI/PII
      SY = HEDNGI/PII
      GAMMA = 0.0
      NZ = 1.0
C
C      XM = XM1
      YM = YM1
      ALTUDE = ALTUDI
C
C      AOA = ACAI
      ALFA = ACAI/PII
      ALFADT = 0.0
C
C      SICESL = SIDESI
      BETA = SIDESI/PII
      BETADT = 3.0
C
C      XT = XTI
      YT = YTI
      HT = HTI
      KANGE = Sqrt((XT-XM)**2+(YT-YM)**2+(HT-ALTUDE)**2)
C
      PHI = 0
      PH2 = C

```

[illegible]

C	*	COMMON	/A/	TIME	FINTIM,DT	OPDT	NCUT	NPTS	CPA	PCOUNT
	*		G	T	RHO	PI	PII	MASS	WT	S
	*		IXX	IYY	IZZ	IXZ	IA	IB	IC	QS
	*		ID	IE	IF	IG	IF	II	IJ	IK
	*		CHORD2,CHORD	SPAN2,SPAN	SPAN	SPAN	SPAN	SPAN	SPAN	SPAN
C	*	COMMON	/B/	LFT1(2,36)	LFT2(2,36)	DRG1(2,36)	DRG2(2,36)			
	*		DRG3(2,36)	DRG4(2,36)	DRG5(2,36)	PITCH1(2,36)	PITCH2(2,36)			
	*		SID1(6,10)	SID2(6,10)	SID3(6,10)	SID4(6,10)	SID5(6,10)			
	*		DRG2(6,10)	DRG3(6,10)	DRG4(6,10)	DRG5(6,10)	DRG6(6,10)			
	*		LTRL1(6,10)	LTRL2(6,10)	LTRL3(6,10)	LTRL4(6,10)	LTRL5(6,10)			
	*		CLQ	CLQ	CLQ	CLQ	CLQ			
	*		CYR	CYR	CYR	CYR	CYR			
	*		CNR	CNR	CNR	CNR	CNR			
C	*	COMMON	/C/	KPTCHR	KROLLR	KYAWRT	KYAWRT			
	*		KGAMMA	KALIM	KALIM	KALIM	KALIM			
	*		RRTLLIM	PLIM	PLIM	PLIM	PLIM			
	*		AIRLON	STBLTR	STBLTR	STBLTR	STBLTR			
	*		BSERO	NZSERU	NZSERU	NZSERU	NZSERU			
C	*	COMMON	/D/	ALFA	BETA	VT	VT			
	*		U	V	W	W	W			
	*		PHI	GAMMA	THETA	THETA	THETA			
	*		CD	CY	CL	CL	CL			
	*		C4	CN	P	P	P			
	*		R	ALFADT	BETADT	BETADT	BETADT			
	*		WDUT	RDCT	NZ	NZ	NZ			
	*		X4	YM	XMDCT	XMDCT	XMDCT			
C	*	COMMON	/E/	XMI	YMI	ALTUD1	ALTUD1			
	*		PITCH1	BANK1	HECAG1	HECAG1	HECAG1			
	*		ADAI	PITCHR1	RULLK1	RULLK1	RULLK1			
	*		XT1	YTI	HT1	HT1	HT1			
C	*	COMMON	/F/	PH1	PH2	PH3	PH3			
	*		CHFFSET	ALTATT	SGDPU	SGDPU	SGDPU			
	*		LAMDZ	LAMDZ	KNFAZ	KNFAZ	KNFAZ			
	*		NZC	PHIC	GAMMAC	GAMMAC	GAMMAC			
	*		PC	QC	RC	RC	RC			
	*		SIGAZ	SIGEL	SIGDAF	SIGDAF	SIGDAF			
	*		SYT	THETAT	XT	XT	XT			
	*		FT	NVC	PUPKNG	PUPKNG	PUPKNG			
C	*	COMMON	/H/	FREQ	SHIFTY	SHIFTY	SHIFTY			
	*		XECM	YECM	HECM	HECM	HECM			
	*				BRNTHK	BRNTHK	BRNTHK			
	*				XGLNT	XGLNT	XGLNT			

```

**          YGLNT      HGLNT      XTECM      YTECM      .
**          PTECM
*****
COMMON BLOCK /1/: OUTPUT ARRAY
*****
COMMON /1/ PIS(300,20),PLIN(6,7),XN(6,7),YN(6,7),TITLE(8,4),
LEG(4,20)
*

*** INITIALIZE THE DATA
*****
COMMON ELCCCK /A/: MISCELLANEOUS CONSTANTS
*****
DATA      TIME      FINTIM      DT      CPDI      /
/C.0      /30.0      /0.01      /0.20      /

DATA      G      T      RHU      PI      WT      MASS      /
/32.17      /242.3      /0.002377      /3.141593      /2200.      /68.38      /

DATA      IXX      IYY      IZZ      IXZ      S      /
/27.8      /1507.0      /1512.0      /11.7      /12.0      /

DATA      CHURD2,CHORD      SPAN2      SPAN      NFAZE      /
/0.707      /1.414      /4.2425      /8.485      /1      /

*****
COMMON ELCCCK /8/: AERODYNAMIC COEFFICIENT TABLES
*****

** STATIC AERODYNAMIC COEFFICIENTS
* 1. LIFT COEFFICIENT DATA
      A. CLBAS VS. AOA (BASIC LIFT COEFFICIENT AS A FUNCTION
        CF ANGLE OF ATTACK)
DATA LFT1/ -12.0,-0.32, -11.0,-0.29, -10.0,-0.46, -9.0,-0.57,
-8.0,-0.70, -7.0,-0.69, -6.0,-0.65, -5.0,-0.56,

```

```

*      -4.0,-0.50,      -3.0,-0.42,      -2.0,-0.30,      -1.0,-0.18,
*      0.0,0.08,        1.0,0.04,        2.0,0.15,        3.0,0.25,
*      4.0,0.38,        5.0,0.47,        6.0,0.58,        7.0,0.69,
*      8.0,0.80,        9.0,0.87,       10.0,0.98,       11.0,1.0,
*     12.0,0.04,       22*9999.0/

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CCCCC

B. DCLSTIE VS. SIBLTR (INCREMENT IN LIFT COEFFICIENT DUE TO SYMMETRIC STABILATOR DEFLECTION)

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DATA LFT2/ -15.0,-.100,      -14.0,-.097,      -13.0,-.094,      -12.0,-.090,
*      -11.0,-.084,      -10.0,-.078,      -9.0,-.071,      -8.0,-.065,
*      -7.0,-.058,      -6.0,-.048,      -5.0,-.040,      -4.0,-.032,
*      -3.0,-.024,      -2.0,-.016,      -1.0,-.008,      0.0,0.000,
*      1.0,0.008,      2.0,0.016,      3.0,0.024,      4.0,0.033,
*      5.0,0.041,      6.0,0.049,      7.0,0.057,      8.0,0.065,
*      9.0,0.073,     10.0,0.080,     11.0,0.086,     12.0,0.092,
*     13.0,0.096,     14.0,0.098,     15.0,0.100,     10*9999. /

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CCCCCCCC

* 2. DRAG COEFFICIENT DATA

A. CCBAS VS. CLBAS (BASIC DRAG COEFFICIENT AS A FUNCTION OF BASIC LIFT COEFFICIENT)

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DATA DRG1/ -9, .080,      -8, .061,      -7, .050,      -6, .042,
*      -5, .035,      -4, .031,      -3, .028,      -2, .023,
*      -1, .022,      0, .020,      0.1, .023,      0.2, .024,
*      0.3, .028,      0.4, .031,      0.5, .038,      0.6, .042,
*      0.7, .049,      0.8, .057,      0.9, .068,      1.0, .080,
*     32*9999. /

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CCCCC

B. CCBSTIE VS. SIBLTR (INCREMENT IN DRAG COEFFICIENT DUE TO SYMMETRIC STABILATOR DEFLECTION)

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DATA DRG2/ -15, .0106,      -14, .0091,      -13, .0077,      -12, .0065,
*      -10, .0044,      -9, .0036,      -8, .0028,      -7, .0022,
*      -6, .0016,      -5, .0011,      -4, .0007,      -3, .0003,
*      -2, .0001,      -1, 0.0001,      0, 0.0001,      1, .0001,
*      2, .0004,      3, .0007,      4, .0011,      5, .0015,
*      6, .0023,      7, .0030,      8, .0039,      9, .0045,
*      10, .0060,     11, .0073,     12, .0089,     13, .0106,
*     14, .0126,     15, .0146,     12*9999. /

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CCCC

C. CCBSTA VS. ALLRON (INCREMENT IN DRAG COEFFICIENT DUE TO ASYMMETRIC STABILATOR DEFLECTION)

DATA DRG3/ -15., .0120, -14., .0102, -13., .0085, -12., .0071,
 * -10., .0048, -9., .0036, -8., .0030, -7., .0023,
 * -6., .0016, -5., .0011, -4., .0007, -3., .0003,
 * -2., .0001, -1., .0000, 0., .0000, 1., .0000,
 * 2., .0017, 3., .0003, 4., .0007, 5., .0011,
 * 6., .0017, 7., .0003, 8., .0007, 9., .0011,
 * 10., .0048, 11., .0055, 12., .0030, 13., .0038,
 * 14., .0100, 15., .0120, 12*9999, 13., .0085,
 * 14., .0100, 15., .0120, 12*9999, 13., .0085,

D. DCDSTR VS. RUDDER (INCREMENT IN DRAG COEFFICIENT
 DUE TO RUDDER DEFLECTION)

DATA DRG4/ -15., .0059, -14., .0054, -13., .0048, -12., .0043,
 * -10., .0032, -9., .0027, -8., .0022, -7., .0017,
 * -6., .0013, -5., .0005, -4., .0006, -3., .0003,
 * -2., .0002, -1., .0001, 0., .0000, 1., .0001,
 * 2., .0001, 3., .0006, 4., .0009, 5., .0013,
 * 6., .0017, 7., .0022, 8., .0027, 9., .0032,
 * 10., .0037, 11., .0043, 12., .0048, 13., .0054,
 * 14., .0059, 15., .0064, 12*9999, 13., .0054,

3. PITCHING MOMENT COEFFICIENT DATA

A. CMBAS VS. ACA (BASIC PITCHING MOMENT COEFFICIENT
 AS A FUNCTION OF ANGLE OF ATTACK)

DATA PTC1/ -10., 1.13, -8., 0.80, -6., 0.50, -4., 0.31,
 * -2., 0.16, 0., 0.08, 2., -0.03, 4., -0.13,
 * 6., -0.22, 8., -0.32, 10., -0.40, 12., -0.62,
 * 14., -0.95, 16., -1.13, 18., -1.31, 20., -1.51,
 * 22., -1.71, 24., -1.91, 26., -2.11, 28., -2.31,
 * 30., -2.51, 32., -2.71, 34., -2.91, 36., -3.11,
 * 38., -3.31, 40., -3.51, 42., -3.71, 44., -3.91,
 * 46., -4.11, 48., -4.31, 50., -4.51, 52., -4.71,
 * 54., -4.91, 56., -5.11, 58., -5.31, 60., -5.51,
 * 62., -5.71, 64., -5.91, 66., -6.11, 68., -6.31,
 * 70., -6.51, 72., -6.71, 74., -6.91, 76., -7.11,
 * 78., -7.31, 80., -7.51, 82., -7.71, 84., -7.91,
 * 86., -8.11, 88., -8.31, 90., -8.51, 92., -8.71,
 * 94., -8.91, 96., -9.11, 98., -9.31, 100., -9.51,
 * 102., -9.71, 104., -9.91, 106., -10.11, 108., -10.31,
 * 110., -10.51, 112., -10.71, 114., -10.91, 116., -11.11,
 * 118., -11.31, 120., -11.51, 122., -11.71, 124., -11.91,
 * 126., -12.11, 128., -12.31, 130., -12.51, 132., -12.71,
 * 134., -12.91, 136., -13.11, 138., -13.31, 140., -13.51,
 * 142., -13.71, 144., -13.91, 146., -14.11, 148., -14.31,
 * 150., -14.51, 152., -14.71, 154., -14.91, 156., -15.11,
 * 158., -15.31, 160., -15.51, 162., -15.71, 164., -15.91,
 * 166., -16.11, 168., -16.31, 170., -16.51, 172., -16.71,
 * 174., -16.91, 176., -17.11, 178., -17.31, 180., -17.51,
 * 182., -17.71, 184., -17.91, 186., -18.11, 188., -18.31,
 * 190., -18.51, 192., -18.71, 194., -18.91, 196., -19.11,
 * 198., -19.31, 200., -19.51, 202., -19.71, 204., -19.91,
 * 206., -20.11, 208., -20.31, 210., -20.51, 212., -20.71,
 * 214., -20.91, 216., -21.11, 218., -21.31, 220., -21.51,
 * 222., -21.71, 224., -21.91, 226., -22.11, 228., -22.31,
 * 230., -22.51, 232., -22.71, 234., -22.91, 236., -23.11,
 * 238., -23.31, 240., -23.51, 242., -23.71, 244., -23.91,
 * 246., -24.11, 248., -24.31, 250., -24.51, 252., -24.71,
 * 254., -24.91, 256., -25.11, 258., -25.31, 260., -25.51,
 * 262., -25.71, 264., -25.91, 266., -26.11, 268., -26.31,
 * 270., -26.51, 272., -26.71, 274., -26.91, 276., -27.11,
 * 278., -27.31, 280., -27.51, 282., -27.71, 284., -27.91,
 * 286., -28.11, 288., -28.31, 290., -28.51, 292., -28.71,
 * 294., -28.91, 296., -29.11, 298., -29.31, 300., -29.51,
 * 302., -29.71, 304., -29.91, 306., -30.11, 308., -30.31,
 * 310., -30.51, 312., -30.71, 314., -30.91, 316., -31.11,
 * 318., -31.31, 320., -31.51, 322., -31.71, 324., -31.91,
 * 326., -32.11, 328., -32.31, 330., -32.51, 332., -32.71,
 * 334., -32.91, 336., -33.11, 338., -33.31, 340., -33.51,
 * 342., -33.71, 344., -33.91, 346., -34.11, 348., -34.31,
 * 350., -34.51, 352., -34.71, 354., -34.91, 356., -35.11,
 * 358., -35.31, 360., -35.51, 362., -35.71, 364., -35.91,
 * 366., -36.11, 368., -36.31, 370., -36.51, 372., -36.71,
 * 374., -36.91, 376., -37.11, 378., -37.31, 380., -37.51,
 * 382., -37.71, 384., -37.91, 386., -38.11, 388., -38.31,
 * 390., -38.51, 392., -38.71, 394., -38.91, 396., -39.11,
 * 398., -39.31, 400., -39.51, 402., -39.71, 404., -39.91,
 * 406., -40.11, 408., -40.31, 410., -40.51, 412., -40.71,
 * 414., -40.91, 416., -41.11, 418., -41.31, 420., -41.51,
 * 422., -41.71, 424., -41.91, 426., -42.11, 428., -42.31,
 * 430., -42.51, 432., -42.71, 434., -42.91, 436., -43.11,
 * 438., -43.31, 440., -43.51, 442., -43.71, 444., -43.91,
 * 446., -44.11, 448., -44.31, 450., -44.51, 452., -44.71,
 * 454., -44.91, 456., -45.11, 458., -45.31, 460., -45.51,
 * 462., -45.71, 464., -45.91, 466., -46.11, 468., -46.31,
 * 470., -46.51, 472., -46.71, 474., -46.91, 476., -47.11,
 * 478., -47.31, 480., -47.51, 482., -47.71, 484., -47.91,
 * 486., -48.11, 488., -48.31, 490., -48.51, 492., -48.71,
 * 494., -48.91, 496., -49.11, 498., -49.31, 500., -49.51,
 * 502., -49.71, 504., -49.91, 506., -50.11, 508., -50.31,
 * 510., -50.51, 512., -50.71, 514., -50.91, 516., -51.11,
 * 518., -51.31, 520., -51.51, 522., -51.71, 524., -51.91,
 * 526., -52.11, 528., -52.31, 530., -52.51, 532., -52.71,
 * 534., -52.91, 536., -53.11, 538., -53.31, 540., -53.51,
 * 542., -53.71, 544., -53.91, 546., -54.11, 548., -54.31,
 * 550., -54.51, 552., -54.71, 554., -54.91, 556., -55.11,
 * 558., -55.31, 560., -55.51, 562., -55.71, 564., -55.91,
 * 566., -56.11, 568., -56.31, 570., -56.51, 572., -56.71,
 * 574., -56.91, 576., -57.11, 578., -57.31, 580., -57.51,
 * 582., -57.71, 584., -57.91, 586., -58.11, 588., -58.31,
 * 590., -58.51, 592., -58.71, 594., -58.91, 596., -59.11,
 * 598., -59.31, 600., -59.51, 602., -59.71, 604., -59.91,
 * 606., -60.11, 608., -60.31, 610., -60.51, 612., -60.71,
 * 614., -60.91, 616., -61.11, 618., -61.31, 620., -61.51,
 * 622., -61.71, 624., -61.91, 626., -62.11, 628., -62.31,
 * 630., -62.51, 632., -62.71, 634., -62.91, 636., -63.11,
 * 638., -63.31, 640., -63.51, 642., -63.71, 644., -63.91,
 * 646., -64.11, 648., -64.31, 650., -64.51, 652., -64.71,
 * 654., -64.91, 656., -65.11, 658., -65.31, 660., -65.51,
 * 662., -65.71, 664., -65.91, 666., -66.11, 668., -66.31,
 * 670., -66.51, 672., -66.71, 674., -66.91, 676., -67.11,
 * 678., -67.31, 680., -67.51, 682., -67.71, 684., -67.91,
 * 686., -68.11, 688., -68.31, 690., -68.51, 692., -68.71,
 * 694., -68.91, 696., -69.11, 698., -69.31, 700., -69.51,
 * 702., -69.71, 704., -69.91, 706., -70.11, 708., -70.31,
 * 710., -70.51, 712., -70.71, 714., -70.91, 716., -71.11,
 * 718., -71.31, 720., -71.51, 722., -71.71, 724., -71.91,
 * 726., -72.11, 728., -72.31, 730., -72.51, 732., -72.71,
 * 734., -72.91, 736., -73.11, 738., -73.31, 740., -73.51,
 * 742., -73.71, 744., -73.91, 746., -74.11, 748., -74.31,
 * 750., -74.51, 752., -74.71, 754., -74.91, 756., -75.11,
 * 758., -75.31, 760., -75.51, 762., -75.71, 764., -75.91,
 * 766., -76.11, 768., -76.31, 770., -76.51, 772., -76.71,
 * 774., -76.91, 776., -77.11, 778., -77.31, 780., -77.51,
 * 782., -77.71, 784., -77.91, 786., -78.11, 788., -78.31,
 * 790., -78.51, 792., -78.71, 794., -78.91, 796., -79.11,
 * 798., -79.31, 800., -79.51, 802., -79.71, 804., -79.91,
 * 806., -80.11, 808., -80.31, 810., -80.51, 812., -80.71,
 * 814., -80.91, 816., -81.11, 818., -81.31, 820., -81.51,
 * 822., -81.71, 824., -81.91, 826., -82.11, 828., -82.31,
 * 830., -82.51, 832., -82.71, 834., -82.91, 836., -83.11,
 * 838., -83.31, 840., -83.51, 842., -83.71, 844., -83.91,
 * 846., -84.11, 848., -84.31, 850., -84.51, 852., -84.71,
 * 854., -84.91, 856., -85.11, 858., -85.31, 860., -85.51,
 * 862., -85.71, 864., -85.91, 866., -86.11, 868., -86.31,
 * 870., -86.51, 872., -86.71, 874., -86.91, 876., -87.11,
 * 878., -87.31, 880., -87.51, 882., -87.71, 884., -87.91,
 * 886., -88.11, 888., -88.31, 890., -88.51, 892., -88.71,
 * 894., -88.91, 896., -89.11, 898., -89.31, 900., -89.51,
 * 902., -89.71, 904., -89.91, 906., -90.11, 908., -90.31,
 * 910., -90.51, 912., -90.71, 914., -90.91, 916., -91.11,
 * 918., -91.31, 920., -91.51, 922., -91.71, 924., -91.91,
 * 926., -92.11, 928., -92.31, 930., -92.51, 932., -92.71,
 * 934., -92.91, 936., -93.11, 938., -93.31, 940., -93.51,
 * 942., -93.71, 944., -93.91, 946., -94.11, 948., -94.31,
 * 950., -94.51, 952., -94.71, 954., -94.91, 956., -95.11,
 * 958., -95.31, 960., -95.51, 962., -95.71, 964., -95.91,
 * 966., -96.11, 968., -96.31, 970., -96.51, 972., -96.71,
 * 974., -96.91, 976., -97.11, 978., -97.31, 980., -97.51,
 * 982., -97.71, 984., -97.91, 986., -98.11, 988., -98.31,
 * 990., -98.51, 992., -98.71, 994., -98.91, 996., -99.11,
 * 998., -99.31, 1000., -99.51, 1002., -99.71, 1004., -99.91,
 * 1006., -100.11, 1008., -100.31, 1010., -100.51, 1012., -100.71,
 * 1014., -100.91, 1016., -101.11, 1018., -101.31, 1020., -101.51,
 * 1022., -101.71, 1024., -101.91, 1026., -102.11, 1028., -102.31,
 * 1030., -102.51, 1032., -102.71, 1034., -102.91, 1036., -103.11,
 * 1038., -103.31, 1040., -103.51, 1042., -103.71, 1044., -103.91,
 * 1046., -104.11, 1048., -104.31, 1050., -104.51, 1052., -104.71,
 * 1054., -104.91, 1056., -105.11, 1058., -105.31, 1060., -105.51,
 * 1062., -105.71, 1064., -105.91, 1066., -106.11, 1068., -106.31,
 * 1070., -106.51, 1072., -106.71, 1074., -106.91, 1076., -107.11,
 * 1078., -107.31, 1080., -107.51, 1082., -107.71, 1084., -107.91,
 * 1086., -108.11, 1088., -108.31, 1090., -108.51, 1092., -108.71,
 * 1094., -108.91, 1096., -109.11, 1098., -109.31, 1100., -109.51,
 * 1102., -109.71, 1104., -109.91, 1106., -110.11, 1108., -110.31,
 * 1110., -110.51, 1112., -110.71, 1114., -110.91, 1116., -111.11,
 * 1118., -111.31, 1120., -111.51, 1122., -111.71, 1124., -111.91,
 * 1126., -112.11, 1128., -112.31, 1130., -112.51, 1132., -112.71,
 * 1134., -112.91, 1136., -113.11, 1138., -113.31, 1140., -113.51,
 * 1142., -113.71, 1144., -113.91, 1146., -114.11, 1148., -114.31,
 * 1150., -114.51, 1152., -114.71, 1154., -114.91, 1156., -115.11,
 * 1158., -115.31, 1160., -115.51, 1162., -115.71, 1164., -115.91,
 * 1166., -116.11, 1168., -116.31, 1170., -116.51, 1172., -116.71,
 * 1174., -116.91, 1176., -117.11, 1178., -117.31, 1180., -117.51,
 * 1182., -117.71, 1184., -117.91, 1186., -118.11, 1188., -118.31,
 * 1190., -118.51, 1192., -118.71, 1194., -118.91, 1196., -119.11,
 * 1198., -119.31, 1200., -119.51, 1202., -119.71, 1204., -119.91,
 * 1206., -120.11, 1208., -120.31, 1210., -120.51, 1212., -120.71,
 * 1214., -120.91, 1216., -121.11, 1218., -121.31, 1220., -121.51,
 * 1222., -121.71, 1224., -121.91, 1226., -122.11, 1228., -122.31,
 * 1230., -122.51, 1232., -122.71, 1234., -122.91, 1236., -123.11,
 * 1238., -123.31, 1240., -123.51, 1242., -123.71, 1244., -123.91,
 * 1246., -124.11, 1248., -124.31, 1250., -124.51, 1252., -124.71,
 * 1254., -124.91, 1256., -125.11, 1258., -125.31, 1260., -125.51,
 * 1262., -125.71, 1264., -125.91, 1266., -126.11, 1268., -126.31,
 * 1270., -126.51, 1272., -126.71, 1274., -126.91, 1276., -127.11,
 * 1278., -127.31, 1280., -127.51, 1282., -127.71, 1284., -127.91,
 * 1286., -128.11, 1288., -128.31, 1290., -128.51, 1292., -128.71,
 * 1294., -128.91, 1296., -129.11, 1298., -129.31, 1300., -129.51,
 * 1302., -129.71, 1304., -129.91, 1306., -130.11, 1308., -130.31,
 * 1310., -130.51, 1312., -130.71, 1314., -130.91, 1316., -131.11,
 * 1318., -131.31, 1320., -131.51, 1322., -131.71, 1324., -131.91,
 * 1326., -132.11, 1328., -132.31, 1330., -132.51, 1332., -132.71,
 * 1334., -132.91, 1336., -133.11, 1338., -133.31, 1340., -133.51,
 * 1342., -133.71, 1344., -133.91, 1346., -134.11, 1348., -134.31,
 * 1350., -134.51, 1352., -134.71, 1354., -134.91, 1356., -135.11,
 * 1358., -135.31, 1360., -135.51, 1362., -135.71, 1364., -135.91,
 * 1366., -136.11, 1368., -136.31, 1370., -136.51, 1372., -136.71,
 * 1374., -136.91, 1376., -137.11, 1378., -137.31, 1380., -137.51,
 * 1382., -137.71, 1384., -137.91, 1386., -138.11, 1388., -138.31,
 * 1390., -138.51, 1392., -138.71, 1394., -138.91, 1396., -139.11,
 * 1398., -139.31, 1400., -139.51, 1402., -139.71, 1404., -139.91,
 * 1406., -140.11, 1408., -140.31, 1410., -140.51, 1412., -140.71,
 * 1414., -140.91, 1416., -141.11, 1418., -141.31, 1420., -141.51,
 * 1422., -141.71, 1424., -141.91, 1426., -142.11, 1428., -142.31,
 * 1430., -142.51, 1432., -142.71, 1434., -142.91, 1436., -143.11,
 * 1438., -143.31, 1440., -143.51, 1442., -143.71, 1444., -143.91,
 * 1446., -144.11, 1448., -144.31, 1450., -144.51, 1452., -144.71,
 * 1454., -144.91, 1456., -145.11, 1458., -145.31, 1460., -145.51,
 * 1462., -145.71, 1464., -145.91, 1466., -146.11, 1468., -146.31,
 * 1470., -146.51, 1472., -146.71, 1474., -146.91, 1476., -147.11,
 * 1478., -147.31, 1480., -147.51, 1482., -147.71, 1484., -147.91,
 * 1486., -148.11, 1488., -148.31, 1490., -148.51, 1492., -148.71,
 * 1494., -148.91, 1496., -149.11, 1498., -149.31, 1500., -149.51,
 * 1502., -149.71, 1504., -149.91, 1506., -150.11, 1508., -150.31,
 * 1510., -150.51, 1512., -150.71, 1514., -150.91, 1516., -151.11,
 * 1518., -151.31, 1520., -151.51, 1522., -151.71, 1524., -151.91,
 * 1526., -152.11, 1528., -152.31, 1530., -152.51, 1532., -152.71,
 * 1534., -152.91, 1536., -153.11, 1538., -153.31, 1540., -153.51,
 * 1542., -153.71, 1544., -153.91, 1546., -154.11, 1548., -154.31,
 * 1550., -154.51, 1552., -154.71, 1554., -154.91, 1556., -155.11,
 * 1558., -155.31, 1560., -155.51, 1562., -155.71, 1564., -155.91,
 * 1566., -156.11, 1568., -156.31, 1570., -156.51, 1572., -156.71,
 * 1574., -156.91, 1576., -157.11, 1578., -157.31, 1580., -157.51,
 * 1582., -157.71, 1584., -157.91, 1586., -158.11, 1588., -158.31,
 * 1590., -158.51, 1592., -158.71, 1594., -158.91, 1596., -159.11,
 * 1598., -159.31, 1600., -159.51, 1602., -159.71, 1604., -159.91,
 * 1606., -160.11, 1608., -160.31, 1610., -160.51, 1612., -160.71,
 * 1614., -160.91, 1616., -161.11, 1618., -161.31, 1620., -161.51,
 * 1622., -161.71, 1624., -161.91, 1626., -162.11, 1628., -162.31,

C

```

DATA DREC1/ 0.0, -8.0, 2.0, 5.0, 8.0, 9999.
-15.0, -0.90, -.097, -.095, -.102, 9999.
-10.0, -.060, -.062, -.062, -.069, 9999.
-5.0, -.332, -.036, -.037, -.042, 9999.
0.0, .004, -.003, -.003, -.003, 9999.
5.0, .040, .042, .038, .034, 9999.
10.0, .070, .066, .062, .066, 9999.
15.0, .100, .098, .092, .096, 9999.
* 12*99999.

```

C C C C C C

B. DCNSTR VS. RUDDER AND AGA (INCREMENT IN YAWING MOMENT
COEFFICIENT DUE TO RUDDER DEFLECTION AND PARAMETER
ANGLE OF ATTACK)

```

DATA DREC2/ 0.0, -8.0, 2.0, 6.0, 8.0, 9999.
-15.0, -.070, .068, .062, .065, 9999.
-10.0, .050, .049, .048, .048, 9999.
-5.0, .026, .024, .022, .018, 9999.
0.0, .000, .000, .000, .000, 9999.
5.0, -.022, -.023, -.018, -.014, 9999.
10.0, -.052, -.048, -.047, -.046, 9999.
15.0, -.080, -.079, -.074, -.075, 9999.
* 12*99999.

```

C C C C C C

C. DCRSTR VS. RUDDER AND AGA (INCREMENT IN ROLLING MOMENT
COEFFICIENT DUE TO RUDDER DEFLECTION AND PARAMETER
ANGLE OF ATTACK)

```

DATA DREC3/ 0.0, -8.0, 2.0, 4.0, 6.0, 9999.
-15.0, -.050, -.0038, -.0032, -.0022, 8.0
-10.0, -.034, -.0029, -.0026, -.0020, -.0002
-5.0, -.018, -.0018, -.0018, -.0014, -.0004
0.0, .0004, .0000, .0003, .0008, -.0013
5.0, .0024, .0012, .0004, .0005, -.0014
10.0, .0048, .0028, .0018, .0000, -.0016
15.0, .0070, .0053, .0040, .0012, -.0025
* 12*99999.

```

C C C C C C C C

* 6. LATERAL CONTROL COEFFICIENT DATA

A. CCYSTA VS. ALLRON AND AGA (INCREMENT IN SIDE FORCE
COEFFICIENT DUE TO ASYMMETRIC STABILATOR DEFLECTION AND
PARAMETER ANGLE OF ATTACK)

```

DATA LTRL1/ 0.0, -8.0, -1.0, 4.0, 10.0, 9999.
-15.0, -0.15, -0.19, -0.17, -0.00, 9999.
-10.0, -0.10, -0.14, -0.10, -0.02, 9999.
-5.0, -0.05, -0.09, -0.02, -0.01, 9999.
0.0, -0.00, -0.07, -0.07, -0.18, 9999.
5.0, -0.05, -0.02, -0.03, -0.26, 9999.
10.0, -0.05, -0.02, -0.14, -0.03, 9999.
15.0, -0.10, -0.09, -0.20, -0.33, 9999.
12*99999. / -0.042, 9999.

```

B. CONSTA VS. AIRLON AND AOA (INCREMENT IN YAWING MUMENT
COEFFICIENT DUE TO ASYMETRIC STABILATOR DEFLECTION AND
PARAMETER ANGLE OF ATTACK)

```

DATA LTRL2/ 0.0, -8.0, -4.0, 0.0, 4.0, 8.0,
-15.0, -0.075, -0.050, -0.00, -0.075, -0.120,
-10.0, -0.040, -0.030, -0.00, -0.050, -0.085,
-5.0, -0.015, -0.020, -0.00, -0.025, -0.060,
0.0, -0.00, -0.010, -0.00, -0.008, -0.020,
5.0, -0.070, -0.030, -0.00, -0.025, -0.050,
10.0, -0.120, -0.045, -0.00, -0.040, -0.120,
15.0, -0.175, -0.070, -0.00, -0.070, -0.175,
12*99999. /

```

C. QCRSTA VS. AIRLON AND AOA (INCREMENT IN ROLLING MUMENT
COEFFICIENT DUE TO ASYMETRIC STABILATOR DEFLECTION AND
PARAMETER ANGLE OF ATTACK)

```

DATA LTRL3/ 0.0, -8.0, -4.0, 0.0, 4.0, 8.0,
-15.0, -0.087, -0.056, -0.00, -0.092, -0.084,
-10.0, -0.060, -0.066, -0.00, -0.064, -0.058,
-5.0, -0.030, -0.033, -0.00, -0.030, -0.030,
0.0, -0.004, -0.004, -0.00, -0.003, -0.000,
5.0, -0.012, -0.024, -0.00, -0.030, -0.020,
10.0, -0.030, -0.056, -0.00, -0.072, -0.047,
15.0, -0.050, -0.080, -0.00, -0.092, -0.067,
12*99999. /

```

2. DYNAMIC STABILITY DERIVATIVES

```

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CL366 / 1825.0, CL366, CMAUT,
CL367 / 1830.0, CL367, CMAUT,
CL368 / 1835.0, CL368, CMAUT,
CL369 / 1840.0, CL369, CMAUT,
CL370 / 1845.0, CL370, CMAUT,
CL371 / 1850.0, CL371, CMAUT,
CL372 / 1855.0, CL372, CMAUT,
CL373 / 1860.0, CL373, CMAUT,
CL374 / 1865.0, CL374, CMAUT,
CL375 / 1870.0, CL375, CMAUT,
CL376 / 1875.0, CL376, CMAUT,
CL377 / 1880.0, CL377, CMAUT,
CL378 / 1885.0, CL378, CMAUT,
CL379 / 1890.0, CL379, CMAUT,
CL380 / 1895.0, CL380, CMAUT,
CL381 / 1900.0, CL381, CMAUT,
CL382 / 1905.0, CL382, CMAUT,
CL383 / 1910.0, CL383, CMAUT,
CL384 / 1915.0, CL384, CMAUT,
CL385 / 1920.0, CL385, CMAUT,
CL386 / 1925.0, CL386, CMAUT,
CL387 / 1930.0, CL387, CMAUT,
CL388 / 1935.0, CL388, CMAUT,
CL389 / 1940.0, CL389, CMAUT,
CL390 / 1945.0, CL390, CMAUT,
CL391 / 1950.0, CL391, CMAUT,
CL392 / 1955.0, CL392, CMAUT,
CL393 / 1960.0, CL393, CMAUT,
CL394 / 1965.0, CL394, CMAUT,
CL395 / 1970.0, CL395, CMAUT,
CL396 / 1975.0, CL396, CMAUT,
CL397 / 1980.0, CL397, CMAUT,
CL398 / 1985.0, CL398, CMAUT,
CL399 / 1990.0, CL399, CMAUT,
CL400 / 1995.0, CL400, CMAUT,
CL401 / 2000.0, CL401, CMAUT,
CL402 / 2005.0, CL402, CMAUT,
CL403 / 2010.0, CL403, CMAUT,
CL404 / 2015.0, CL404, CMAUT,
CL405 / 2020.0, CL405, CMAUT,
CL406 / 2025.0, CL406, CMAUT,
CL407 / 2030.0, CL407, CMAUT,
CL408 / 2035.0, CL408, CMAUT,
CL409 / 2040.0, CL409, CMAUT,
CL410 / 2045.0, CL410, CMAUT,
CL411 / 2050.0, CL411, CMAUT,
CL412 / 2055.0, CL412, CMAUT,
CL413 / 2060.0, CL413, CMAUT,
CL414 / 2065.0, CL414, CMAUT,
CL415 / 2070.0, CL415, CMAUT,
CL416 / 2075.0, CL416, CMAUT,
CL417 / 2080.0, CL417, CMAUT,
CL418 / 2085.0, CL418, CMAUT,
CL419 / 2090.0, CL419, CMAUT,
CL420 / 2095.0, CL420, CMAUT,
CL421 / 2100.0, CL421, CMAUT,
CL422 / 2105.0, CL422, CMAUT,
CL423 / 2110.0, CL423, CMAUT,
CL424 / 2115.0, CL424, CMAUT,
CL425 / 2120.0, CL425, CMAUT,
CL426 / 2125.0, CL426, CMAUT,
CL427 / 2130.0, CL427, CMAUT,
CL428 / 2135.0, CL428, CMAUT,
CL429 / 2140.0, CL429, CMAUT,
CL430 / 2145.0, CL430, CMAUT,
CL431 / 2150.0, CL431, CMAUT,
CL432 / 2155.0, CL432, CMAUT,
CL433 / 2160.0, CL433, CMAUT,
CL434 / 2165.0, CL434, CMAUT,
CL435 / 2170.0, CL435, CMAUT,
CL436 / 2175.0, CL436, CMAUT,
CL437 / 2180.0, CL437, CMAUT,
CL438 / 2185.0, CL438, CMAUT,
CL439 / 2190.0, CL439, CMAUT,
CL440 / 2195.0, CL440, CMAUT,
CL441 / 2200.0, CL441, CMAUT,
CL442 / 2205.0, CL442, CMAUT,
CL443 / 2210.0, CL443, CMAUT,
CL444 / 2215.0, CL444, CMAUT,
CL445 / 2220.0, CL445, CMAUT,
CL446 / 2225.0, CL446, CMAUT,
CL447 / 2230.0, CL447, CMAUT,
CL448 / 2235.0, CL448, CMAUT,
CL449 / 2240.0, CL449, CMAUT,
CL450 / 2245.0, CL450, CMAUT,
CL451 / 2250.0, CL451, CMAUT,
CL452 / 2255.0, CL452, CMAUT,
CL453 / 2260.0, CL453, CMAUT,
CL454 / 2265.0, CL454, CMAUT,
CL455 / 2270.0, CL455, CMAUT,
CL456 / 2275.0, CL456, CMAUT,
CL457 / 2280.0, CL457, CMAUT,
CL458 / 2285.0, CL458, CMAUT,
CL459 / 2290.0, CL459, CMAUT,
CL460 / 2295.0, CL460, CMAUT,
CL461 / 2300.0, CL461, CMAUT,
CL462 / 2305.0, CL462, CMAUT,
CL463 / 2310.0, CL463, CMAUT,
CL464 / 2315.0, CL464, CMAUT,
CL465 / 2320.0, CL465, CMAUT,
CL466 / 2325.0, CL466, CMAUT,
CL467 / 2330.0, CL467, CMAUT,
CL468 / 2335.0, CL468, CMAUT,
CL469 / 2340.0, CL469, CMAUT,
CL470 / 2345.0, CL470, CMAUT,
CL471 / 2350.0, CL471, CMAUT,
CL472 / 2355.0, CL472, CMAUT,
CL473 / 2360.0, CL473, CMAUT,
CL474 / 2365.0, CL474, CMAUT,
CL475 / 2370.0, CL475, CMAUT,
CL476 / 2375.0, CL476, CMAUT,
CL477 / 2380.0, CL477, CMAUT,
CL478 / 2385.0, CL478, CMAUT,
CL479 / 2390.0, CL479, CMAUT,
CL480 / 2395.0, CL480, CMAUT,
CL481 / 2400.0, CL481, CMAUT,
CL482 / 2405.0, CL482, CMAUT,
CL483 / 2410.0, CL483, CMAUT,
CL484 / 2415.0, CL484, CMAUT,
CL485 / 2420.0, CL485, CMAUT,
CL486 / 2425.0, CL486, CMAUT,
CL487 / 2430.0, CL487, CMAUT,
CL488 / 2435.0, CL488, CMAUT,
CL489 / 2440.0, CL489, CMAUT,
CL490 / 2445.0, CL490, CMAUT,
CL491 / 2450.0, CL491, CMAUT,
CL492 / 2455.0, CL492, CMAUT,
CL493 / 2460.0, CL493, CMAUT,
CL494 / 2465.0, CL494, CMAUT,
CL495 / 2470.0, CL495, CMAUT,
CL496 / 2475.0, CL496, CMAUT,
CL497 / 2480.0, CL497, CMAUT,
CL498 / 2485.0, CL498, CMAUT,
CL499 / 2490.0, CL49
```

```

* /0.0 /0.15 /,
* CFP /0.4 /,CNR /,
* /0.2 /,CNP /,
* CFP /-0.1 /,CYBDT /,
* /-0.4 /-0.1 /

```

CCCCCCCC

```

*****
COMMON BLOCK /C/: CONTROL SYSTEM PARAMETERS
*****

```

*** CONTROL SYSTEM PARAMETERS

```

DATA      KPTCHR      KROLLR      KYAWRT      KBAWK
* /0.28 /0.10 /0.40 /10.8 /,
* KGAMMA /1.0 /0.3 /CGARML /CGARMIN /,
* /RT LIM /KNY /KNZ /0.05/
* /75.0 /

```

CCCCCCCC

```

*****
COMMON BLOCK /E/: INITIAL CONDITIONS
*****

```

*** MISSILE INITIAL CONDITIONS

```

DATA      XM1      YM1      ALTUD1
* /0.0 /0.0 /50.0 /,
DATA      PITCH1      BANK1      HEDNG1
* /3.00 /0.0 /0.0 /,
DATA      AUA1      PTCHR1      ROLLR1
* /3.00 /0.0 /0.0 /,

```

CCCCC

*** TARGET INITIAL CONDITIONS

```

DATA      XT1      YTI      HT1
* /24000.0 /0.0 /10.0 /,

```

CCCCC

```

*****
COMMON BLOCK /F/: GUIDANCE PARAMETERS
*****

```

```

*****
*** PROPORTIONAL NAVIGATION & NAV FILTER CONSTANTS (AZIMUTH & ELEV.)
DATA      LAMDAZ      ,LAMDEL      ,KNFAZ      ,KNFEL
*          /3.15      ,/3.85      ,/0.8        ,/0.50 /

*** MISSION PHASE FLAGS & DECISION PARAMETERS
DATA      PH1        ,PH2        ,PH3        ,PH4
*          /0         ,/0         ,/0         ,/0
DATA      CFFSET      ,ALIAIT      ,SGDZPU      ,MISDST
*          /10.0      ,/200.0     ,/1.12      ,/0.0 /

*****
COMMON ELCCCK /H/: ECM/GLINT PARAMETERS
*****

DATA      FREQ        ,SHIFT      ,SHIFTH      ,BRNTHR
*          /0.00      ,/75.0     ,/10.0      ,/250.0 /

END

*****
SUBROUTINE MISSN
*****
MAKES MISSION PHASE DECISIONS AND INVOKES THE DIFFERENT MODES
OF GUIDANCE AS REQUIRED. DELIVERS NZC AND PHIC TO THE AUTOPILOT
CONTRCL LOOPS. NYC IS ASSUMED TO ALWAYS BE ZERO EXCEPT DURING
ATTACK. NZC IS LIMITED TO *4.0 AND -2.0 G'S.
*****
IMPLICIT REAL(A-Z)
INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NULT,PCJUNT,NFAZE

*****
COMMON ELCCCK /A/: MISCELLANEOUS CONSTANTS
*****

COMMON /A/ TIME ,FINTIM,DT ,CPUT ,NCT ,NPTS ,CPA ,PCJUNT,
, I ,PHO ,PI ,PII ,PASS ,NT ,S ,

```

```

* * *
      IXX      , IYV      , IZ2      , IXZ      , IA      , IB      , JS      ,
      ID      , IE      , IF      , IG      , IH      , II      , IK      ,
      CHORD2, CHORD      , SPAN2, SPAN      , NFAZE

```

```

*****
COMMON BLOCK /C/: CONTROL SYSTEM PARAMETERS
*****

```

```

* * * * *
COMMON /C/  KPITCHR      , KROLLR      , KY ART      , KBANK      ,
              KGAMMA      , KALT      , CGARML      , CGARM      ,
              RRTLLIM      , PLIM      , KNY      , KNZ      ,
              AILRON      , STBLTR      , RUCCER      ,
              BSERO      , NZ SERO      , NY SERO
* * * * *

```

```

*****
COMMON BLOCK /D/: MISSILE FLIGHT DYNAMICS PARAMETERS
*****

```

```

* * * * *
COMMON /D/  ALFA      , BETA      , VT      , HMDUT      ,
              U      , V      , W      , X      , Y      , Z      ,
              PHI      , GAMMA      , THETA      , SY      ,
              CD      , CY      , CL      , CR      ,
              CM      , CN      , P      , PDUT      ,
              R      , ALFAUT      , BE TAUT      , Q      ,
              CUOT      , RDOT      , NZ      , ALTUDE      ,
              XM      , YM      , XMDCT      , YMDCT
* * * * *

```

```

*****
COMMON BLOCK /F/: GUIDANCE PARAMETERS
*****

```

```

* * * * *
COMMON /F/  PH1      , PH2      , PH3      , PH4      ,
              CFFSET      , ALTATT      , SGZPU      , M1SDST      ,
              LAMDZ      , LAMDEL      , KNFAPZ      , M1SUFEL      ,
              NZC      , PHIC      , GAMMAC      , KNFEL      ,
              PC      , QC      , RC      , PCLIM      ,
              SIGAZ      , SIGEL      , SIGUAF      , KANGE      ,
              SYT      , THETAT      , XT      , SIGDEF      ,
              FT      , NYC      , PUPRNG      , YI
* * * * *

```

```

*****
COMMON BLOCK /G/: CLUTPUT PARAMETERS
*****

```

```

* * * * *
COMMON /G/  AJA      , Sidesl      , BANK      , FLTPHC      ,
              EANKC      , PITCH      , KULLKT      , KULLTC      ,
              PTCRT      , YAWRT      , HEALNG      , FLTPH
* * * * *

```

```

* * * * *
HEADT      ,ELEV      ,DSIGAZ      ,DSIGEL      ,
DSGOAZ      ,USGDEL      ,ERFEK      ,ERFRR      ,
ERF AZ
*****
MISSION PHASE LOGIC AND GUIDANCE CCMANES

1 IF (PH4.EC.1) GO TO 40
  IF (PH3.EC.1) GO TO 30
  IF (PH2.EC.1) GO TO 20
  IF (PH1.EC.1) GO TO 10

*** INGRESS FROM INITIAL CONDITION TO OFFSET MANEUVER
      IF (RANGE.LT.18000.0) GO TO 5
      ALTITUDE HOLD

      ALTC      = 50.0
      ALTUOF      = ALTUOE
      GAMMAC      = KALT*(ALTC-ALTUOF)/VT
      GAMMAF      = GAMMA
      AZC      = COS (GAMMAF)*KGAMMA*VT*(GAMMAC-GAMMAF)/G

      PROPORTIONAL NAVIGATION IN AZIMUTH

      AYC      = LAMCAZ*VT*SIGDAF/G
      FFIC      = ATAN2(AYC,AZC)
      NZC      = AZC*CUS(PHI)+AYC*SIN(PHI)
      GC TO 100
      FF1      = 1

5
*** OFFSET TURN (60 DEG BANK) TO OFFSET HEADING
1C      ABSCSZ = ABS(DSIGAZ)
      IF (AESDSZ.GT.OFFSET) GO TO 19
      ALTITUDE HOLD

      ALTC      = 50.0
      ALTUOF      = ALTUOE
      GAMMAC      = KALT*(ALTC-ALTUOF)/VT
      GAMMAF      = GAMMA
      AZC      = COS (GAMMAF)*KGAMMA*VT*(GAMMAC-GAMMAF)/G

```

```

C      C      BANK ANGLE HCLD (60 DEG)
C      C      AYC = 0.0
C      C      PFIC = 60.0/PII
C      C      NZC = AZC/COS(PHI)
C      C      GC TO 100
C      C      PF2 = 1
C      C      15
C      C      ***
C      C      COURSE HCLD UN OFFSET HEADING TO PUPUP
C      C      20
C      C      ABDSC2 = ABS(DSGCAZ)
C      C      IF(AEDSD2.GT.SGDZPU) GU TO 29
C      C      C
C      C      ALTITUDE HCLD
C      C      C
C      C      ALTC = 50.0
C      C      ALTUDF = ALTUCE
C      C      GAMMAC = KALT*(ALTC-ALTUDF)/VT
C      C      GAMMAF = GAMMA
C      C      AZC = COS(GAMMAF)+KGAMMA*VT*(GAMMAC-GAMMAF)/G
C      C      C
C      C      BANK ANGLE HCLD (0 DEG)
C      C      C
C      C      AYC = 0.0
C      C      PFIC = 0.0
C      C      NZC = AZC/COS(PHI)
C      C      GC TO 100
C      C      PF3 = 1
C      C      25
C      C      ***
C      C      PULLUP TO ATTACK ALTITUDE
C      C      PROPORTIONAL NAVIGATION IN AZIMUTH
C      C      C
C      C      30
C      C      IF(ALTUDE.GT.ALTATT) GU TO 39
C      C      C
C      C      VERTICAL FLIGHT PATH ANGLE HCLD (8.5 DEG)
C      C      C
C      C      ALTC = 0.0
C      C      GAMMAC = 8.5/PII
C      C      GAMMAF = GAMMA
C      C      AZC = COS(GAMMAF)+KGAMMA*VT*(GAMMAC-GAMMAF)/G
C      C      C
C      C      PROPORTIONAL NAVIGATION IN AZIMUTH
C      C      C
C      C      AYC = LAMDAZ*VT*SIGDAF/G
C      C      NZC = AZC*COS(PHI)+AYC*SIN(PHI)
C      C      PFIC = ATAN2(AYC,AZC)
C      C      GC TO 100
C      C      PF4 = 1
C      C      35

```



```

C ***
C      ATTACK
C      PROFCRTICNAL NAVIGATION IN AZIMUTH AND ELEVATION
C
C      4 C
C
C      ALTIC = 0.0
C      GAMMAC = 0.0
C      GAMMAF = GAMMA
C      AYC = LAMCAZ*VI*SIGDAF/G
C      AZC = LAMDEL*VI*SIGDEF/G+COS(GAMMAF)
C      NZC = AZC*COS(PHI)+AYC*SIN(PHI)
C      NYC = 0.0
C
C      BANK ANGLE CCMAND ROUTINE INSURES ROLL
C      IN SHORTEST DIRECTION
C
C      PFIC = ATAN2(AYC,AZC)
C      CELPHI = PHIC-PHI
C      LPHIAB = ABS(CELPHI)
C      IF(OPHIAB.LT.PI) GO TO 100
C      IF(PFIC.GE.0.0) GC TC 90
C      PFIC = PHIC+2.0*PI
C      GC TO 100
C      PFIC = PHIC-2.0*PI
C
C      9C CONTINUE
C      10C *****
C *** NZ COMMAND LIMITED TO -2 & +4 G'S
C      NZC = LIMIT(-2.0,4.0,NZC)
C
C      RETURN
C      END
C
C      *****
C      SUBROUTINE APILOT
C      *****
C      LIMIT, FEALPL
C      *****
C      MODELS THE INNER LOOP AUTOPILOT AND CONTROL MIXER. CALCULATES
C      REQUIRED ELEVATOR,AILERON & RUDDER REQUERES THESE TO GET
C      THE FIN STABILATOR COMMANDS, APPLIES THE FIN LIMITS UP +-15 DEG.
C      AND ADJUSTS THE THREE CONTROL OUTPUTS TO ACCOUNT FOR THE LIMITS.
C      *****
C      IMPLICIT REAL(A-Z)
C      INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CFA,ROLL,PLUNTI,NFAZE

```

9-07-84

```

*****
COMMON BLOCK /A/: MISCELLANEOUS CONSTANTS
*****
COMMON /A/ TIME , FINTIM, DT , CPDT , NCUT , NPTS , CPA , PCOUNT,
* , , , , , , , , , ,
* , IXX , IYY , IRHU , PI , PI1 , PASS , WT , S ,
* , ID , IE , IF , IG , IA , IB , IC , Q ,
* CHORD2, CHURD , SPAN2, SPAN , NFAZE , IH , II , JK ,
*****

*****
COMMON BLOCK /C/: CONTROL SYSTEM PARAMETERS
*****
COMMON /C/ KPTCHR , KRCLLR , KYAWKT , KBANK ,
* , KGAMMA , KALT , CGARMN ,
* , RRTLLIM , PLIM , CGARML ,
* , AILRON , STBLTR , KNYDCER ,
* , BSERU , NZSERU , NYSERO ,
*****

*****
COMMON BLOCK /D/: MISSILE FLIGHT DYNAMICS PARAMETERS
*****
COMMON /D/ ALFA , BETA , VT , HMDUT ,
* , PHI , V , W , ,
* , CD , GAMMA , THETA , SY ,
* , CM , CY , CL , CR ,
* , R , CN , P , Q ,
* , QDOT , ALFADT , PDUT ,
* , XM , RDCT , NZ , ALTUDE ,
* , YMDCT ,
*****

*****
COMMON BLOCK /F/: GUIDANCE PARAMETERS
*****
COMMON /F/ PHI , PH2 , PH3 , PH4 ,
* , OFFSET , ALIATT , SDCZPU , MISDST ,
* , LAMDAZ , LAMDEL , KNFAPZ , KNFEL ,
* , PC , PHIC , GAMFAC , PCLIM ,
* , SIGAZ , QC , KC , RANGE ,
* , SYT , THETAT , XI , SIODEF ,
* ,
*****

```

```

* HT ,NYC ,PU PRNG
EXECUTABLE SIMTS *****
INNER LCCF AUTOPILOT

NORMAL ACCELERATION COMMAND SYSTEM

NZCLIM = LIMIT(-2.0,4.0,NZC)
NZZ = NZ+CGARM*(DOT/G
ENZ = NZCLIM-NZZ
ENZKNZ = ENZ*KNZ
QC = QC + ENZKNZ*DT
NZSERI = QC-KPTCHR*G
NZSEFC = REALPL(NZSERO,0.025,NZSERI,DT)
ELE = -PII*NZSERO

BANK ANGLE COMMAND SYSTEM

EPHI = PHIC-PHI
PC = KBANK*EPHI
PCLIM = LIMIT(-PLIM,PLIM,PC)
EP = PCLIM-P
BSERI = EP*KROLLR
BSERC = REALPL(BSERO,0.025,BSERI,DT)
AIL = -PII*BSERO

TURN COORDINATOR
IF(PT4,EC.1) GO TO 30
NYC = 0.0
CONTINUE
NYV = NY+CGARM*L*RDOT/G
ENY = NYC-NYV
RC = ENY*KNY*DT
NYSEFI = RC-KYAW*TR
NYSEFC = REALPL(NYSERO,0.025,NYSERI,DT)
RUD = -PII*NYSERC
CONTROLS MIXER AND LIMITS
LSTABI = ELE-AIL
KSTABI = ELE+AIL
LSTAB = LIMIT(-15.0,15.0,LSTABI)
30

```



```

* *      AILRON      STBLTR      RUDDER      ,
      BSERO      NZSERO      NYSERO      ,

*****
COMMON BLOCK /D/: MISSILE FLIGHT DYNAMICS PARAMETERS
*****

COMMON /C/ ALFA      BETA      VT      HMDOT
      PHI      V      W      THETA      ,
      CO      CY      CL      SY      ,
      CM      CN      P      CR      ,
      R      Q      PUOT      ,
      QUOT      ALFADT      BETADT      ,
      XM      RDCT      NZ      ALTUDE      ,
      YMDCT      YMDCT      ,

*****
SIDESL = PII*BETA
AOA = FII*ALFA

CLEAS = TABLE1(LFT1,ACA)
DCLSTE = TABLE1(LFT2,STBLTR)
CDBAS = TABLE1(DRG1,CLBAS)
DCCDSTE = TABLE1(DRG2,STBLTR)
DCCSTIA = TABLE1(DRG3,AILRON)
DCLCSTR = TABLE1(DRG4,RUDDER)
CMBAS = TABLE1(PTCH1,ACA)
DCMSTE = TABLE1(PTCH2,STBLTR)
CYBAS = TABLE2(SID1,ACA,SIDESL)
CRBAS = TABLE2(SID2,ACA,SIDESL)
CNRBAS = TABLE2(SID3,ACA,SIDESL)
DCVSTR = TABLE2(DREC1,ACA,RUDDER)
DCNSTR = TABLE2(DREC2,ACA,RUDDER)
DCVSTA = TABLE2(LTRL1,ACA,AILRCN)
DCNSTA = TABLE2(LTRL2,ACA,AILRCN)
DCRSTA = TABLE2(LTRL3,ACA,AILRCN)

AERCDYNAMIC COEFFICIENTS

CL = CLEAS+DCLSTE+CHORD2*(CLAUT*ALFADT+CLQC*Q)/VT
CD = CLEAS+DCLSTE+DCCDSTE+DCCDSTR+CHORD2*(CDACT*ALFADT+CDQC*Q)/VT
CY = CLEAS+DCVSTR+DCYSTA+SPAN2*(CYR*R+CYP*P+CYBUT*BETADT)/VT
CM = CMEAS+DCMSTE+CHORD2*(CMADT*ALFADT+CMQ*Q)/VT
CN = CNEAS+DCNSTR+DCNSTA+SPAN2*(CNBDT*BETADT+CNRR*R+CNPP*P)/VT
CK = CREAS+DCRSTA+DCRSTR+SPAN2*(CKRLT*BETADT+CKRR*R+CKPP*P)/VT

```

```

C C C C
AERODYNAMIC FORCES AND MOMENTS
L = CL*CS
D = CD*CS
LA = SPAN*CR*QS
MA = CFCR*CM*QS
NA = SPAN*CN*QS
X = L*SIN(ALFA)-D*COS(ALFA)
Y = CY*QS
Z = -L*COS(ALFA)-D*SIN(ALFA)

C C C
NORMAL & LATERAL ACCELERATIONS
NZ = -Z/(MASS*G)
NY = Y/(MASS*G)

C C C C
*** COMMENCE INTEGRATION OF EQUATIONS OF MOTION
EULER ANGLES
PHIDOT = P*TAN(THETA)*(Q*SIN(PHI)+R*COS(PHI))
THETAD = Q*COS(PHI)-R*SIN(PHI)
SYDOT = (Q*SIN(PHI)+R*COS(PHI))/COS(THETA)
PHI = PHI + PHIDOT*DT
THETA = THETA + THETAD*DT
SY = SY + SYDOT*DT

C C C
LINEAR ACCELERATIONS AND VELOCITIES
UDOT = -G*SIN(THETA)+V*R-W*Q+X/MASS+T/MASS
VDOT = G*SIN(PHI)+C*(THETA)-U*R+W*P+Y/MASS
WDOT = G*COS(PHI)+C*(THETA)+U*Q-V*P+Z/MASS
U = U + UDOT*DT
V = V + VDOT*DT
W = W + WDOT*DT
VT = SQR(U**2+V**2+W**2)
VTCOT = SQR(UDOT**2+VDOT**2+WDOT**2)

C C C
ANGULAR ACCELERATIONS AND VELOCITIES
PDCT = IR*LA+IC*NA-ID*P*Q-IE*R*L
QDOT = IR*MA-IG*P*R-IH*(P**2-R**2)
RDOT = IC*LA+II*NA-IJ*P*Q-IK*K*W
P = P + PDCT*DT
Q = Q + QDOT*DT

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```

K = R + RCOT*DT
ANGLES OF ATTACK, SIDESLIP, AND FLIGHT PATH
ALFADT = (ATAN(W/U)-ALFA)/DT
BETADT = (ASIN(V/VT)-BETA)/DT
ALFA = ATAN(W/U)
BETA = ASIN(V/VT)
GAMMA = ASIN(HMDOT/VT)

MISSILE POSITION IN INERTIAL SPACE
XMDOT = U*COS(SY)*COS(THETA)+V*(COS(SY)*SIN(THETA)*SIN(PHI)
      -SIN(SY)*COS(PHI))*W*(COS(SY)*SIN(THETA)*COS(PHI)+
      SIN(SY)*SIN(PHI))
YMDOT = U*SIN(SY)*COS(THETA)+V*(SIN(SY)*SIN(THETA)*SIN(PHI)
      +COS(SY)*COS(PHI))*W*(SIN(SY)*SIN(THETA)*COS(PHI)-
      COS(SY)*SIN(PHI))
HMDOT = U*SIN(THETA)-V*COS(THETA)*SIN(PHI)-W*COS(THETA)*COS(PHI)
HURDOT = SCR(XMDOT**2+YMDOT**2)
XM = XM + XMDOT*DT
YM = YM + YMDOT*DT
ALTUDE = ALTUDE + HMDOT*DT

RETURN
END

*****
FUNCTION TABLE (ARRAY,IP)
*****
TABLE LOOKUP WITH LINEAR INTERPOLATION FOR A FUNCTION
OF ONE VARIABLE, Y=F(X). MAXIMUM NUMBER OF FUNTS IS
LIMITED TO 30 BY THE DIMENSION STATEMENT. NCIE: THE
FIRST ARRAY ENTRY (ARRAY(1,1)) EXACTLY BE 9999.0 AND ALL
UNUSED ARRAY ELEMENTS MUST BE EXACTLY 9999. THE INDEPENDENT
VARIABLE DATA IS STORED IN ROW 1, THE DEPENDENT CALLS (ABOUT 5 DT'S)
WARNINGS ARE SUPPRESSED AFTER 20 CONSECUTIVE CALLS (ABOUT 5 DT'S)
*****
REAL ARRAY(2,30),IP,C,TABLE1
INTEGER I,J,K,N,SUPRES
DATA J,K,N /3*0/
K = K+1
IF (.NOT.IP.LT.ARRAY(1,1)) GO TO 10
TABLE1=ARRAY(2,1)

```



```

C      IF(SUPRES(J,K,N).EQ.1) WRITE(6,101) IF, TABLE1
C      RETURN
C      ENC IF
C
10 DO 90 I=1,30
    IF(.NOT.ARRAY(1,I).EQ.9995.0) GO TO 20
    TABLE1=ARRAY(2,I-1)
    IF(SUPRES(J,K,N).EQ.1) WRITE(6,102) IP, TABLE1
    RETURN
20 IF(.NOT.IP.GT.ARRAY(1,I)) GO TO 30
    GO TO 90
30 IF(.NOT.IP.EQ.ARRAY(1,I)) GO TO 40
    TABLE1 = ARRAY(2,I)
    RETURN
40 IF(.NOT.IP.LT.ARRAY(1,I)) GO TO 90
    C = (IP-ARRAY(1,I-1))/(ARRAY(1,I)-ARRAY(1,I-1))
    TABLE1 = ARRAY(2,I-1) + C*(ARRAY(2,I)-ARRAY(2,I-1))
    RETURN
C      ENC IF
C      CONTINUE
C      WRITE(6,103)
C      RETURN
C
C      FORMAT STATEMENTS FOR SUBROUTINE TABLE1*****
101 FORMAT('0','SUBROUTINE TABLE1: INPUT BELOW INDEPENDENT VARIABLE DA
    *TA.//:
    *      USED LOWEST DATA AVAILABLE = ',F10.2,
102 FORMAT('0','SUBROUTINE TABLE1: INPUT ABOVE INDEPENDENT VARIABLE DA
    *TA.//:
    *      USED HIGHEST DATA AVAILABLE = ',F10.2,
103 FORMAT('0','SUBROUTINE TABLE1: ERROR. SUBROUTINE DID NOT END )
    END
C
C
C      9-07-84*****
C      FUNCTION TABLE2(A,IP,IV)*****
C      *****
C      TABLE LOOKUP WITH LINEAR INTERPOLATION FOR A FUNCTION
C      OF TWO VARIABLES, Z=F(X,Y). MAXIMUM NUMBER OF INPUT PARAMETERS IS
C      LIMITED TO 5, INDEPENDENT VARIABLE DATA POINTS TO 9 BY THE
C      DIMENSION OF THE ARRAY. A(1,1) IS NOT USED. THE PARAMETER VALUES
C      ARE STORED IN COL 1, INDEP. VAR. VALUES IN ROW 1. THE COEFFICIENT
C      DATA ARE STORED IN THE GRID CREATED BY ROW AND COL 1.
C      TABLE2 WARNINGS ARE SUPPRESSED AFTER 5 CONSECUTIVE OCCURRENCES.***

```

```

C      REAL A(6,10),IP,IV,CP,CV,LFI,RGT, TABLE 2
C      INTEGER I,LI,UI,J,K,N,SUPRES
C      DATA J,K,N /3#0/

C      K = K+1
C      IF(.NOT.IP.LT.A(2,1)) GO TO 10
C      CP = 0.
C      LI = 2
C      UI = 2
C      IF(SUPRES(J,K,N).EQ.1) WRITE(6,1001) IP,A(2,1)
C      GO TO 55

C      10  DC 50 I=2,6
C      IF(.NOT.A(I,1).EQ.9999.0) GO TO 20
C      IF(SUPRES(J,K,N).EQ.1) WRITE(6,1002) IP,A(I-1,1)
C      CP = 0.
C      LI = I-1
C      UI = I-1
C      GO TO 55

C      20  IF(IP-A(I,1)) 30,40,50
C      IP < A(I,1)
C      CP = (IP-A(I-1,1))/(A(I,1)-A(I-1,1))
C      LI = I-1
C      UI = I
C      GO TO 55

C      30  IF = A(I,1)
C      CP = 0
C      LI = I
C      UI = I
C      GO TO 55

C      40  END IF
C      CONTINUE

C      50  IF(.NOT.IV.LT.A(1,2)) GO TO 60
C      IF(SUPRES(J,K,N).EQ.1) WRITE(6,1003) IV,A(1,2)
C      TABLE2=A(LI,2)+CP*(A(UI,2)-A(LI,2))
C      RETURN

C      55  DC 100 I=2,10
C      IF(.NOT.A(I,1).EQ.9999.0) GO TO 70
C      IF(SUPRES(J,K,N).EQ.1) WRITE(6,1004) IV,A(I-1,1)
C      TABLE2=A(LI,I-1)+CP*(A(UI,I-1)-A(LI,I-1))
C      RETURN

```

```

7C      IF (IV-A(L,I)) 80,90,100
C      IV < A(L,I)
80      CV = (IV-A(L,I-1))/(A(L,I)-A(L,I-1))
      LFT = A(L,I-1)+CP*(A(L,I)-A(L,I-1))
      RGT = A(L,I)+CP*(A(L,I)-A(L,I-1))
      TABLE2 = LFT+CV*(RGT-LFT)
      RETURN
C      IV = A(L,I)
90      TABLE2 = A(L,I)+CP*(A(L,I)-A(L,I-1))
      RETURN
C      END IF
100      CONTINUE
C      END IF
C      WRITE(6,1005)
C      RETURN
C
C      FORMAT STATEMENTS FOR SUBROUTINE TABLE2*****
1001  FORMAT('0','SUBROUTINE TABLE2: INPUT PARAMETER, BELOW DATA.',
*      'INPUT PARAMETER',
*      'USED LOWEST PARAMETER',
1002  FORMAT('0','SUBROUTINE TABLE2: INPUT PARAMETER, ABOVE DATA.',
*      'INPUT PARAMETER',
*      'USED HIGHEST PARAMETER',
1003  FORMAT('0','SUBROUTINE TABLE2: INPUT INDEP. VAR. BELOW DATA.',
*      'INPUT INDEP. VAR.',
*      'USED LOWEST INDEP. VAR.',
1004  FORMAT('0','SUBROUTINE TABLE2: INPUT INDEP. VAR. ABOVE DATA.',
*      'INPUT INDEP. VAR.',
*      'USED HIGHEST INDEP. VAR.',
1005  FORMAT('0','SUBROUTINE TABLE2: ERROR. SUBROUTINE DID NOT END.')
C      END
C
C      *****
C      FUNCTION SUPRES(J,K,N)
C      *****
C      DETERMINES TO SUPPRESS WARNINGS FROM TABLE1 OR TABLE2 AFTER THEY
C      HAVE BEEN CALLED ABOUT 20 TIMES IN A ROW. (ABOUT 5 UT INTERVALS.)
C      *****
C      INTEGER J,K,N, SUPRES
C
C      IF (K-J.EQ.1) GO TO 10
C      N = 0
C      K = 0
C      J = 0
C      GO TO 10

```

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```

10 CONTINUE
   N = N+1
   J = K
15 CONTINUE
   IF (N.EC.20) WRITE(6,105)
105  FORMAT('0','TABLE LCOKUP WARNINGS SUPPRESSEC')
   IF (N.GE.20) SUPRES = 1
   IF (N.LT.20) SUPRES = 0
   RETURN
   END

```

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```

*****
SUBROUTINE TGINAV
*****
RNG, SCV
*****
NAVIGATES THE TARGET AND COMPUTES RELATIVE RANGE, RANGE RATES,
INCCRPCTATES ECM AND GLINT MODELS TO GIVE APPARENT TARGET
POSITIONS. ALSO CALCULATES LINE OF SIGHT ANGLES AND RATES.
*****
IMPLICIT REAL(A-Z)
INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CFA,NOLI,PCOUNT,NFAZE
*****
COMMON BLUCK /A/: MISCELLANEOUS CONSTANTS
*****
COMMON /A/ TIME , FINTIM,DT , CPDT ,NCLT ,NPTS ,CPA ,PCOUNT,
IXX , IYV ,RHO ,PI ,PTI ,MASS ,WT ,S ,
ID , IE , IZZ , IZ , IA , IB , IC ,
CHORD2,CHORD ,SPAN2 ,SPAN ,NFAZE ,IH ,IJ ,IK ,

```

```

*****
COMMON BLUCK /D/: MISSILE FLIGHT DYNAMICS PARAMETERS
*****
COMMON /D/ ALFA ,VT ,HMDOT ,
V ,W ,THETA ,
GAMMA ,SY ,
CY ,CL ,CK ,
CN ,P ,Q ,

```

```

** *
** *
** *
R      QUOT      ALFADT      BETADT      PDUT      ,
XM      XM      ,RUOT      ,NZ      ,ALTUDE      ,
      ,YM      ,XMDCT      ,VMDCT      ,

```

```

*****
COMMON BLOCK /E/: INITIAL CONDITIONS
*****

```

```

** *
** *
COMMON /E/  XM1  PITCH1  YM1  ALTUD1  UI  DES1
      AQAI  XTI  ,BANK1  ,HECNS1  ,SI  DES1
      ,XTI  ,PCHRI  ,KULLRI  ,YAWRI
      ,XTI  ,HTI  ,TSPEED

```

```

*****
COMMON ELCCCK /F/: GUIDANCE PARAMETERS
*****

```

```

** *
** *
COMMON /F/  PH1  CFFSET  PH2  ALTATT  PH3  SGZPU  PH4  MISDST
      LAMDZ  NZC  ,LAMDZ  ,ALTATT  ,SGZPU  ,MISDST
      PC  ,PHIC  ,KNFEL  ,KNFEL
      SIGAZ  ,WC  ,GAMMAC  ,PC  ,PCLIM
      SYT  ,SIGEL  ,RC  ,RANGE
      HT  ,THETAT  ,NYC  ,SI  GDEF
      ,XTI  ,YI

```

```

*****
COMMON ELCCCK /H/: ECM/GLINT PARAMETERS
*****

```

```

** *
** *
COMMON /H/  FREQ  SHIFT  BKNTHR
      XECM  ,YECM  ,XGLNT
      YGLNT  ,HGLIT  ,XTECM
      HTECM

```

```

C EXECUTABLE STATEMENTS:

```

```

** * TARGET ACTION

```

```

XI = XTI
YT = YTI+TSPEED*TIME
HT = HTI

```

```

RELATIVE RANGE TO TARGET

```

```
C      XR = XT-XM  
C      YR = YT-YM  
C      HR = HT-ALTUDE  
  
C *** RANGE & MISS DISTANCE  
C  
C      RINCE = SQRT(XR**2+YR**2+HR**2)  
C      IF(RNCE.GT.2000.)GC TO 25  
C      IF(RNCE.LT.RANGE)GO TC 25  
C          CPA = 1  
C          MISCST = RANGE  
C  
C      25 CONTINUE  
C      RANGE = RNCE  
C  
C *** GLINT MODEL (SUPPRESSED AT A RANGE OF 100 FT)  
C *****  
C KTEST = 1  
C IF(KTEST.EQ.1) GO TC 50  
C ***** ENDTEST  
C CALL RNG(RAND)  
C  
C IF(PCCLNT.NE.1) GO TO 100  
C   IF(RANGE.LT.100.0) GO TO 50  
C     XGLNT = 20*RAND  
C     YGLNT = 50*RAND  
C     HGLNT = 20*RAND  
C     GC TO 100  
C  
C       CCNTINE  
C  
C       XGLNT = 0.0  
C       YGLNT = 0.0  
C       HGLNT = 0.0  
C  
C 100 CONTINUE  
C  
C *** ECM BLINKING MODEL (SUPPRESSED AT BURN-THROUGH RANGE)  
C * SELECT THE PHASE APPLIED TO THE ECM SIGNAL  
C  
C   GO TO(1C1,1C2,103,104),NFAZE  
C 101 PPHASE = 0.0  
C    GC TC 105  
C 102 PPHASE = PI*.5  
C    GC TC 105  
C 103 PPHASE = PI  
C    GC TC 105  
C 104 PPHASE = PI*.5
```

```

C      105 CONTINUE
C      POPRNG = PHASE*PI11
C      IF (RANGE.LT.BRNTHR) GO TO 350
C      XECMH = SIN(2*PI*FREQ*TIME+PHASE)
C      XECM = SQWV(XECMH,SHIFTX)
C
C      YECMH = SIN(2*PI*FREQ*TIME+PHASE)
C      YECM = SQWV(YECMH,SHIFLY)
C
C      HECMH = SIN(2*PI*FREQ*TIME+PHASE)
C      HECM = SQWV(HECMH,SHIFTH)
C      GO TO 400
C
C      35C CONTINUE
C      XECM = 0.0
C      YECM = 0.0
C      HECM = 0.0
C
C      400 CUNTINUE
C
C      XTECM = XI+XECM+XGLNT
C      YTECM = YI+YECM+YGLNT
C      HTECM = HI+HECM+HGLNT
C
C      *** RELATIVE RANGE AND RANGE RATE TO RADAR TARGET
C
C      XTECM = XTECM-XM
C      YTECM = YTECM-YM
C      HTECM = HTECM-ALTUDE
C      RNTECM = SQRT(XTECM**2+YTECM**2)
C      RGECHT = SQRT(XTECM**2+YTECM**2+HTECM**2)
C
C      XDCTR = -XMDOT
C      YDCTR = TSPEED-YMCDOT
C      HDCTR = -HMDOT
C      HURDTR = SQRT(XDCTR**2+YDCTR**2)
C
C      *** SEEKER LCS AND LCS RATE CALCULATIONS
C
C      SYT = ATAN2(YTECM,XTECM)
C      TRAKAZ = ATAN2(YMDCT,XMDUT)
C      SIGAZ = SYT-TRAKAZ
C
C      VTANAZ = -XDCTR/SIN(SYT)+YDCTR*CGS(SYT)
C      SIGGAZ = VTANAZ/RNTECM
C      SIGDAF = REALPL(SIGDAF,KNFAZ,SIGGAZ,DT)

```



```

SUBROUTINE PREPAR
*****
DESIGNATES UP TO 20 PARAMETERS TO BE STORED FOR OUTPUT AND
ASSIGNS THEM TO THE NEXT ROW OF THE PITS ARRAY. EACH PARAM. IS
STORED IN A COLUMN OF THE ARRAY FROM ROW 3 UNTIL THE END OF THE
ARRAY IS REACHED OR CPA OCCURS. ROWS 1 & 2 CONTAIN MINIMUM AND
MAXIMUM VALUES OF EACH VARIABLE RESPECTIVELY. COL. 1 CONTAINS
THE VALUES OF TIME FOR EACH POINT. NPTS IS COMMON TO BLOCK A
AND INDICATES THE NUMBER OF POINTS STORED.
*****
IMPLICIT REAL(A-Z)
INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NUCT,PCOUNT,NFAZE
DIMENSION KEEP(20)
*****
COMMON /A/ TIME , FINTIM,DT , CPDT , NUCT , NPTS , CPA , PCOUNT,
IXX , IYY , IZZ , IXXZ , IYA , IYB , IYC , IYQ , IYJ , IYK ,
ID , IE , IF , IG , IH , II , IJ , IK ,
CHORD2,CHURC , SPAN2,SPAN ,NFAZE
*****
C' "MON /C/ KPTCHR ,KYAWRT ,KBANK ,
KGAMMA ,CGARML ,CGARMIN ,
RRTLLIM ,KNY ,KNZ ,
AILRON ,RUDCEK ,
BSERO ,NYSERO ,
*****
COMMON /C/ ALFA ,VT ,HMDOT ,
U ,W ,THETA ,SY ,CR ,Q ,POOT ,ALTUDE ,YMDOT ,
PHI ,CL ,P ,BEIADT ,NZ ,XMDCT ,
CU ,CN ,ALFADT ,RDOT ,YM ,
CM ,R ,CDOOT ,XM ,
*****
COMMON /E/ XM1 ,ALTLU1 ,U1 ,STDESI ,YAWRI ,TSPEED ,
PITCH1 ,HEDNCL ,ROLLR1 ,HT1 ,
AUA1 ,BANK1 ,PTCHR1 ,VT1 ,
XT1 ,PH2 ,PH3 ,SGDZPU ,MI SUST ,PH4 ,MISUST ,NNFEL ,PCLLIM ,RANGE ,
*****
COMMON /F/ PH1 ,OFFSET ,PH1 ,LAMDALZ ,LAMDAL ,KAFZ ,GAMMAC ,KC ,
UFFSET ,LAMDALZ ,NLC ,PC
*****

```

```

* * * SIGAZ SIGDEF
* * * SYT ,YI
* * * FT ,POPRNG

COMMON /G/ AOA ,FLTPHC
BANKC ,ROLKTC
PTCHRT ,FLTPTH
HEADT ,DSIGEL
DSGDAZ ,ERFRK
ERFAZ

COMMON /H/ FREQ ,BRNTHK
XECM ,XULNT
VGLNT ,YTECM
HTECM

COMMON /I/ PTS(300,20),PLTN(6,7),XN(6,7),YN(6,7),TITLE(6),
LEG(4,20)

EXECUTABLE STMTS *****
RACIAN TC DEGREE CONVERSIONS FOR ULPUT

AOA = ALFA*PII
SIDESL = BETA*PII
BANK = PHI*PII
FLTPHC = GAMMA*PII
BANKC = PHIC*PII
PTCH = THETA*PII
ROLLRT = P*PII
ROLKTC = PCLIM*PII
PTCHRT = C*PII
YAWRT = R*PII
HEADNG = SY*PII
FLTPTH = GAMMA*PII
ELEV = SYT*PII
DSIGAZ = THETA*PII
DSIGEL = SIGAZ*PII
DSGDAZ = SIGEL*PII
DSGLEL = SIGDAF*PII

*** CREATE THE MISSION PHASE MARKER (MARK)
MARK = C.0
IF (PH1.EC.1)MARK = 1.0
IF (PH2.EC.1)MARK = 2.0

```

```

C      IF (PH3.EQ.1)MARK = 3.0
C      IF (PH4.EQ.1)MARK = 4.0
C      NPTS = NPTS+1
C      K = NPTS+2
C      *** COMPUTE THE ERROR FUNCTIONS
C
C      IF (MARK.EQ.4) GO TO 50
C      ERBK = 0.0
C      ERRRR = 0.0
C      ERRAZ = 0.0
C      ERREL = 0.0
C      GC TC 100
C      50 CONTINUE
C      ERBK = ERRBK + ABS(BANKC-BANK) *DI
C      ERRRR = ERRRR + ABS(ROLLRTC-ROLLKT) *DI
C      ERRAZ = ERRAZ + ABS(DSQUAZ) *DI
C      ERREL = ERREL + ABS(DSGUEL) *DI
C      100 CONTINUE
C
C      ERFBK = ERRBK/TIME
C      ERFRK = ERRRR/TIME
C      EKFEZ = ERRAZ/TIME
C      *** SELECT THE VARIABLES TO BE STORED
C      KEEP(1) = TIME
C
C      GRAPH 1 = NZC
C      KEEP(2) = NZC
C      KEEP(3) = NZ
C
C      GRAPH 2 = BANKC
C      KEEP(4) = BANKC
C      KEEP(5) = BANK
C
C      GRAPH 3 = ROLLRTC
C      KEEP(6) = ROLLRTC
C      KEEP(7) = ROLLRT
C
C      GRAPH 4 = YECM
C      KEEP(8) = YECM
C      KEEP(9) = YCLNT
C
C      GRAPH 5 = AILRCN
C      KEEP(10) = AILRCN

```

```

C      KEEP(11) = STBLTR
C      KEEP(12) = RUDDER
C
C      GRAPH 6
C      KEEP(13) = ALTUDE
C
C      GRAPH 7
C      KEEP(14) = XM
C      KEEP(15) = YM
C      KEEP(16) = XT
C      KEEP(17) = YT
C
C      SPARES
C      KEEP(18) = RANGE
C      KEEP(19) = MARK
C      KEEP(20) = NYC
C
C      *** STORE MINIMUM AND MAXIMUM VALUES OF EACH VARIABLE
C
C      DO 20 I=1,20
C      IF (NPTS.GT.1) GO TO 10
C      P1S(1,I) = KEEP(1)
C      P1S(2,I) = KEEP(1)
C      10      CCNTINUE
C      P1S(1,I) = AMIN1(P1S(1,I),KEEP(1))
C      P1S(2,I) = AMAX1(P1S(2,I),KEEP(1))
C      20 CONTINUE
C
C      *** STORE VALUES OF EACH VARIABLE WITH THE TIME
C
C      DO 30 I=1,20
C      P1S(K,I) = KEEP(1)
C      30 CONTINUE
C
C      *** CHECK FOR ARRAY OVERFLOW AND TERMINATE AT 255 POINTS
C      IF (NPTS.GE.295) CPA = 3.0
C
C      RETURN
C      END
C
C      *****
C      SUBROUTINE CUIPUT(NPTS,CPA)
C      *****
C      HEACER, PLOT1, PLOT2, PLOT3, PLOT21, PLOT13
C      *****
C      *****

```

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```

C C C C C C C
RECEIVES THE DATA FROM THE PROGRAM IN THE PTS ARRAY. PRINTS THE
PRIME CLIPUT AND DATA RANGES TO THE SCREEN AND TABULAR OUTPUT TO
FILE 9 (TCMC DATA). THEN IT PROCESSES THE DATA FOR PLOTTING USING
DISPLA. THE BASIC FORMAT OF THE SEVEN GRAPHS CALLED IN THIS S/R
IS FIXED BUT THE TITLES AND THE VARIABLES CAN BE EASILY CHANGED BY
CHANGING THE PARAMETERS IN THE DATA STATEMENTS IN THIS S/R. THE
TITLE GIVEN HERE WILL BE PRINTED FOR ALL PLOTS.
*****
IMPLICIT REAL(A-Z)
INTEGER KFILE,NPTS,I,J,K,L,M,N,NN,CPA,
NDV(5,7),DV(4),LEG(4,20),PLIN(6,7),
XN(6,7),YN(6,7),TITLE(8,4),MESS1(2),MESS2(2)
*
*

```

```

C C C C
DIMENSION YP(10),XP(10)
*****

```

```

COMMON /F/ PH1 OFFSET
LAMDZ
NZC
PC
SIGAZ
SYT
HT
PH2
ALTTAT
LAMDEL
PHIC
QC
SIGEL
THETAT
NYC
PH3
SGDZPU
KNFAZ
GAMMAC
RC
SIGCAF
XT
POPRNG
PH4
MISOST
KNFEL
PCLIM
RANGE
SIGDEF
YT

```

```

COMMON /G/ AOA
BANK
PITCHRT
HEADT
CSGDZ
ERFAZ
SIDESL
PITCH
YAWRT
ELEV
DSGDEL
ERFEL
BANK
ROLLRT
HEADING
USIGAZ
ERFER
FLTPHC
RULRTIC
FLTPTH
USIGEL
ERFER

```

```

COMMON /H/ FREQ
XECM
YGLNT
HTECM
SHIFTH
HECM
XTECM
BRNTHR
XGLNT
YTECM

```

```

C C C C C C C
COMMON /I/ PTS(300,20)
*****
***** INITIALIZE THE GRAPHICS CONTRCL ARRAY *****
*****

```

EACH ROW IN THE DATA STATEMENT (COLUMN OF THE ARRAY) CORRESPONDS TO A SINGLE GRAPH. THE FIRST ELEMENT IS A FLAG (1 TO PLOT, 0 TO PASS OVER). THE NEXT 4 ELEMENTS


```

C      FLAG = 1.0
C      18 CONTINUE
C
C      ***** WRITE PRIMARY DATA OUTPUT *****
C      ***** TO FILE 6 (TERMINAL) AND THEN FILE 9 (TCMC DATA) *****
C
C      DO 100 K=1,2
C      IF(K.EQ.1)KFILE=0
C      IF(K.EQ.2)KFILE=5
C
C      ***** TITLES *****
C      *****
C      20 WRITE(KFILE,20)((TITLE(I,J),I=1,8),J=1,4)
C      FCRMAT('1',4(20X,8A47))//)
C
C      ***** INDICATE HOW THE SIMULATION TERMINATED *****
C      ***** GC TC(30,40,50),CPA *****
C
C      30 WRITE(KFILE,35)
C      35 FCRMAT(1X,'SIMULATION TERMINATED DUE TO CPA')
C      GC TO 60
C
C      40 WRITE(KFILE,45)
C      45 FCRMAT(1X,'SIMULATION TERMINATED DUE TO FINTIME')
C      GC TO 60
C
C      50 WRITE(KFILE,55)
C      55 FCRMAT(1X,'SIMULATION TERMINATED DUE TO FULL ARRAY')
C
C      60 CCNTINUE
C
C      ***** VALUE OF THE ITERATED PARAMETER *****
C
C      65 WRITE(KFILE,65) FREQ
C      FCRMAT(1X,'*** BLINKER FREQUENCY= ',F8.2)
C
C      67 WRITE(KFILE,67) PCPKNG
C      FCRMAT(1X,'*** BLINKER PHASE = ',F6.0//)
C
C      ***** LIST THE PRIMARY DATA OUTPUTS *****
C
C      75 WRITE(KFILE,75) MISDST,ERFBK,ERFKR,ERFAZ,ERFEL
C      FCRMAT(1X,'MISSED ***** ERROR ***** BANK *****')
C      ***** / ***** DISTANCE ***** * *****

```

```

* * ROLLRATE * AZIMUTH * ELEVATION *//
5(3X,F10.5,2X,*,*////////)

C **
C LIST THE VARIABLE RANGES
C
C 80
C WRITE(KFILE,80)
C FCFMAT(18X,*,* RANGES FOR ALL SAVED VARIABLES *****
C //30X,*,* MINIMUM
C WRITE(KFILE,90)((LEG(I,J),I=1,4),PTS(1,J),PTS(2,J),J=1,20)
C FCFMAT(11X,4A4,4X,F12.6,3X,F12.6)
C
C 100 CONTINUE
C
C ***** TABULAR DATA OUTPUT *****
C
C DO 200 I=1,4
C J=(I-1)*4+2
C K=J+3
C WRITE(9,20)((TITLE(L,M),L=1,8),M=1,4)
C WRITE(5,65) FREQ
C WRITE(9,125) I
C FCFMAT(50X,*,* DATA SET NUMBER *,I,*,*(F 4,///)
C WRITE(9,135)((LEG(L,1),L=1,4),((LEG(L,M),L=1,4),M=J,K)
C FCFMAT(2X,20A4,///)
C
C 125
C 135
C
C NN=APTS+2
C DC 150 N=3,NN
C START NEW PAGE EVERY 65 LINES
C L = MOD(N,65)
C IF(L.NE.0) GC TO 140
C WRITE(9,20)((TITLE(L,M),L=1,8),M=1,4)
C WRITE(9,65) FREQ
C WRITE(9,125) I
C WRITE(9,135)((LEG(L,1),L=1,4),((LEG(L,M),L=1,4),M=J,K)
C
C 140
C CONTINUE
C WRITE(9,145) PTS(N,1),PTS(N,L),L=J,K)
C FCFMAT(1X,5(*,*,F12.6,3X))
C
C 145
C 150
C 200 CONTINUE
C
C ***** PRCLUCE GRAPHIC OUTPUT USING DISSPLA SUEROUTINES *****
C
C *****

```


[illegible]

```

DO 50 J=1,3
DC 30 I=1,8
      HC(I) = TITLE(I,J)
30  CONTINUE
50  CALL HEADIN(HC ,32 , 1-1 ,4)
DO 60 I=1,6
      HC(I) = PLTN(I,KP)
      XNM(I) = XN(I,KP)
      YNM(I) = YN(I,KP)
60  CONTINUE
      CALL HEADIN(HD ,24 , 1-0 ,4)
      CALL XNAME( XNM ,24)
      CALL YNAME( YNM ,24)
      RETURN
END
*** FILE: FLCT1 ***
*** CONTAINS ALL S/R'S THAT INTERFACE WITH CISSPLA EXCEPT HEADER ***
*** 9-10-84 ***
*** SUBROUTINE PLOT1(MESS1,MESS2,VARI,VAR2) ***
*** INITIALIZES DISSPLA FGR A NEW PAGE AND GRAPH ***
*** IMPLICIT REAL(A-H,C-Z),INTEGER(I-N) ***
*** DIMENSION MESS1(2),MESS2(2) ***
      CALL NCCKEK
      CALL GRACE(0.)
      CALL BLCAUP(3.,647)
      CALL PACET(11.,8.5)
      CALL HWFCT('AUTO')
      CALL HNSCAL('SCREEN')
      CALL NCERDR
      CALL PHYSQR(1.,.75)
      CALL AREA2C(9.,6.5)
      CALL SWISSM
*** PUT THE MESSAGES INTO THE GRAPHS
CALL MESSAGE(MESS1,8,0.2,0.0)

```

```

CALL SUBROUTINE PLOT2(P1S,LEG,DV,IV,NPTS)
RETURN
END
SUBROUTINE PLOT2(P1S,LEG,DV,IV,NPTS)
LOADS THE LEGEND ARRAY WITH CURVE LABELS: P1S THE POINTS FOR
EACH CURVE, DEPENDENT VARIABLE: PLOT2S: INDEXES. IV,DV ARE IN-
DEPENDENT, DEPENDENT VARIABLE: P1S: INDEXES. THE COLUMN IN
THE P1S ARRAY WHERE THE LABELS FOR EACH CURVE IS A 4
ELEMENT ARRAY CONTAINING THE INDEXES FOR UP TO 4 DEP VAR'S.

```

```

** ** ** ** ** ** ** ** **  8-26-84  ** ** ** ** 
** ** ** ** 
** SUBROUTINE PLOT2(P,T,S,LEG,DV,I,V,NPTS)  ** ** ** ** 
** ** ** ** 
** LOADS THE LEGEND ARRAY WITH CURVE LABELS; GETS THE POINTS FOR EACH CURVE FROM THE P T S ARRAY; PLOTS EACH CURVE. I,V,DV ARE INDEPENDENT, DEPEND ON THE VARIABLE INDEXES. THEY GIVE THE COLUMN IN THE P T S ARRAY WHERE THEIR VALUES ARE FOUND. LEG IS THE PACKED ARRAY CONTAINING THE LABELS FOR EACH VARIABLE. DV IS A 4 ELEMENT ARRAY CONTAINING THE INDICES FOR UP TO 4 DEP VAR'S.
** ** ** ** 

```

```
DATA MONEY /' $ ' /
*** FIRST FIND OUT HOW MANY CURVES THERE ARE
```

```

I=1
5 IF (DV(I)-EQ,0) GO TO 10
   MCFV=I
   IF (I-EQ,4) GO TO 10
   I=I+1

```

*** NEXT PACK THE LEGEND ARRAY AND RANGE THE Y-AXIS

```

15      CCNTINE = AMIN1(YMIN,PTS(1,K))
          YMIN = AMIN1(YMIN,PTS(1,K))
          YMAX = AMAX1(YMAX,PTS(2,K))

```


AD-A152 193

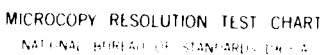
AN INVESTIGATION INTO THE CONTROL LIMITATIONS OF A BANK 3/3
TO TURN MISSILE IN THE TERMINAL HOMING PHASE(U) NAVAL
POSTGRADUATE SCHOOL MONTEREY CA B P ANDERSON SEP 84

UNCLASSIFIED

F/G 17/7

NL





```

09-05-84
** SUBROUTINE PLOT3(NPTS,PTS,TITLE)
** *****
** CREATES A 3-D GEOGRAPHICAL PLOT OF MISSILE AND TARGET
** TRACKS. BY CHANGING THE VIEWPOINT YCU CAN RESERVE DIFFERENT
** PORTIONS OF THE MISSION FROM VARIOUS PERSPECTIVES.
** *****
** IMPLICIT REAL(A-H,C-Z), INTEGER(I-N)
** INTEGER TITLE(8,4),HU(6)
** DIMENSION PTS(300,20),XP(300),YP(300),ZP(300),IPACK(100)

CALL BLCWUP(1.0)

*** CREATE THE TITLES

DO 40 J=1,3
DC 30 I=1,8
      HC(I) = TITLE(I,J)
30 CONTINUE
40 CALL HEADIN(HC,32,1.1,4)
   CALL HEADIN('GEOGRAPHICAL TRACKS',15,1.0,4)

*** DEFINE THE WORKBOX

CALL VCLM3D(10,20,7.5)

*** LABEL THE AXES

CALL XNAME('FEET EAST',9)
CALL YNAME('FEET NCRTH',10)
CALL ZNAME('ALTITUDE (FT)',13)

** DEFINE THE VIEWPCINT

CALL VLANGL(130,40,26)

** SET UP THE AXIS SYSTEM

CALL CRCS
CALL GRAF3D(-1000.,1000.,4000.,0.0,5000.,25000,
```


APPENDIX E

LISTING FOR SUBROUTINE MISSN1

```

*****9-07-84*****
SUBROUTINE MISSN1
*****
SEA SKIMMER GUIDANCE SCHEME. ALLOWS VARIABLE POPUP IN CLOSE
WITH NC OFFSET TURN. AFTER POPUP, GUIDANCE IS STANDARD PRO-
PORTIONAL. POPUP USES ONLY ALTITUDE COMMAND VICE GAMMAC.
*****
MAKES MISSION PHASE DECISIONS AND INVOKES THE DIFFERENT MODES
OF GUIDANCE AS REQUIRED. DELIVERS NZC AND PHIC TO THE AUTOPILOT
CONTROL LOOPS. NYC IS ASSUMED TO ALWAYS BE ZERO. NZC IS LIMITED
TO +4.C AND -2.0 G.S.
*****
IMPLICIT REAL(A-Z)
INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NULT,PCOUNT,NFAZE
*****
COMMON ELCK /A/: MISCELLANEOUS CONSTANTS
*****
COMMON /A/ TIME , FINTIM,DT , CPDT , NCLT , APTS , CPA , PCOUNT,
IXX , IYY , RHU , PI , PII , MASS , WT , S ,
ID , IZ , IZ2 , IA , IB , IC , US ,
CHORD2,CHORD , SPAN2,SPAN , NFAZE , IH , II , IK ,
*****
COMMON /C/: CONTROL SYSTEM PARAMETERS
*****
COMMON /C/ KPTCHR , KRCCLR , KYAKNT , KQANK ,
KGAMMA , KALT , CGARML , CGARMLN ,
RRTLIM , KJY , KJY , KNZ ,
AILRON , STBLTR , RUDDER ,
BSERO , NZSERO , NYSEK
*****
COMMON BLOCK /D/: MISSILE FLIGHT DYNAMICS PARAMETERS
*****

```

[illegible]

APPENDIX F

LISTING FOR SUBROUTINE MISSA2

```

*****
***** SUBROUTINE MISSA2 *****
***** 9-07-84 *****
*****
***** BALLISTIC GUIDANCE SCHEME. ALLOWS VARIABLE POPUP IN CLOSE *****
***** WITH NC OFFSET TURN. AFTER POPUP, MISSILE RCLLS TO 50 DEGREES *****
***** ANGLE OF BANK AND USES LATERAL AND VERTICAL PROPORTIONAL NAV. *****
*****
***** MAKES MISSION PHASE DECISIONS AND INVOKES THE DIFFERENT MODES *****
***** OF GUIDANCE AS REQUIRED. DELIVERS NZC AND PHIC TO THE AUTOPILOT *****
***** CONTRL LGOPS. NYC IS ASSUMED TO ALWAYS BE ZERO. NZC IS LIMITED *****
***** TO +4.C AND -2.0 G.S. *****
*****
***** IMPLICIT REAL(A-Z) *****
***** INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NULT,PCOUNT,NFAZE *****
*****
***** COMMON /A/ TIME ,FINTIM,DT ,CPUT ,NULT ,NPTS ,CPA ,PCOUNT, *****
***** IXX ,IYY ,RHO ,PI ,PII ,MASS ,MT ,S *****
***** ID ,IE ,IZZ ,IXZ ,IA ,IB ,IC *****
***** CHORD2,CHORD ,SPAN2,SPAN ,NFAZE ,IH ,IJ ,IK *****
*****
***** COMMON /C/ KPTCHR ,KRULLR ,KYAWRT ,KBANK *****
***** KGAMMA ,KALT ,CGARML ,CGARMN *****
***** RRTLLM ,PLIM ,KNZY ,CGARMN *****
***** AILRUN ,STBLTR ,RUDDER *****
***** RSERO ,NZSERO ,NYSERU *****
*****
***** COMMON /C/ ALFA ,BETA ,VT *****
***** LPHI ,V ,THETA *****
***** CD ,CY ,CL *****
***** CM ,CN ,P *****
***** R ,ALFADT ,BETAUT *****
***** QUOT ,RDGT ,NZ *****
***** XM ,YM ,XMDCT *****
*****
***** COMMON /F/ PH1 ,PH2 ,PH3 *****
***** OFFSET ,ALFATT ,SGDZPU *****
***** PH4 ,MISUST *****
*****

```

[illegible]


```

C **      PULLF TC ATTACK ALTITUDE
C          PROFCRTIONAL NAVIGATION IN AZIMUTH
C
C          ***** PATCH TC RETAIN BIT GUIDANCE TO IMPACT (KTEST=1)
C          KTEST = 1
C          IF (KTEST.EQ.1) GO TO 32
C          ***** ENDPATCH *****
C          3C      IF (ALTITUDE.GE.ALTAIT) GO TO 39
C
C          32      CONTINUE
C                  CCMMAND BALLISTIC ATTACK ALTITUDE
C
C                  ALIC = ALTAIT
C                  ALTUDF = ALTUDE
C                  GAMMAC = KALT*(ALIC-ALTUDF)/VT
C                  GAMMAF = GAMMA
C                  AZC = COS(GAMMAF)+KGAMMA*VT*(GAMMAC-GAMMAF)/G
C
C                  PROPORTIONAL NAVIGATION IN AZIMUTH
C
C                  AYC = LAMCAZ*VT*SIGDAF/G
C                  NZC = AZC*COS(PHI)+AYC*SIN(PHI)
C                  PFIC = ATAN2(AYC,AZC)
C                  GC TO 100
C                  PF4 = 1
C
C          35
C          ***      ATTACK
C          PROFCRTIONAL NAVIGATION IN AZIMUTH AND ELEVATION
C
C          CCMMAND ATTACK ALTITUDE & ROLL TC 90 DEG BANK.
C
C          4C      PFIC = PI/2.
C                  ALIC = ALTAIT
C                  ALTUDF = ALTUDE
C                  GAMMAC = KALT*(ALIC-ALTUDF)/VT
C                  GAMMAF = GAMMA
C                  AZC = KGAMMA*VT*(GAMMAC-GAMMAF)/G
C
C                  PROFCRTIONAL NAVIGATION IN AZIMUTH
C
C                  AYC = LAMDAZ*VT*SIGDAF/G
C                  NZC = AZC*COS(PHI)+AYC*SIN(PHI)
C                  NYC = AYC*COS(PHI)-AZC*SIN(PHI)
C                  NYC = 0.0
C
C          10C CONTINUE
C          *****

```

NZ COMPAND LIMITED TO -2 & +4 G'S; NYC TO +/- 0.5 G.
 NZC= LIMIT(-2,0; 4,0,NZC)
 NYC= LIMIT(-0.5; 0.5,NYC)
 RETURN
 END

C
 C
 C

LIST OF REFERENCES

1. Fitterson, Kent E., BANK-TO-BANK CONVERSION MANUAL, Fitterson Guidance and Control Systems, Inc., 14511, California, 1983.
2. IBM Company, Continuous System Modelling Program III (CSMP III), Program Reference Manual, Program Number 5734-XS9, December 1975.
3. Speckhart, F.H., and Green, W. L., A Guide to Using CSMP-III, Continuous System Modelling Program, Prentice-Hall, 1975.
4. Hewett, M.D., Guidance and Control Systems Course (Class Notes), 1983.
5. Boskam, J., Airplane Flight Dynamics and Automatic Flight Controls, Boskam Aviation and Engineering Corp., 1979.

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